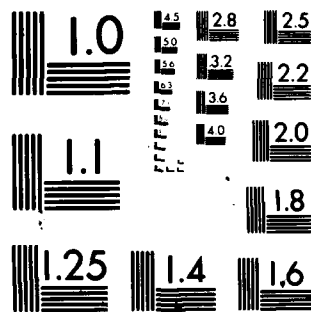


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 DEC61 USERS MANUAL. A FORTRAN IV PROGRAM FOR COMPUTING THE STA--ETC(U)
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CIVIL ENGINEERING LABORATORY

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20. Continued

As written, DECEL1 should be compilable on most Fortran IV compilers with Boolean algebra capabilities.

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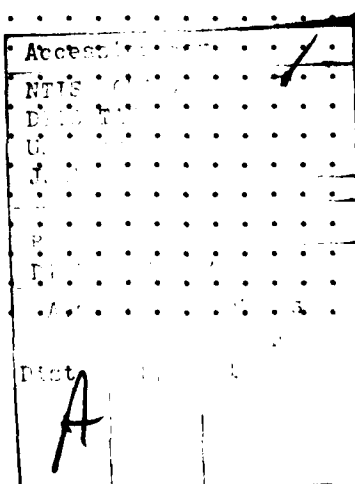
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CONTENTS

	Page
PREFACE	1
Force Calculations	1
Current Field Definition	1
Plotting Options	2
Miscellaneous User Conveniences	2
Iteration Control	2
INTRODUCTION	2
Computer Requirements	4
Program Operation	4
Array Description	4
Reduction to a Statically Determinate Array	7
Coordinate Systems	8
Current Field - Input Option 0	12
Current Field - Input Option 1	12
Current Field - Input Option 2	13
Current Field - Input Option 3	15
TANGENTIAL DRAG	17
CABLE DEVICES	17
REFERENCE CONFIGURATION	18
ITERATION CONTROL AND EXECUTION ERROR MESSAGES	18
What To Do If	19
DECEL1 USER EXPERIENCE	19
Load Distribution	19
Non-Convergent Problems	21
Convergence Parameters	23
INPUT CARDS	24
LUN Card	26
Main Descriptive Title Card	28
NJNC Card	29
ANC Card	30
IR Card	31
CAB Card	32
Continuation CAB Card	34
DCAB Card	35
DJNC Card	37
DEN Card	38
EOD Card	39
NDAT Card	41
Parametric Descriptive Title Card	44



	Page
COMP Card	45
VEL Card	47
ANG Card	52
PPLT Card	54
CPLT Card	55
EOD Card	57
EOP Card	58
Cable Array Source Deck	59
Cable Array Source Tape	59
Parametric Study Source Decks	60
OVERALL INPUT DECK	62
ERROR MESSAGES	64
DEFINITION OF ERRORS	64
ARRAY DESCRIPTIVE OUTPUT	69
STRUCTURAL OUTPUT	69
DEVICE LOCATION OUTPUT	70
REC Record	71
CUR Record	71
DEV Record	72
EOP Record	72
REFERENCES	78
APPENDICES	
A - Example Problem	79
B - DECEL1 Program Listing	93

LIST OF ILLUSTRATIONS

	Page
Figure 1. Generalized flow diagram of DECEL1 operation.	5
Figure 2. Typical cable arrays which can be analyzed using DECEL1.	6
Figure 3. Examples of proper reductions to statically deter- minate structures for the arrays shown in Figures 2a and 2b.	9

	Page
Figure 3. Examples of proper reductions to statically determine structures for the arrays shown in Figures 2c and 2d.	10
Figure 4. Description and relationship between the magnetic and array referenced coordinate systems.	11
Figure 5. Current field option 1 used in DECEL1 (a) Current angle, θ , (b) Current profile; $V(Z)$	14
Figure 6. Interpolation/extrapolation in the case of 2-string data.	16
Figure 7. Arrangement of data sets for velocity option 3.	49
Figure 8. Perspective view of the undeformed structure (field 3 = 0).	57
Figure 9. Perspective view of the deformed structure (field 3 = 1).	58
Figure 10. Perspective view of the deformed structure with the undeformed shape for comparison (field 3 = 2).	59
Figure 11. Unidirectional current field.	60
Figure 12. Non-unidirectional current field. (Note by sighting along the arrows that the field does curve.)	61
Figure 13. DECEL1 test case structure.	83
Figure 14. Current profile.	84
Figure 15. DECEL1 test case structure model.	85
Figure 16. Input card images.	86
Figure 17. Output from DECEL1 for the example problem.	87
Figure 18. Output from DECEL1.	90
Figure 19. Undeformed and deformed configurations of the test case structure.	92

PREFACE

The Civil Engineering Laboratory (CEL), under sponsorship of the Naval Facilities Engineering Command, is engaged in a program of developing numerical tools for analyzing cable systems. As part of this work the NRL-written DESADE program has been used. In the course of using DESADE several improvements and additions have been made. The modifications are for the most part minor and serve to increase the accuracy of the mathematical modeling and to add user conveniences.

This report documents these modifications in the form of a revised users manual. (Much of the text of the original manual is used without modification.) To distinguish the updated program from the original NRL version, the program has been renamed DECEL1 for DESADE, CEL version one.

CEL's modifications were in five general areas:

1. Force calculations
2. Current field definition
3. Plotting options
4. Miscellaneous user conveniences
5. Iteration control

Force Calculations

Drag force and weight of cable sections covered by in-line devices have been deleted. (This assumes an in-line device that terminates the cable at each end of the device; floats that are in-line and envelope the cable must have their buoyancy adjusted by the weight of the enveloped cable segment.) This addition has a relatively minor effect except when in-line devices envelope a significant portion of a cable.

Calculation of tangential drag has been added to both cables and in-line devices.

Current Field Definition

The capability to accept a current field defined by 2, 3 or 4 current meter strings of up to 25 meters each has been added. Since much current meter data is referenced to magnetic north, the cable structure can be referenced to the current field by specifying the angle between the structure's X-axis and magnetic north.

The specification of current direction has been changed to be consistent with oceanographic terminology: a 90° current flows due east.

An option has been added to specify the input current velocity units; all velocities within an NDAT case must be the same units.

Plotting Options

Options have been added to plot the current field defined by two or more current meter strings and to plot the cable structure in either its deformed or undeformed configuration. Perspective or plan or elevation views can be depicted.

Miscellaneous User Conveniences

Required title cards have been added for the cable structure source deck and for each parametric case.

The specification of indexed and unindexed devices has been simplified. User selected devices now are automatically indexed, in order, by their location along a cable.

The changes allowed in a parametric study deck are such that the physical appearance of the array could be altered in the parametric case so much that referencing displacements to the original no-current case is illogical. An option has been added to declare any parametric case as the new no-current reference case. Displacements are printed referenced to both the original no-current case and to the present parametric reference case. The reference parametric case can be redefined any number of times since the original no current case is retained for the duration of the problem.

The error detection and display scheme has been altered. Errors that are detected by DECEL1 cause the entire input deck to be listed. Then, the cards with errors are flagged with a coded error number. The coded error message text is printed below the input card listing. All cards are scanned for errors; however, only the first error on a particular card is detected. The error messages are identical to those in the original DESADE manual except that only the portion of the message applicable to the card type is printed.

In some cases it is desirable to be able to punch on cards the locations of particular devices for input to other programs. An option has been added to select, based on device weight, the devices whose location is to be punched.

Iteration Control

Under some circumstances that have not been well defined, DECEL1 may either fail to converge or converge very slowly. To protect the user from high execution costs, iteration limits have been imposed. Iterative techniques are used to satisfy the imaginary reaction displacement constraints and to obtain the structure shape. Both iteration processes have had limits imposed because both have been the cause of excessively high execution costs.

These modifications have added to the capabilities of DECEL1 and have made it a more useful tool for the cable structure analyst.

INTRODUCTION

DECEL1 is a Fortran IV program for computing the ocean current-induced static deflections of undersea structural cable arrays. The solution algorithm is the Method of Imaginary Reactions (Refs 1,2)

combined with the method of successive approximations for treating position and configuration dependent forces (Refs 3,4).

As dimensioned, the program can handle arbitrarily configured arrays of up to 22 cables. The cables can be electromechanical, wire rope, or synthetic. Any number of discrete devices (buoyancy elements, current meters, tensiometers, etc.) may be incorporated in the array.

Certain limitations are placed on the structural characteristics of the arrays which can be analyzed by this program. These limitations are as follows:

1. No cables or cable segments may lie on the ocean floor. (No surface or bottom interaction is modeled, thus a cable may hang below the lowest anchor point.)
2. The dimensions of each discrete device must be small compared to overall array dimensions. Thus, for example, the application of this program to the analysis of an anchorage for a submerged submarine is not valid.
3. All parts of the array must be submerged. Thus, an array containing a surface buoy cannot be validly analyzed using this program. (The reason for this is that a surface buoy generates only one geometric constraint on its location.) An exception occurs when all three coordinates of a device on the surface can be specified - for example, the coordinates of a ship handling a crown line.

Also, certain hydromechanical assumptions are incorporated in the program as written. These are as follows:

1. The only hydrodynamic force considered to be acting on the discrete devices is a drag force. For in-line devices a normal drag coefficient and a tangential drag coefficient can be specified. For a free device, only the normal drag coefficient is to be specified. Lift forces are neglected as being small compared to the weight, buoyancy, and drag forces on these devices.
2. The only hydrodynamic force considered to be acting on the cable is a drag force. This drag force consists of both normal and tangential components and consequently two drag coefficients (normal and tangential) are to be specified for each cable.
3. The current option 1 is depth dependent in magnitude, uni-directional and horizontal. The current option 2 permits direction and magnitude variation as a function of depth. The current option 3 also permits magnitude and direction variation as a function of depth. This option requires two, three or four "strings" of depth dependent velocity data (where the strings are located at arbitrary points). These velocity data are used within the code via interpolation or extrapolation to obtain the velocity at any arbitrary point in space. In all cases the vertical component of velocity is assumed to be zero.

An option for parametric studies (changes in weights, diameters, cable lengths, anchor locations, etc.) is included in the program. DECEL1 also contains a series of error checks which insure that all input data are properly formulated.

Perspective plotting package SSP has been incorporated into DECEL1 to plot the deformed and/or undeformed configuration of the array.

The program uses the internally generated nodal points of the cables as the points to be plotted.

Scratch files 3, 4 and 10 must be available for use in the plotting package SSP.

Computer Requirements

As written, DECEL1 should be compilable on most Fortran IV compilers with Boolean algebra capabilities. Memory requirements for the program are approximately 206,000 (octal) words in single precision. Access to one, two, or three magnetic tape units, depending on the I/O options chosen, is required by the program.

Program Operation

The overall operation of the program DECEL1 is shown in the flow diagram in Figure 1. Numerical examples in Appendix A and the source language listing of the program is given in Appendix B.

Array Description

Typical cable arrays which can be analyzed using DECEL1 are shown in Figures 2a-2d. The figures also show the numbering and coordinate system conventions required for transmitting the array geometry to DECEL1. These conventions are as follows:

1. The cables comprising the array must be numbered consecutively from one to the total number of cables in the array (C1, C2, ... in Figure 2). Each cable so designated must have uniform properties (weight, drag coefficients, diameter, and constitutive relation) along its length. A change in property also requires a change in cable number as illustrated in Figure 2a.
2. The termination points of the cables in the array are called junctions. A junction may designate an anchor, the intersection point of two or more cables, or the free end of a cable such as illustrated by junction J9 in Figure 2c. The junctions must also be numbered consecutively from one to the total number of junctions in the array (J1, J2, ... in Figure 2).
3. A fixed, right-handed (X, Y, Z) Cartesian coordinate system must be chosen to describe the configuration of the array in space. This coordinate system is called the array-referenced coordinate system. The origin of the coordinate system can be arbitrarily located. The Z axis must be defined parallel to the direction of gravity and increasing upward. All distances are measured in feet.

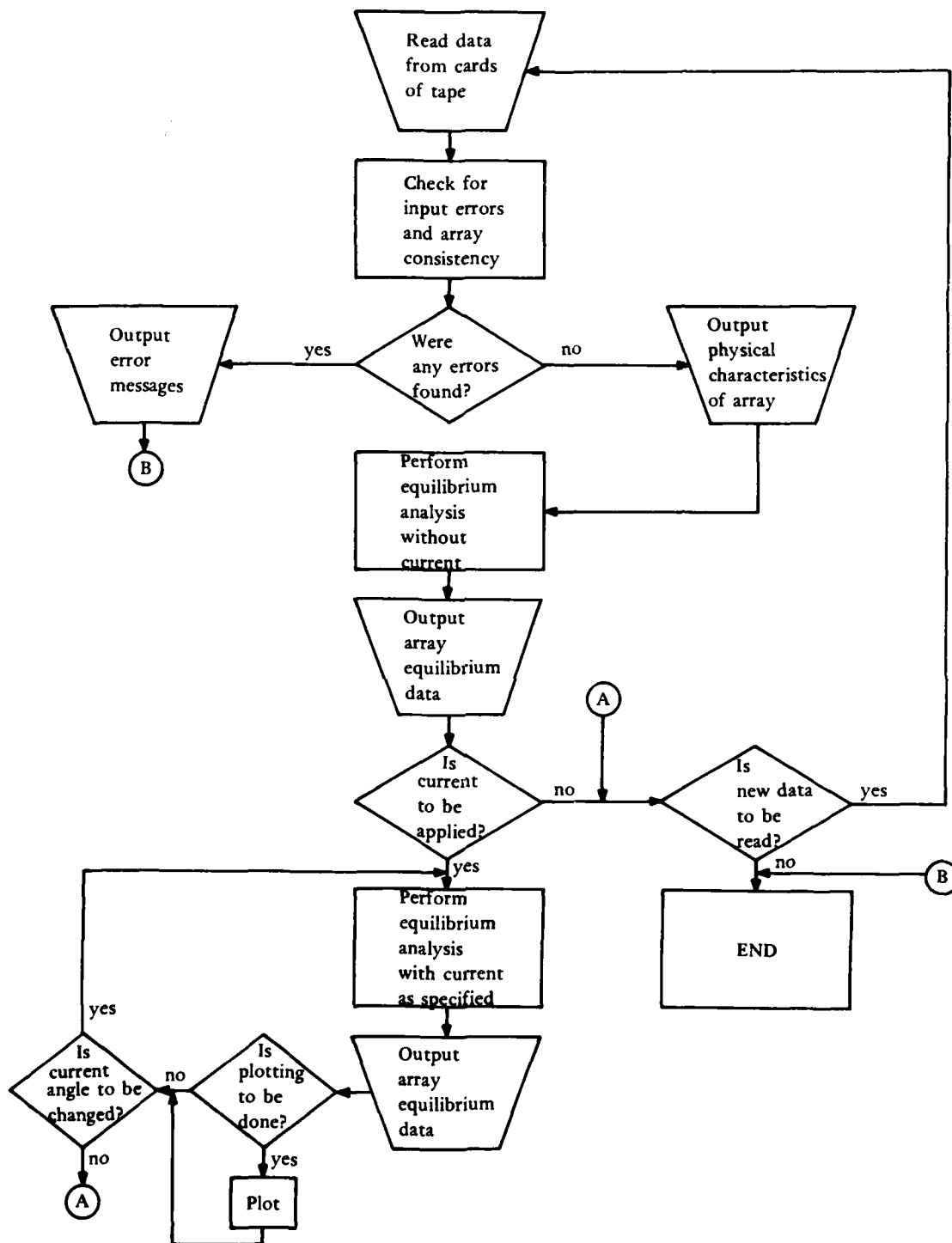


Figure 1. Generalized flow diagram of DECEL1 operation.

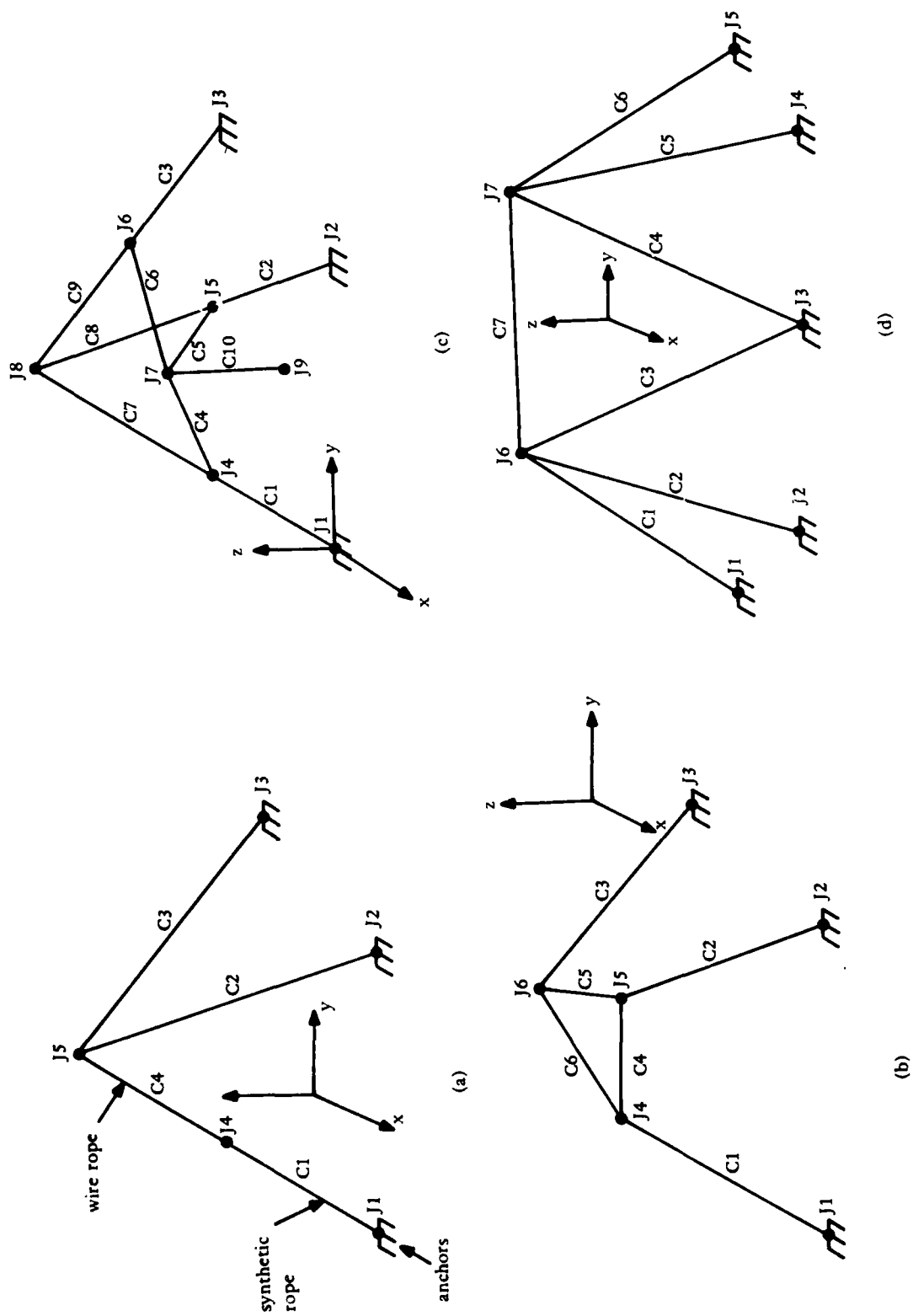


Figure 2. Typical cable arrays which can be analyzed using DECELL1.

4. The junction numbers corresponding to anchors and the coordinate of the anchors must be tabulated according to the scheme illustrated in Table 1.

Table 1. Anchor Tabulation

<u>Column 1</u>	<u>Column 2</u>	<u>Column 3</u>	<u>Column 4</u>
Junction number of Anchor	X coordinate (ft)	Y coordinate (ft)	Z coordinate (ft)

Anchors are defined to be any fixed end point of a cable; thus an "anchor" can be placed on the bottom or at the surface or anywhere within the water column.

Reduction to a Statically Determinate Array

Before an arbitrary cable array can be analyzed by DECELL, a sufficient number of cuts must be made in the array to reduce it to a statically determinate structure. The effects of the constraints removed by these cuts are replaced by imaginary and equilibrating reactions (Refs 1,2).

The number of cuts required to reduce a cable array to a statically determinate structure is determined uniquely from the relation

$$\begin{aligned} \text{number of cuts} &= \text{number of cables} + \text{number of anchors} \\ &\quad - \text{number of junctions} \end{aligned} \quad (1)$$

Certain rules must be adhered to as the required cuts are made. These rules are as follows:

1. All required cuts must be made at points directly adjacent to array junctions - that is at end points of the cables comprising the array.
2. The first group of cuts must be made so as to release all but one cable from an anchor.
3. The remaining cuts (if required) are made within the array structure and must be located so as not to break the array into two (or more) parts.
4. As cuts are made, each new cut must be assigned a consecutive junction number, continuing from the last-used junction number. Also, the junction number (in the original array) at which the cut is made must be tabulated.

In effect, applying rules 1-3 reduces the array to the equivalent of a topological tree. As the name implies, this is a continuous structure containing only one fixed point and for which a unique (nonduplicative) path exists from any point to any other point.

Examples of proper reductions to statically determinate structures for the arrays illustrated in Figures 2a-2d are shown in Figures 3a-3d, respectively. In each of these figures, the left-hand schematic shows the reduced array while the right-hand schematic depicts the topological tree representation of the reduced array. The information required by rule 4, which represents geometric constraints on the reduced array, is tabulated below the left-hand schematic in each figure.

Finally, it is necessary to define directions of increasing arc length along the cables comprising the array. The tree representation of the reduced array is used primarily for this purpose. These directions, indicated by the arrowheads in the right-hand schematic of each figure, are identified by starting from the base of the tree and climbing "up" the tree.

Let the measure of arc length along a cable be denoted by s which increases from zero to the total length of the cable L . Then, the required information on increasing directions of arc length can be summarized in terms of array junctions as shown in the table below the right-hand schematic in each figure.

Once an array has been reduced to the state represented by Figure 3, it is amenable to analysis by the program DECEL1.

Coordinate Systems

There are two coordinate systems used for inputting the data to DECEL1. They are the magnetically aligned reference coordinate system (N, W, Z) and the array or laboratory reference coordinate system (X, Y, Z). The two coordinate systems share the same origin and the same Z -axis; Z is positive upward. Consequently, the two coordinate systems can differ from one another by an arbitrary angular rotation in the horizontal plane which is denoted by ϕ . For arbitrary locations on the earth, the magnetic axes N - S and E - W are preestablished. Consequently, the angular rotation of the array-referenced coordinate system is referenced to the magnetic axes. In particular, ϕ is the angle between the N -axis and the positive X -axis. A positive rotation of the X -axis with respect to the N -axis is in the clockwise sense. Figure 4 illustrates the two coordinate systems.

The direction of positive rotation is in the clockwise sense in the magnetically aligned coordinate system. The zero degree reference is taken as the N -axis.

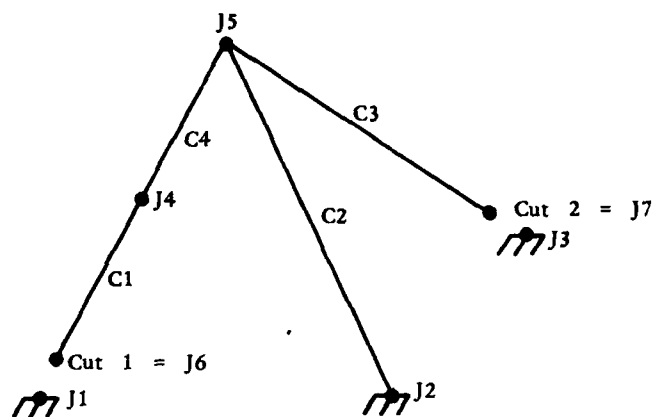
All current data to be input into the program are to be referenced with respect to the magnetic coordinate system. For example, a current having an inclination of 0° is flowing due north; a current with 270° inclination is flowing due west.

When current field input option 3 is selected, it is necessary to specify the locations on the ocean surface (horizontal plane) of the stations where current data have been gathered (relative to the N, W, Z coordinate origin). Typical examples of locations of such stations might be:

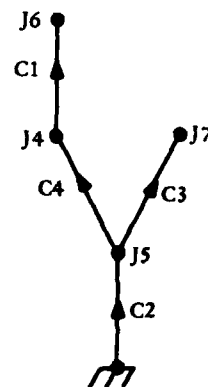
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100 ft N by 3000 ft W = ( 100, 3000)
700 ft S by 1500 ft E = (-700, -1500)
  0 ft N by  800 ft E = (   0, -800)
400 ft N by  450 ft W = ( 400,  450)

```

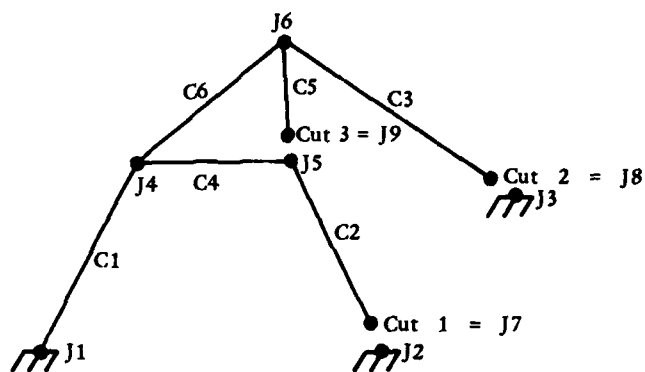



Cut No.	Junction No. Assigned To Cut	Junction No. At Which Cut Made
1	6	1
2	7	3

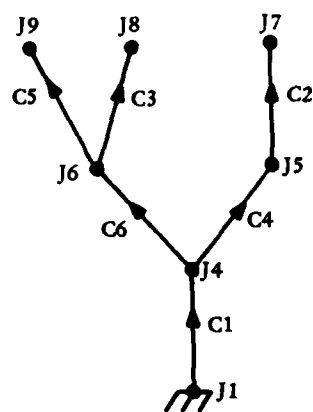


Cable No.	Junction No. At $s = 0$	Junction No. At $s = L$
1	4	6
2	2	5
3	5	7
4	5	4

(a)



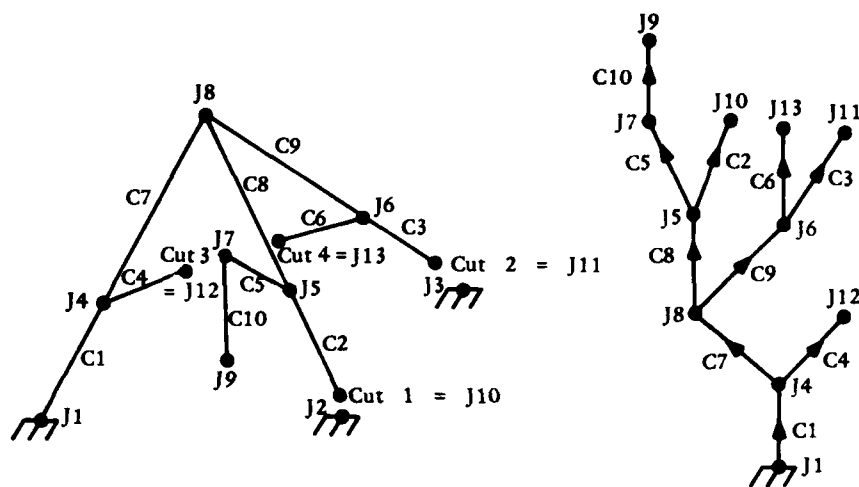
Cut No.	Junction No. Assigned To Cut	Junction No. At Which Cut Made
1	7	2
2	8	3
3	9	5



Cable No.	Junction No. At $s = 0$	Junction No. At $s = L$
1	1	4
2	5	7
3	6	8
4	4	5
5	6	9
6	4	6

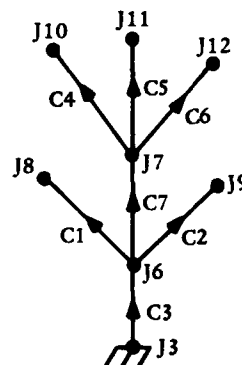
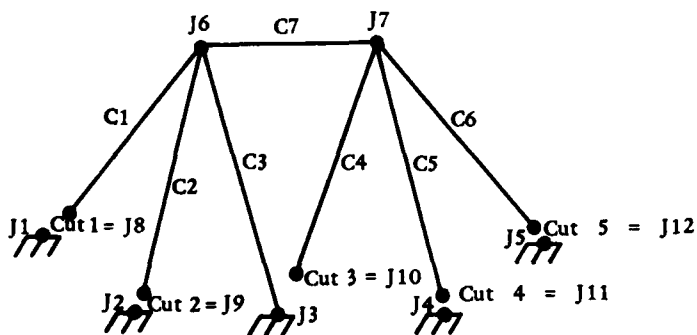
(b)

Figure 3. Examples of proper reductions to statically determinate structures for the arrays shown in Figures 2a and 2b.



Cut No.	Junction No. Assigned To Cut	Junction No. At Which Cut Made	Cable No.	Junction No.	
				At $s = 0$	At $s = L$
1	10	2	1	1	4
2	11	3	2	5	10
3	12	7	3	6	11
4	13	7	4	4	12
			5	5	7
			6	6	13
			7	4	8
			8	8	5
			9	8	6
			10	7	9

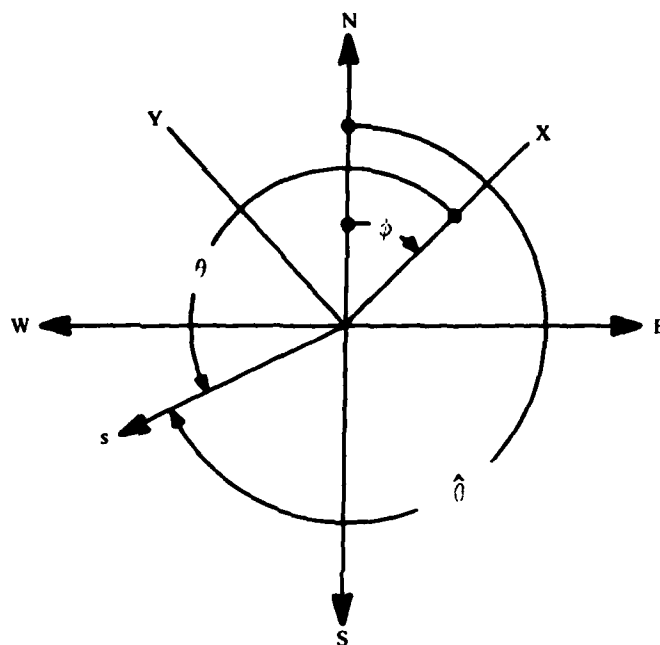
(c)



Cut No.	Junction No. Assigned To Cut	Junction No. At Which Cut Made	Cable No.	Junction No.	
				At $s = 0$	At $s = L$
1	8	1	1	6	8
2	9	2	2	6	9
3	10	3	3	3	6
4	11	4	4	7	10
5	12	5	5	7	11
			6	7	12
			7	6	7

(d)

Figure 3. Examples of proper reductions to statically determinate structures for the arrays shown in Figures 2c and 2d.



$$s = \sqrt{N^2 + W^2}$$

$$\theta = 360 + \phi - \hat{\theta}$$

$$X = s \cos \theta$$

$$Y = s \sin \theta$$

In the magnetic coordinate system the N,W axes are positive. (N,W) form a coordinate pair of a right handed coordinate system. The positive direction of rotation $\hat{\theta}$ in the (N,W) coordinate system is clockwise with the zero degree reference being the N - axis. The array coordinate system (X,Y) system. The relationship between the two systems is given above.

Figure 4. Description and relationship between the magnetic and array referenced coordinate systems.

Above (on the right), is an example of how such locations should be interpreted for input preparation as coordinate pairs. Note that the north-west quadrant is the first quadrant of a right-handed coordinate system. Consequently, north and west are positive axes while south and east are the negative axes. When current field input option 3 is selected, the current data are printed out in both the magnetic and array-referenced coordinate systems.

The specification of the anchor locations is accomplished with respect to the array-referenced (X, Y, Z) coordinate system. All internal calculations within DECELL are performed with respect to the array-referenced coordinate system. The (X, Y, Z) coordinate system is also right-handed. In the horizontal plane in this frame of reference the direction of positive rotation is counter-clockwise with the positive X-axis being the zero degree reference.

Directions of Positive Rotation

<u>Reference System</u>	<u>0° Reference</u>	<u>Positive Rotation</u>
Magnetic	N-axis	clockwise
Array	X-axis	counter-clockwise

Current Field - Input Option 0

There is an input option for determining the static deflections of a cable system immersed in a currentless environment. This is current field input option 0. This option is automatically processed when any of the subsequently described current field input options are exercised. It can be exercised independently.

Current Field - Input Option 1

The current field option 1 is taken to be unidirectional and horizontal, though depth dependent in magnitude. The direction of the current is specified from the magnetic north axis by using the ANG card. [Within the code, the current is referenced to the array coordinate system for calculation purposes. Thus, if the direction of the flow with respect to the X-axis is denoted by θ , the current field is expressed by:

$$V_1 = V(Z)(\underline{e}_1 \cos \theta + \underline{e}_2 \sin \theta)$$

Here, \underline{e}_1 , \underline{e}_2 are unit base vectors with respect to the X- and Y- axes, respectively.] $V(Z)$ specifies the magnitude of the current as a function of depth, Z. This functional relationship must be tabulated as in Table 2.

Table 2. Current Tabulation - Option 1

<u>Column 1</u>	<u>Column 2</u>
Z coordinate (ft)	V(Z) knots

Up to 25 rows are permitted in Table 2. At least one of the Z-coordinates in Table 2 must be less than or equal to the Z-coordinate of the lowest anchor. A sorting scheme is invoked within the program that arranges Table 2 data according to ascending values of Z. Such sorting is necessary within the program for the determination of the current of an arbitrary depth. This is accomplished via a linear interpolation of the currents using the data at the two depths encompassing the depth of interest.

Figure 5 illustrates the magnetic-referenced coordinate system and the linear interpolation of the velocity between given data points.

For current field input option 1, the directionality of the current is a constant for the entire velocity field. Also, for any point (X, Y) on the plane (Z = constant), the value of velocity is invariant.

Current Field - Input Option 2

Current field input option 2 is a slight generalization of the current field input option 1. The generalization involves allowing the current direction θ to vary with depth. The input specification for this option requires depth Z, current magnitude and current direction from the magnetic north axis. The positive direction of rotation is clockwise in the magnetically-aligned reference coordinate system and a zero degree current flows due north. The current specification for option 2 requires a tabulation as in Table 3.

Table 3. Current Tabulation - Option 2

<u>Column 1</u>	<u>Column 2</u>	<u>Column 3</u>
Z-coordinate	V(Z) magnitude, knots	$\theta(Z)$ direction, degrees from magnetic N-axis, positive in clockwise sense

Up to 25 rows are permitted in Table 3. The velocity sorting scheme is invoked by the program. One entry for this data must correspond to a depth less than or equal to the Z-coordinate of the lowest anchor. The above current magnitude and direction data are used to generate velocity components along the (X, Y) axes. To obtain the velocity at an arbitrary depth, linear interpolation is performed using the (X, Y) velocity components above and below the depth of interest; the angular direction of the current is also found by interpolation.

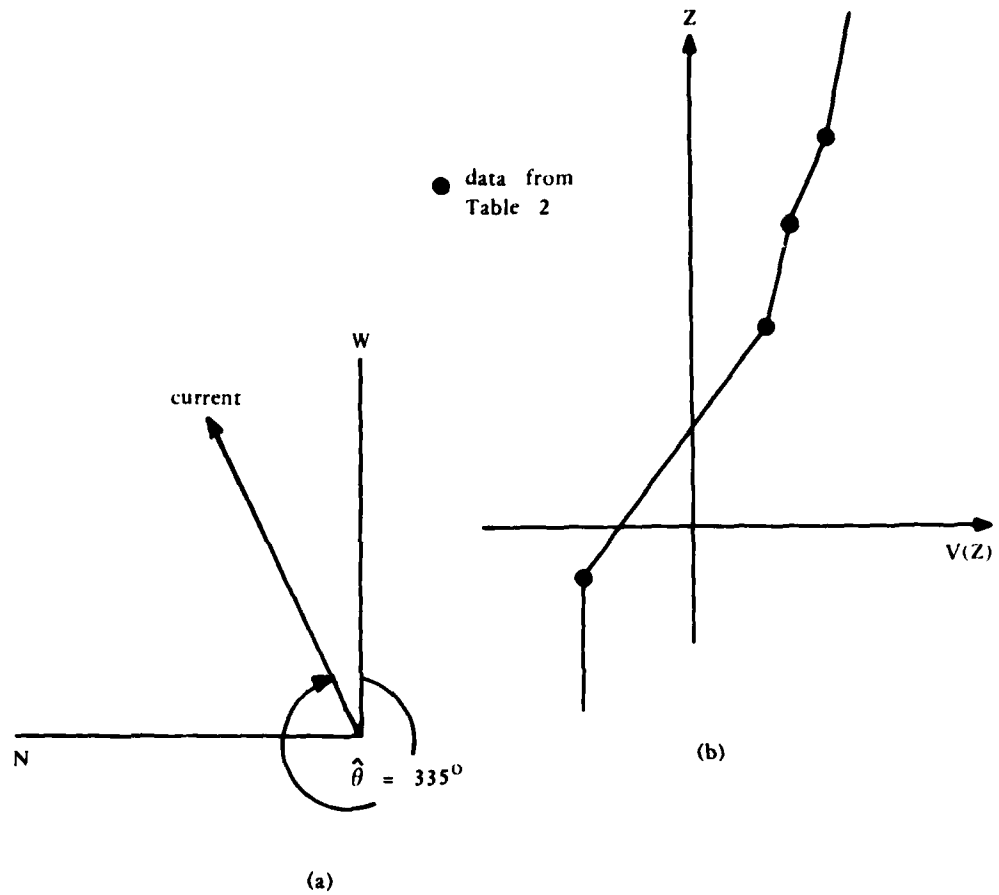


Figure 5. Current field option 1 used in DECEL1 (a) Current angle, θ , (b) Current profile, $V(Z)$.

For current option 2, the value of velocity at any (X, Y) point on the plane $Z = \text{constant}$ is invariant.

An ANG card can be used to rotate the entire current profile in the same manner that a unidirectional current profile is rotated.

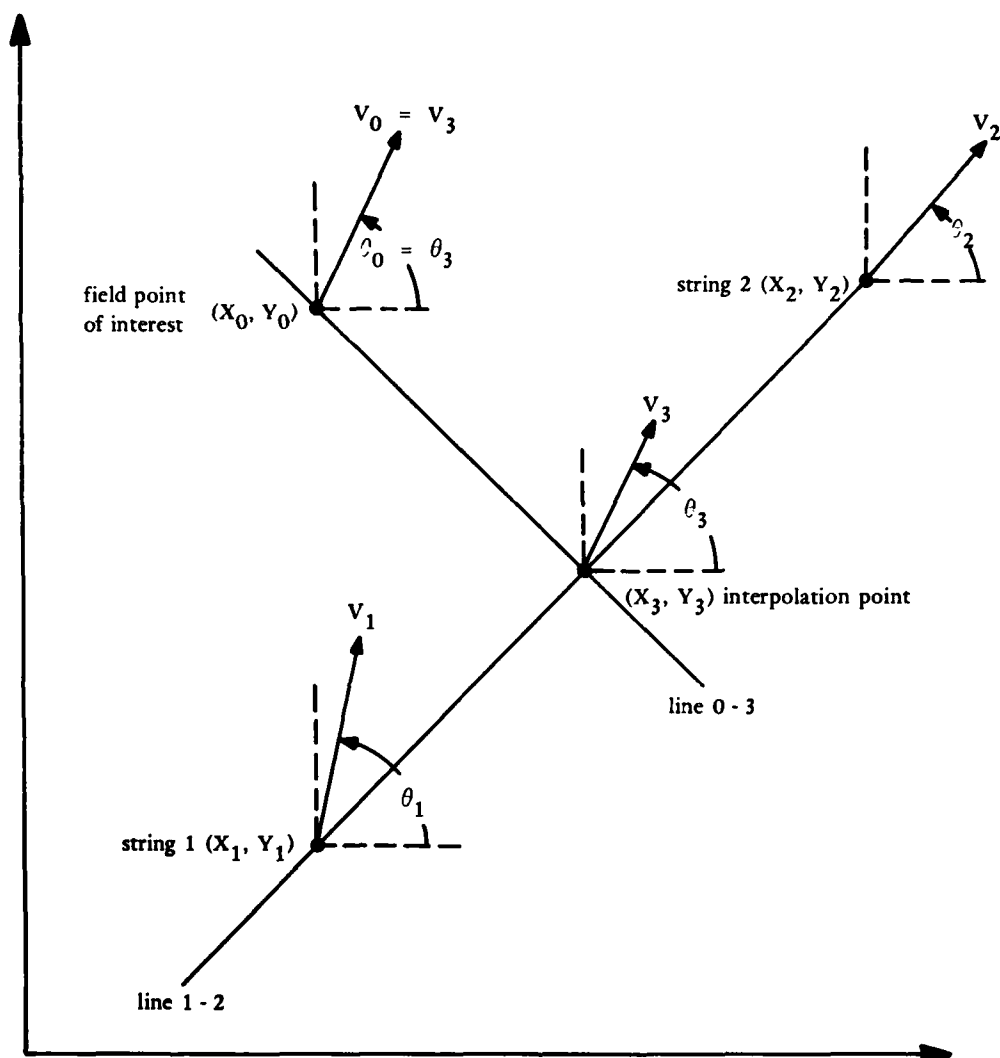
Current Field - Input Option 3

The current field input option 3 employs a linear interpolation/extrapolation scheme on current (magnitude and direction) data to give velocity variation in horizontal planes. When this option is invoked the program expects current data from 2, 3 or 4 current meter strings. Up to 25 measurements of current data can be contained on each string. For each string the first data entry must be at a depth equal to or less than the lowest anchor. The depth dependent data on the various strings do not have to correspond one to the other. That is, if on one string current data are obtained at $Z_1, Z_2, Z_3, \dots, Z_n$, then on the other strings data can be collected at completely different depths. This current field input option has been designed to treat mildly varying current fields. It does not provide acceptable results for eddy currents or reverse shear flows. The interpolation/extrapolation scheme to obtain the velocity at an arbitrary point in the field works as follows:

Case of 2 Strings. The field point (X_o, Y_o, Z_o) is determined where the velocity is to be found. On the plane $Z=Z_o$ there are three points of interest. They are (X_o, Y_o, Z_o) , (X_1, Y_1, Z_o) and (X_2, Y_2, Z_o) where the last two points denote the location on the plane $Z=Z_o$ at the meter strings. At each of these locations current magnitude and direction data are determined by a straight line interpolation of the data values given directly above and below the Z_o elevation. Figure 6 illustrates the situation after this linear interpolation. There, (V_1, θ_1) and (V_2, θ_2) are obtained from the vertical interpolation just mentioned.

A line normal to the line connecting (X_1, Y_1) and (X_2, Y_2) through the field point (X_o, Y_o) is constructed to locate the interpolation point (X_3, Y_3) . The point (X_3, Y_3) lies on the line joining (X_1, Y_1) and (X_2, Y_2) . Linear interpolations are now performed to find V_3 and θ_3 from the corresponding values at (X_1, Y_1) and (X_2, Y_2) . The current (V_3, θ_3) are assumed to prevail at all points along the normal line. Hence, (V_3, θ_3) provide the description of the current at the field point (X_o, Y_o) .

Case of 3 Strings. Suppose the field point is (X_o, Y_o, Z_o) . The current magnitude and direction are determined by linear vertical interpolation at the three string locations (X_1, Y_1, Z_o) , (X_2, Y_2, Z_o) and (X_3, Y_3, Z_o) . The corresponding velocity data obtained at these locations are (V_1, θ_1) , (V_2, θ_2) and (V_3, θ_3) . At the string location on the horizontal plane $(Z=Z_o)$ V_1, V_2 and V_3 are amplitudes through which a velocity plane can be passed. (A unique plane can be passed through any three non-collinear points.) The velocity V_o at the field point (X_o, Y_o, Z_o) then can be obtained by determining the amplitude on the velocity plane corresponding to the position (X_o, Y_o, Z_o) . The procedure is exactly the same for the determination of the current direction θ_o . For this quantity a direction plane has to be established using the direction amplitudes θ_1, θ_2 and θ_3 .



Line 0 - 3 is orthogonal to line 1 - 2. The velocities (V_1, θ_1) and (V_2, θ_2) are obtained by linearly interpolating string 1 and string 2 data, respectively. The velocity of any point along line 1 - 2 can be obtained by linear interpolation/extrapolation of the velocities (V_1, θ_1) , (V_2, θ_2) . The assumption is made that the velocity (V_3, θ_3) of an arbitrary point (X_3, Y_3) on line 1 - 2 is propagated along the orthogonal trajectory to that line at that point.

Figure 6. Interpolation/extrapolation in the case of 2-string data.

Case of 4 Strings. The field point is (X_0, Y_0, Z_0) . The string points are (X_1, Y_1, Z_1) , (X_2, Y_2, Z_2) , (X_3, Y_3, Z_3) and (X_4, Y_4, Z_4) . Through any three of the string points the procedure used in the preceding case can be repeated exactly. There are four independent ways that three points can be selected from four points, namely: (1, 2, 3); (1, 3, 4); (1, 2, 4); (2, 3, 4). The current is determined at the field point by averaging the results obtained by applying the case of three strings four times to the four combinations of points just indicated.

TANGENTIAL DRAG

The tangential drag computation on the cable is straightforward and is based on the expression

$$\Delta F_{TD} \begin{pmatrix} X \\ Y \\ Z \end{pmatrix} = \frac{1}{2} \rho [\pi D(1+\epsilon)] C_{DT} V_{TM} V_T \begin{pmatrix} X \\ Y \\ Z \end{pmatrix}$$

where $\Delta F_{TD} \begin{pmatrix} X \\ Y \\ Z \end{pmatrix}$ = tangential drag force component
per unit length in the direction X, Y or Z

$V_T \begin{pmatrix} X \\ Y \\ Z \end{pmatrix}$ = tangential velocity component along X, Y or Z
axis

V_{TM} = $\sqrt{V_T^2(X) + V_T^2(Y) + V_T^2(Z)}$, magnitude of
tangential velocity

C_{DT} = tangential drag coefficient

ρ = density of fluid

D = cable diameter

ϵ = strain developed by cable tension

The above calculation forms a part of the hydrodynamic cable drag force. The hydrodynamic force is comprised of a normal drag and a tangential drag.

CABLE DEVICES

In FUNCTION EFORCE (I, M, N) the tangential drag contribution to in-line devices is included in the drag calculation. It is required therefore to supply a tangential drag coefficient for each in-line device as input.

For in-line cable devices the weight of the cable and the hydrodynamic drag over a portion of the cable covered by an in-line device is deleted. Cable devices are referred to as in-line or free devices (two types). All cable devices are numbered automatically within the program. The numbering is accomplished sequentially with respect to cable number

and location of the device away from its $s=0$ end. That is, if on cable 1 there are three cable devices located at $s=s_1$, $s=s_2$, and $s=s_3$ with a $s_3 > s_2 > s_1$, then cable device indices 1, 2, 3 refer to devices located on cable 1 at $s=s_1, s_2, s_3$, respectively.

REFERENCE CONFIGURATION

An option exists to specify a particular parametric study case as a new no current reference configuration. Displacements with respect to the new no current reference configuration as well as the displacement from the original no current reference configuration are part of the output.

ITERATION CONTROL AND EXECUTION ERROR MESSAGES

To protect the user from excessively high execution costs coupled with the risk of not receiving any output, iteration limits have been added to DECEL1. Two separate iteration processes are involved: one attempts to satisfy the displacement constraints, where the cuts are made, imposed by the COMP card; where the other determines the structure's shape. Both iteration processes have been observed on rare occasions to converge very slowly, if at all.

The first iteration process deals with the imaginary reactions. The associated displacement errors have been observed to be large and to change slowly in some slowly convergent problems. An arbitrary definition of slow convergence coupled with a maximum iteration limit is used to terminate execution of a particular parametric case. Slow convergence has been defined to occur when, after half of the iteration limit is achieved, the displacement error is large (100 times the COMP value) and the error is changing by less than the COMP value per iteration. Iteration is terminated due to slow convergence with the message: SLOW CONVERGENCE AFTER XXX ITERATIONS. The previous and present displacement error values are printed to aid in determining how closely the solution has converged. If only one of the slow convergence criteria is satisfied iteration will continue until convergence occurs or the iteration limit is reached. Iteration is terminated due to reaching the iteration limit with the message: NO CONVERGENCE IN XXX ITERATIONS and the present and previous displacement error values are printed.

The second iteration process to determine the structure's shape occurs after the imaginary reaction iteration has been successful. This process has been observed on some occasions to oscillate about the correct solution. The normal iteration process is allowed to continue until half of the nodal position iteration limit is reached. At this point, the solution is arbitrarily assumed to be oscillating and a half-step iteration scheme is imposed (the iteration process is unchanged except that each node is allowed to move only half as far as calculated). This half-step technique continues until the iteration limit is reached or convergence occurs. Execution of the parametric case is terminated with the message: PROGRAM DID NOT CONVERGE AFTER XXX ITERATIONS, PARAMETRIC CASE TERMINATED. The displacement error is printed and the full output for the case is printed preceded by the message: APPROXIMATE RESULTS PRINTED. The user must judge if an adequate displacement error has been achieved for the results to be meaningful.

What To Do If . . .

When execution has been terminated by reaching the imaginary reaction iteration limit, several options are still available. The iteration limit (field 4 of the COMP card) can be increased; however, this probably will have to be done in conjunction with an increase in the COMP value. The COMP value should still be kept in a range that will be judged to produce usable results. The error values printed upon execution termination will give an idea of how much the COMP value will have to be increased.

In some cases, the desired current is too strong to apply in one step; strong currents have caused the imaginary reaction iteration limit to be reached. To handle this and other sensitive cases, an option has been added to apply the current in increments (field 11 of the NDAT card). Using this option, the program iterates to a solution for the first current increment as if this were the total current to be applied. Then the current is incremented and the process is repeated. An option exists to print the solution for each increment of the current (see field 11 of the NDAT card). This technique has been highly effective in obtaining solutions in high currents up to 10 knots.

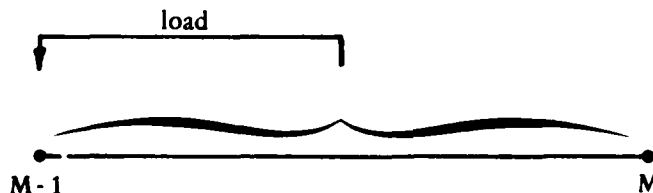
DECEL1 USER EXPERIENCE

In the course of using DECEL1 a wide variety of structures in various current profiles have been analyzed. Some results have been compared with experimental data with close agreement (Ref 7). Other cases have been cross-checked against other computer models again with good agreement. The program is easy to use to the point that a user with a general engineering background can use the manual to formulate the required input and expect to receive back usable results once obvious input errors are corrected. The ease of use is an exceptional attribute of the program.

In the course of making modifications to the program a great deal of insight has been gained regarding the mathematical modeling. Many of the details are of no importance to the user. However there are several characteristics that the user should be aware of; these deal with the internal distribution of loads, non-convergent problems, and the convergence parameter.

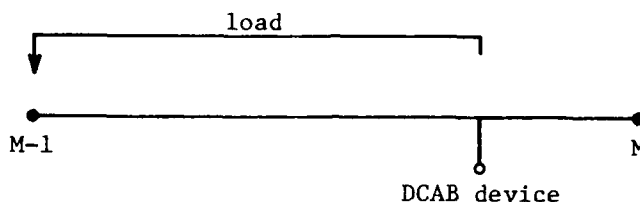
Load Distribution

Loads (weight and drag) are generated from three sources: cables, cable devices, and junction devices. Cable forces due to drag and weight are calculated for the cable length between two nodes [$\text{length} = (\text{total cable length})/(\text{no. of elements in the cable})$]. (See CAB card.) The forces are assigned to the M-1 node as shown below:



Clearly, the smaller the distance between the nodes, the more accurate the mathematical representation.

Loads due to devices on the cable (DCAB card) are modeled in a similar way except that the device is physically located at a specific point along the cable between the two nodes. The DCAB loads are modeled as shown below:



This is a good representation when the device is actually near node (M-1). However, when the device is near node M and the distance between the nodes is large, this may be a poor representation. This is not to say the computer results will be grossly in error; this depends upon the size and number of DCAB devices. If the devices are few and/or small such that the system is cable-load dominated, the results should be acceptable.

Probably the most serious error will arise when there are few elements and the DCAB devices produce large static or drag loads. In this case large loads may be assigned to locations quite distant from their actual point of application.

Loads due to DJNC devices are most accurately modeled. The loads are assigned exactly where the device is located.

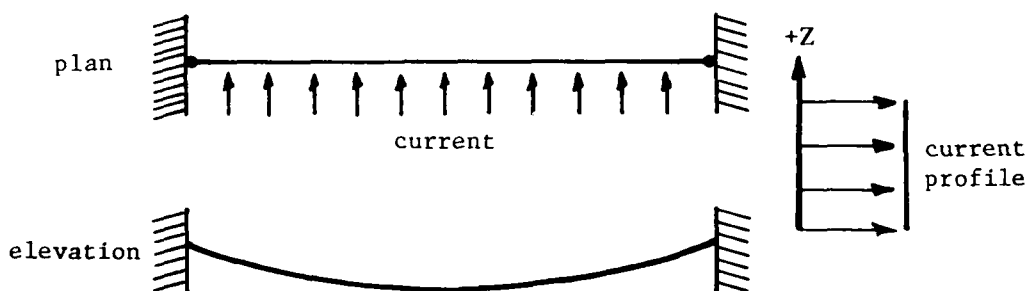
It may appear that a better modeling of cable and DCAB loads could be achieved by proportioning the loads between the appropriate adjacent nodes. However, this single change is not consistent with other internal force accounting schemes. To implement force proportioning, a major re-write of the program would be required; this has not been done.

As the program stands, the majority of problems can be analyzed with wholly satisfactory results even ignoring the way loads are distributed. Where the load distribution scheme is judged by the user to pose a problem in obtaining a satisfactory model, the following suggestions are presented.

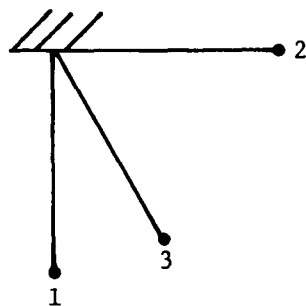
1. Model all cables with as many elements as possible (50). This will make the distance between nodes least so that DCAB loads will be assigned as close to the actual device location as possible.
2. Model large bodies as DJNC devices - loads will be assigned exactly where the device is located.
3. Model long cables as a series of shorter series-connected cables. This will aid in making elements short.

Non-Convergent Problems

DECEL1 treats statically determinate and statically indeterminate problems differently. The indeterminate problems are solved using the imaginary reaction technique (Ref 1). This is a powerful method and usually converges rapidly to a solution. (Reference 1 shows that the method is unconditionally convergent.) However, at least one case has been encountered where the method is at best very slowly convergent. The case involves a nearly neutrally buoyant cable hung in a catenary between two fixed points with a strong current acting perpendicular to the plane of the catenary:

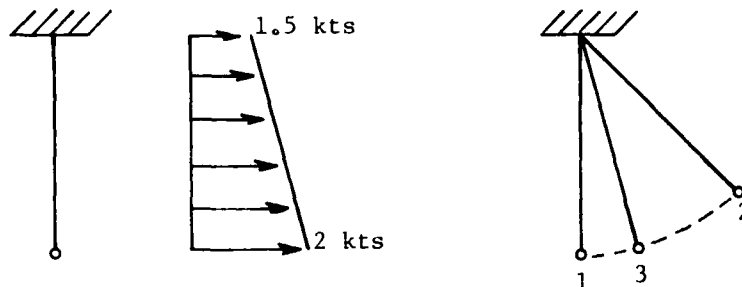


The positions attained by the cable during the iteration procedure are sketched below.



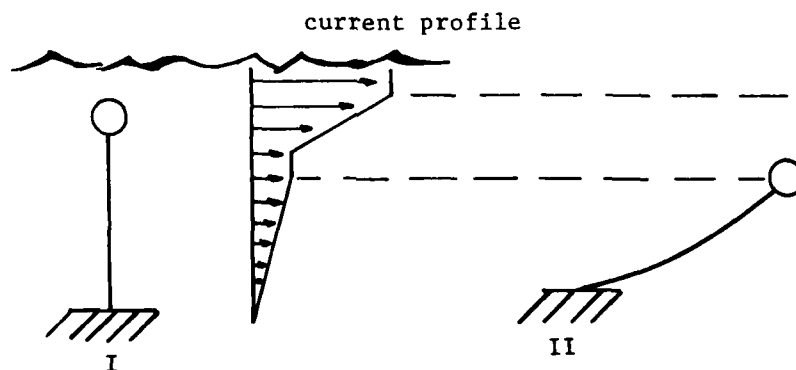
The cable is initially driven from the no-current position (1) to a nearly horizontal position (2). Here there is low- or no-normal drag to support the cable so in the next iteration it falls to position (3) (which may be coincident with position (1)). Internally, the iterations appear to oscillate between positions (2) and (3), and the solution fails to converge. Convergence can be achieved by reducing the current or by increasing the weight of the cable.

Statically determinate cases bypass the imaginary reaction routine, thus convergence is not as certain. There are combinations of current and geometry that interact in such a way as to appear to be unstable. An example is a lightweight anchor suspended from the surface in a current that increases with depth.



From the no-current position (1), the first iteration is to position (2) where the normal drag force is reduced both because of the orientation change (toward horizontal) and the reduced current in the new position. The reduced loading causes the system to attain position (3). The solution then oscillates between positions (2) and (3). Whether another case using this configuration will converge or not depends on both the magnitude of the current and the system weight. The particular case in question probably would converge in a more uniform current field or if the system weight were to be increased.

Another non-convergent case involved a sharp change in the velocity profile.



The subsurface buoy was initially in a high current zone (sketch I); in the first iteration it moved to a lower current region (sketch II). Here the high current was no longer acting on the system so on the next iteration the buoy was moved back into the high current regime. This case failed to converge primarily because the current shear was very near the initial depth of the buoy. Thus the buoy moved in and out of the high current on subsequent iterations. If the current shear had been much below the buoy and always acted only on the cable the solution most likely would have converged.

The above cases are presented simply to illustrate non-convergent problems. They by no means represent all non-convergent cases; however, they serve to illustrate what kinds of situations can be difficult to solve. If a user encounters a case that does not converge, the discussion of the examples here will help guide his reasoning in determining why non-convergence occurs.

In an attempt to improve the iteration technique, a half-step iteration technique has been introduced. The process is implemented only after 100 standard iterations have occurred. (The 100 iteration number has been relatively arbitrarily judged to be an indicator of oscillation during iteration.) After the first 100 iterations have occurred the next 100 iteration steps are calculated in the same way but the allowed displacement is reduced by one-half. This approach has not yet (as of this writing) been user tested; however, initial tests indicate that formerly oscillating cases will converge to a solution. As part of the half-step technique, an informative printout has been added that states the number of iterations required to achieve convergence. After 200 total iterations have occurred, iteration will be stopped, a message printed and the next parametric case will be analyzed. (The 200 iteration limit is arbitrarily taken as an indicator that the solution is not converging.)

Convergence Parameters

The variable on the COMP card is used as the convergence test parameter. The discussion of the COMP card defines a lower limit for the parameter that can be quite small. Iteration continues until two consecutive calculated positions for each node on the structure differ by less than the convergence parameter. Very small values of the convergence parameter can cause certain "sensitive" cases (such as some of those discussed above) to appear to oscillate. Adequate solutions and more rapid convergence can be obtained by picking a convergence parameter value that is consistent with the size of the structure being analyzed. The table below lists suggested convergence parameter values that are consistent with the structure size as determined by cable length.

<u>Cable Length (ft)</u>	<u>Convergence Parameter (ft)</u>
<10	<0.01
<100	0.01-0.1
<1000	0.1-1.0
<10,000	1.0-10.0
>10,000	5.0-20.0

These are only suggested values that may be used as initial values in order to insure that successful convergence does occur. For particular problems the user must judge for himself the adequacy of the convergence tolerance chosen. However, the user must realize that an unnecessarily small convergence parameter can cause a case to fail to converge mathematically even though a physically adequate solution has been reached in the iteration process.

INPUT CARDS

Input cards to DECEL1 contain a 4-digit integer (-999 to 9999) card number in columns 1-4, a 4-character card type identifier in columns 5-8, and descriptive properties of the array in the remaining fields with the exception of the following input cards.

- 1 - Main Descriptive Title Card
- 2 - Parametric Descriptive Title Card
- 3 - Continuation Card for CAB
- 4 - Velocity Field for Current Option 3

The card number has two uses. First, it is used as a convenience for the user to define the order of the cards in the deck, should the deck be dropped. Secondly, it is used as a cross-check in changing parameters in the Parametric Study Source Deck: when a parameter on a card is to be changed, both the card number and type must match the card in the Cable Array Source Deck or an error will occur. In the Cable Array Source Deck, duplicate card numbers are detected as errors; however, any number of input cards may have the card number omitted with no errors.

**** CABLE ARRAY SOURCE DECK CARDS ****

LUN CARD (optional card; if used it must be the first card in the deck)

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	^LUN	Right adjust
3	9-16	I8	Unit number of card reader	
4	17-24	I8	Unit number of line printer	
5	25-32	I8	Unit number of temporary storage tape	
6	33-40	I8	Input option (0 or 1)	See notes
7	41-48	I8	Blank if input option = 0. Unit number of source tape if input option = 1.	
8	49-56	I8	Output option (0, 1 or 2)	See notes
9	57-64	I8	Blank if output option = 0. Unit number of output tape or card punch if output option = 1 or 2.	
10	65-72		Not used	See notes
11	73-77		Not used	
12	78-80		Not used	

- NOTES: 1. The carot symbol (^) is used to indicate one blank column in the position shown.
2. The LUN card is used to transmit the logical unit numbers of the I/O devices and the I/O options. The LUN card is optional. If it is omitted then input option 0 and output option 0 are the default options.

Two input options are available:

- 0 - The physical characteristics of the array are to be read from the cable array source deck (see CABLE ARRAY SOURCE DECK)
- 1 - The physical characteristics of the array are to be read from the cable array source tape (see CABLE ARRAY SOURCE TAPE)

Three output options are available:

- 0 - A structural output to the line printer (see
STRUCTURAL OUTPUT)
- 1 - A device location output to tape or cards (see
DEVICE LOCATION OUTPUT)
- 3 - both of the above

MAIN DESCRIPTIVE TITLE CARD

Field	Columns	Format	Contents	Comments
1-10	1-80	8A10	Main descriptive title	See notes

NOTE: A single "Main Descriptive Title Card" must always follow the LUN card. If no title is desired a blank card must be inserted. This card does not adhere to the convention requiring a card number and card type, so that the entire card can be utilized for a title. If the LUN card is omitted then this must be the first input card.

NJNC CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	NJNC	
3	9-16	I8	Number of junctions in original (unreduced) array	2-44
4	17-24		Not used	
5	25-32		Not used	
6	33-40		Not used	
7	41-48		Not used	
8	49-56		Not used	
9	57-64		Not used	
10	65-72		Not used	
11	73-77		Not used	
12	78-80		Not used	

NOTE: The NJNC card is used to transmit the number of junctions in the original (unreduced array).

ANC CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	^ANC	Right adjust
3	9-16	I8	Junction number of anchor	1-44
4	17-24	F8.0	X coordinate of anchor	ft
5	25-32	F8.0	Y coordinate of anchor	ft
6	33-40	F8.0	Z coordinate of anchor	ft
7	41-48		Not used	
8	49-56		Not used	
9	57-64		Not used	
10	65-72		Not used	
11	73-77		Not used	
12	78-80		Not used	

NOTE: The ANC cards are used to transmit the data in Table 1.
There must be one ANC card for each anchor in the array.

IR CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	^^IR	Right adjust
3	9-16	I8	Junction number assigned to a cut in the reduced array	1-44
4	17-24	I8	Junction number at which cut is made in the original array	1-44
5	25-32		Not used	
6	33-40		Not used	
7	41-48		Not used	
8	49-56		Not used	
9	57-64		Not used	
10	65-72		Not used	
11	73-77		Not used	
12	78-80		Not used	

NOTE: The IR cards are used to transmit the information contained in the table below the left-hand schematic of each of Figures 3a-3d. There must be one IR card for each cut made in going from the original to the reduced array.

CAB CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	^CAB	Right adjust
3	9-16	I8	Cable number	1-22
4	17-24	I8	s=0 junction number	1-44
5	25-32	I8	s=L junction number (after required cuts are made)	1-44
6	33-40	F8.0	Cable weight per length in surrounding fluid; + if positively buoyant, - if nega- tively buoyant	lb/ft
7	41-48	F8.0	Normal drag coefficient of cable	
8	49-56	F8.0	Cable diameter	in.
9	57-64	F8.0	Total cable length (unstressed)	ft
10	65-72	F8.0	Cable rigidity, C (see notes) if k=1, C=EA	lb
11	73-77	F5.0	Exponent in constitu- tive relation, k (see notes)	≥ 0
12	78-80	I3	Number of straight ele- ments by which cable is to be represented	$>0, \leq 50$

NOTE: The CAB cards are used to transmit the information contained in the table below the right-hand schematic in Figures 3a-3d (fields 3 to 5), the physical characteristics of the cables in the array (fields 6 to 11), and the fineness by which the cables in the array are to be modeled (field 12). There must be one CAB card and one continuation CAB card for each cable in the array. The constitutive relation for a cable can, in general, be written (6) as $\epsilon = (T/C)^k$ where ϵ is the

NOTES FOR CAB CARD (continued)

strain and T the tension. C and k are constants which depend on the cable material and construction. Fields 10 and 11 transmit the values of C and k , respectively. An inextensible cable is transmitted to DECEL1 by leaving fields 10 and 11 blank.

CONTINUATION CAB CARD

Field	Columns	Format	Contents	Comments
1	1-8	F8.0	Tangential drag coefficient of cable	See notes
2	9-80	9F8.0	Not used	

NOTE: Each CAB card must be followed by an additional card. If no tangential drag is desired a blank card must be inserted. This card does not adhere to the convention requiring a card number and card type since it is in fact a continuation of the tangential drag coefficient. Default value is zero.

DCAB CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	DCAB	
3	9-16	I8	Number of cable to which device is attached	1-22
4	17-24	I8	Device type (1,2)	See notes
5	25-32	I8	Print flag for cable devices. If flag = 0, print device characteristics and location. If flag \neq 0, don't print.	
6	33-40	F8.0	Device weight in surrounding fluid; + if positively buoyant, - if negatively buoyant	lb (See note 3)
7	41-48	F8.0	Normal drag coefficient	
8	49-56	F8.0	Diameter on which drag coefficient is based (Type 1) Frontal area on which drag coefficient is based (Type 2).	in. ft ²
9	57-64	F8.0	Device length (Type 1)	ft
10	65-72	F8.0	Unstressed distance of device from s=0 junction of the cable	ft
11	73-77	F5.0	Tangential drag coefficient	
12	78-80		Not used	

NOTE: 1. The DCAB cards are used to transmit the physical characteristics of the discrete devices (buoyancy elements, current meters, etc.) attached to the cables in the array. There must be one DCAB card for each such device

NOTES FOR DCAB CARD (continued)

in the array. Two types of devices are permitted: (a) in-line (Type 1) any elongated device (cylinder, ellipse, etc.) attached so that its longitudinal axis is aligned with the cable axis; and (b) free devices (Type 2).

2. Dummy DCAB devices with no weight and zero drag can be used as conveniences to print the location of the device in the cable array's deformed state. With no DCAB devices, no information about the cable shape between junctions is printed.
3. Include cable weight in water if device covers segment of cable.

Each device is automatically assigned a unique number based on its location on the structure. Low numbered devices are located on low numbered cables. On each cable the lowest number device is nearest the $s=0$ end of the cable.

DJNC CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	DJNC	
3	9-16	I8	Number of junction to which device is attached	1-44
4	17-24	I8	Not used	
5	25-32	I8	Not used	
6	33-40	F8.0	Device weight in surrounding fluid; + if positively buoyant, - if negatively buoyant	lb
7	41-48	F8.0	Device drag coefficient	
8	49-56	F8.0	Frontal area on which drag coefficient is based	ft ²
9	57-64		Not used	
10	65-72		Not used	
11	73-77		Not used	
12	78-80		Not used	

NOTE: The DJNC cards are used to transmit the physical characteristics of the discrete devices attached to the junctions in the array. There must be one DJNC card for each such device in the array.

Since an in-line device cannot physically exist at a junction (cable termination), only free devices are permitted at a junction.

DJNC devices are indexed automatically for counting purposes only; they are counted in the total number of indexed devices.

DEN CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	ADEN	Right adjust
3	9-16	F8.0	Density of fluid in which array is suspended	$\text{lb s}^2 \text{ft}^{-4}$ (1.99 for seawater)
4	17-24		Not used	
5	25-32		Not used	
6	33-40		Not used	
7	41-48		Not used	
8	49-56		Not used	
9	57-64		Not used	
10	65-72		Not used	
11	73-77		Not used	
12	78-80		Not used	

NOTE: The DEN card is used to transmit the density of the fluid in which the array is suspended.

EOD CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	^EOD	Right adjust
3	9-16		Not used	
4	17-24		Not used	
5	25-32		Not used	
6	33-40		Not used	
7	41-48		Not used	
8	49-56		Not used	
9	57-64		Not used	
10	65-72		Not used	
11	73-77		Not used	
12	78-80		Not used	

NOTE: The EOD card is used to specify the end of data transmission.

**** PARAMETRIC STUDY SOURCE DECK CARDS ****

NDAT CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	NDAT	
3	9-16	I8	Current field option	See note 1
4	17-24	I8	Number of stations at which current data is taken for current field option 3. Otherwise not used.	See note 2
5	25-32	I8	Option for defining a particular parametric study as the new no current reference configuration. Option = 0, no new ref. config. Option \neq 0, new ref. config.	
6	33-40	F8.0	PHI	degrees See note 3
7	41-48	F8.0	Device location punch output option; option \neq 0, punch device locations on cards	See note 4
8	49-56	F8.0	Weight of device whose location is to be punched	lb
9	57-64		Not used	
10	65-72	F8.0	Velocity units input option	See note 5
11	73-77	F5.0	Number of steps used to apply full current	See notes 6 and 7 (default value = 1.0)
12	78-80		Not used	

SEE NEXT PAGE FOR NOTES

NOTE:

1. The NDAT card is used to specify that new, modified, or additional data follow and to transmit the current field option. Three current field options are available.
 - 0 - No current.
 - 1 - Current field is unidirectional and horizontal. (There is no vertical component.) The current magnitude can vary with depth. At any point in the plane Z-constant, the velocity is invariant. The no-current configuration is also calculated as part of this option.
 - 2 - Same as current field option 1 except that the current can have a directionality that depends on depth. That is, this option relaxes the unidirectional constraint on the velocity field. At any point in the plane Z-constant, the velocity is invariant. An example of a possible current candidate requiring this option would be a helical current where the axis of the helix is aligned with gravity. The no-current configuration is also calculated as part of this option.
 - 3 - Interpolation/extrapolation scheme for field current (magnitude and direction) data. The current is assumed to have no vertical component. Two, three, or four stations can be selected in the horizontal plane and at each of these stations, current (direction and magnitude) data can be obtained at up to 25 elevations. This option affords current variation in horizontal planes. The no-current configuration is also calculated as part of this option.
2. For current option 3, the value in field 4 on the NDAT card must appear on all successive NDAT cards even if the velocity field is not to be varied in any of the parametric studies.
3. The angle ϕ specifies the rotation of the X-axis from the N-axis. ϕ is measured positive in the clockwise sense and the N-axis is $\phi=0$. That is, when $\phi=0$ then the (N,W) coordinate system is coincident with the (X,Y) coordinate system (see Figure 4). The ϕ value should appear on each NDAT card.
4. It is sometimes desirable to have the locations of particular devices punched on cards for input to other programs. For example, both hydrophones and buoys may be distributed as DCAB devices along the structure, but only the location of the hydrophones is important. By specifying field 7 \neq 0 and field 8 = hydrophone weight, DECEL1 will punch for each hydrophone: (a) device index, (b) cable number, (c) distance from the s = 0 end of the cable, and (d) x,y,z coordinates of the device. Preceding this punched output is a card totalling the number of cards in the punched output.

NOTES FOR NDAT CARD (continued)

5. Velocity units input option:

- 0 - input magnitude of velocity in knots (default)
- 1 - input magnitude of velocity in cm/sec
- 2 - input magnitude of velocity in ft/sec

6. This is a coded value: the integer portion represents the number of steps used to apply the full current; the fractional part controls printed output: a non-zero fractional part (i.e., 10.1) causes the shape calculated for each increment of the current to be printed. For example: the value 10.1 will cause the current to be applied in ten equal increments and the structure shape will be printed for each increment. A 10.0 value will apply the current in ten increments but print only the shape with the full current value applied. If plotting is requested, only the shape with the full current applied is plotted.
7. This input option is intended to aid in obtaining solutions where high currents cause SLOW/NO CONVERGENCE messages to be printed.

PARAMETRIC DESCRIPTIVE TITLE CARD

Field	Columns	Format	Contents	Comments
1-10	1-80	8A10	Parametric descriptive title	See notes

NOTE: Descriptive Title Card must always follow an NDAT card. If no title is desired, then a blank card must be inserted. This card does not adhere to the convention requiring a card number and card type, so that the entire card can be utilized for a title.

COMP CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	COMP	
3	9-16	F8.0	Accuracy required in array equilibrium calculations (COMP value)	ft (0.01 typ)
4	17-24	F8.0	Nodal position iteration limit	See note 2 (200 default value)
5	25-32	F8.0	Imaginary reaction iteration limit	See note 2 (1000 default value)
6	33-40		Not used	
7	41-48		Not used	
8	49-56		Not used	
9	57-64		Not used	
10	65-72		Not used	
11	73-77		Not used	
12	78-80		Not used	

NOTES:

1. The COMP card is used to transmit the accuracy requirement imposed on the array equilibrium calculations. This accuracy requirement, specified in field 3, insures that the calculated coordinates of every point in the array are within \pm field 3 of their exact values.

The accuracy obtainable is limited by the significant figure capacity of the computer being used and by the largest linear dimension in the array. Let the number of significant figures carried in single precision be n , and let the characteristic of the common logarithm of the largest linear dimension be m . Then, the value of field 3 is usually bounded by field 3 $\geq 10^{m-n+3}$. (For example, suppose $n = 8$ and the largest dimension is 25,000 ft. Then, field 3 ≥ 0.1 ft.) Occasionally, a larger minimum value must be used. A

NOTES FOR COMP CARD (continued)

COMP card must appear after the first NDAT card. See PARAMETRIC STUDY SOURCE DECKS. Accuracy requirements can be changed in subsequent Parametric Study Decks by using new COMP cards.

2. See the descriptions in the text on pages 18 and 19.

VEL CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	VEL	Right adjust
3	9-16	F8.0	Z coordinate at which current velocity is specified	ft
4	17-24	F8.0	Magnitude of current at Z coordinate specified in field 3	knots; cm/sec; ft/sec (consistent with NDAT card)
5	25-32	F8.0	Direction of current at Z coordinate (current option 2 only)	degrees
6	33-40		Not used	
7	41-48		Not used	
8	49-56		Not used	
9	56-64		Not used	
10	65-72		Not used	
11	73-77		Not used	
12	78-80		Not used	

NOTE: The VEL cards are used to transmit the data in Table 2. There must be one VEL card for each value of Z at which the current velocity is specified.

Up to 25 VEL cards are permitted. At least one of the Z coordinates transmitted by the VEL cards must be less than or equal to the minimum Z coordinate transmitted by the ANC cards. For further information see CURRENT FIELD INPUT OPTION 1.

The VEL cards must not appear after an NDAT card specifying a current field option = 0. All VEL cards required to transmit the current profile must appear after the first NDAT card specifying a current field option = 1. See PARAMETRIC STUDY SOURCE DECKS.

A given current profile will be applied in all subsequent parametric cases until a new field is defined.

NOTES FROM VEL CARD (continued)

Current Option 1 - Only the magnitude of the current is input (field 4). The direction is varied by the ANG card.

Current Option 2 - Both magnitude and direction of current are input fields 4 and 5, respectively. The direction of the field also may be modified by the ANG card. Current direction is to be specified from the magnetic north axis. Clockwise rotation is positive.

Current Option 3 - Fields 3, 4 and 5 are ignored. The velocity information is read from the velocity continuation group immediately following the VEL card.

The following is a brief description of the velocity cards under current option 3.

After a VEL card is encountered there will be 2, 3 or 4 sets of velocity data depending on the number of stations at which velocity profiles were measured.

Each set of data for a station will contain one Station Location Card and N Velocity Definition Cards. N is the number of Z-coordinates at which velocity is measured for the particular station. The maximum value of N is 25.

The 2, 3 or 4 sets of data are stacked as indicated in Figure 7.

The Station Location Cards and Velocity Definition Cards are defined on the next two pages.

To further clarify the velocity option 3 data requirements we present another example using 3 stations of current data. The data deck will be arranged as follows:

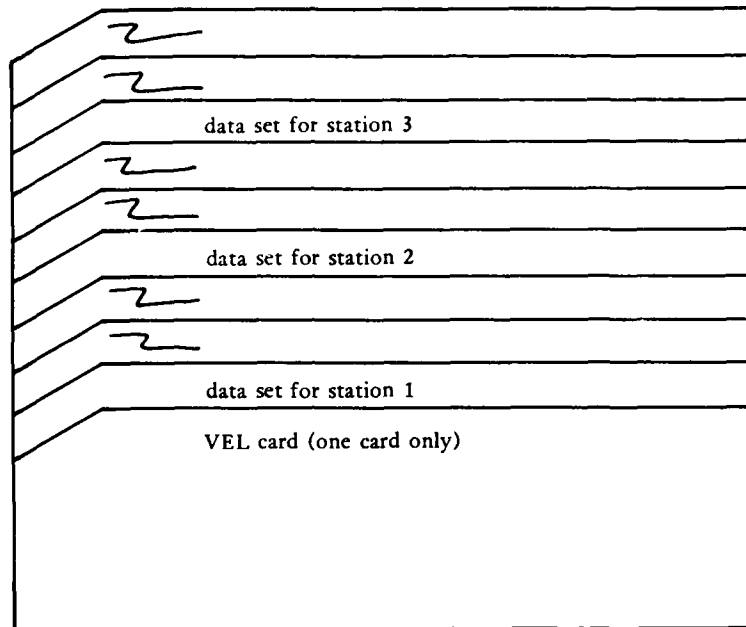


Figure 7. Arrangement of data sets for velocity option 3.

NOTES FROM VEL CARD (OPTION 3 ONLY) (continued)

Field	Columns	Format	Contents	Comments
1	1-5	I5	Station number at which velocity profile measured	
2	6-10	I5	Number of Z-coordinates at which velocity is measured for this station (field 1)	
3	11-20	F10.0	North coordinate of this station*	ft (see notes)
4	21-30	F10.0	West coordinate of this station**	ft (see notes)
5	31-80		Not used	

*Coordinate is positive for north, negative for south.

**Coordinate is positive for west, negative for east.

NOTES FROM VEL CARD (OPTION 3 ONLY) (continued)

Field	Columns	Format	Contents	Comments
1	1-5	I5	Station number	
2	6-10		Not used	
3	11-20	F10.0	Z-coordinate of velocity	ft
4	21-30	F10.0	Magnitude of velocity at Z-coordinate of this station (field 1)*	See notes
5	31-40	F10.0	Direction of current at Z-coordinate of this station (field 1)**	degrees (see notes)
6	41-80		Not used	

NOTE: There must be as many of this card as there are current readings at the station (= field 2 of preceding card).

*The magnitude of velocity may be input in three different units according to the option definition on the NDAT card.

Units Option 0 - knots (default)

Units Option 1 - cm/sec

Units Option 2 - ft/sec (see NDAT card)

**The direction of current is positive in the clockwise sense from the magnetic north axis (degrees).

ANG CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	^ANG	Right adjust
3	9-16	F8.0	Initial current angle	degrees
4	17-24	F8.0	Increment in current angle	deg, > 0
5	25-32	F8.0	Final current angle	deg, ≥ field 3
6	33-40		Not used	
7	41-43		Not used	
8	49-56		Not used	
9	57-64		Not used	
10	65-72		Not used	
11	73-77		Not used	
12	78-80		Not used	

NOTE: The ANG card is used to transmit instructions for changing the angular direction of the current with respect to the N-axis for current options 1 and 2 only. DECEL1 calculates the array response to the specified current profile from the initial to the final current angles in increments transmitted by field 4. An ANG card must not appear after an NDAT card specifying a current field option = 0. One ANG card must appear after the first NDAT card specifying a current field option = 1, 2, or 3. See PARAMETRIC STUDY SOURCE DECKS.

If no parametric range of current direction variation is required, then Fields 3 and 5 should have identical values and field 4 should have a non-zero positive value.

When exercising the angular rotation option, it is important to recognize the difference between current options 1 and 2. For current option 1, the input value in field 3 of the ANG card establishes the directionality of the entire flow field. This is not the case for current option 2 since current directionality is established and specified as input on the VEL card.

NOTES FROM ANG CARD (continued)

For current option 2 the field 3 input value on the ANG card should be set equal to ϕ (the angle between the N- and X-axes) plus the initial angle of interest. The value in field 5 of the ANG card should be set equal to $\phi + \beta$ where β is the total angle through which the current is to be rotated. The value of field 4 is $\Delta\beta$, the increment. When current option 2 is selected and no rotation of the current field is desired, the fields 3 and 5 should be set equal to ϕ and any positive value set in field 4.

PPLT CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	PPLT	
3	9-16	F8.0	Plotting option: 0 - Undeformed only 1 - Deformed only 2 - Both	Undeformed plotted as a dotted line. Deformed plotted as a solid line.
4	17-24	F8.0	Height of plot, y	in. (default 10)
5	25-32	F8.0	View angle, x (see note)	degrees (default 30)
6	33-40	F8.0	View angle, y (see note)	degrees (default 120)
7	41-48	F8.0	View angle, z (see note)	degrees (default 90)

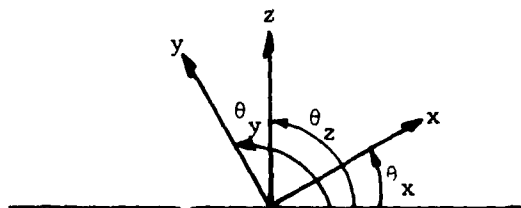
NOTE: For a plan or elevation view (not a perspective view) one view angle must be 361°. This is a code indicating which axis is perpendicular to the plot. For example, a plan view is specified by:

View Angle, x = 0.001 (0 gives the 30° default value)

View Angle, y = 90°

View Angle, z = 361°

The x, y and z view angles are shown below for the default configuration.



θ_x - View angle for x axis. 30 degrees.

θ_y - View angle for y axis. 120 degrees.

θ_z - View angle for z axis. 90 degrees.

Examples perspective plots are shown in Figures 8-10.

CPLT CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	CPLT	
3	9-16	F8.0	ZUP-Max. depth plane level	ft
4	17-24	F8.0	ZDN-Min. depth plane level	ft
5	25-32	F8.0	DZ -Delta depth	ft
6	33-40	F8.0	YIN-Height in Y direction of a single plane	in.
7	41-48	F8.0	XMIN	ft (If blank default values selected)
8	49-56	F8.0	XMAX	
9	57-64	F8.0	YMIN	
10	65-72	F8.0	YMAX	
				Minimum & maximum coord. of area to be covered by plot
11	73-77	F5.0	ANG-View angle Y	degrees default = 90
12	78-80	I3	NY -Number of mesh points in Y direction, including boundary	default = 6

NOTE: Current plots may be depicted at one or more depths by varying input parameters ZUP, ZDN, DZ. The vertical height for each plane of the plot is input as YIN, and the corresponding width is calculated by the program. The product of the number of planes and the vertical height of a single plane cannot exceed 10 inches.

The plots may vary in perspective view angle y over the range $0 < \text{ANG} < 180^\circ$, where $\text{ANG} = 90^\circ$ is the plan view. For purposes of plotting the current field, each plane is assumed to have z coordinate zero and view angle x equal to zero.

NOTES FROM CPLT CARD (continued)

The mesh for plotting current is controlled by input NY. NY is the number of mesh points in the y direction, for a plane, including the boundary. The corresponding number of mesh points, for the x direction, is calculated by the program. ($NY = 2 + \text{number of current arrows encountered when moving from YMIN to YMAX.}$)

The area covered by the current field plot may be selected in two ways. If the values XMIN, XMAX, YMIN, YMAX are left blank, the program determines the area to be plotted. The area is based on the maximum and minimum anchor point coordinates. The second method is to define XMIN, XMAX, YMIN, YMAX in terms of the x, y coordinate system. If there is only one anchor point XMIN, XMAX, YMIN, YMAX must be defined by the user. A star will be plotted at each anchor point within the defined area.

Examples of current field plots are shown in Figures 11 and 12.

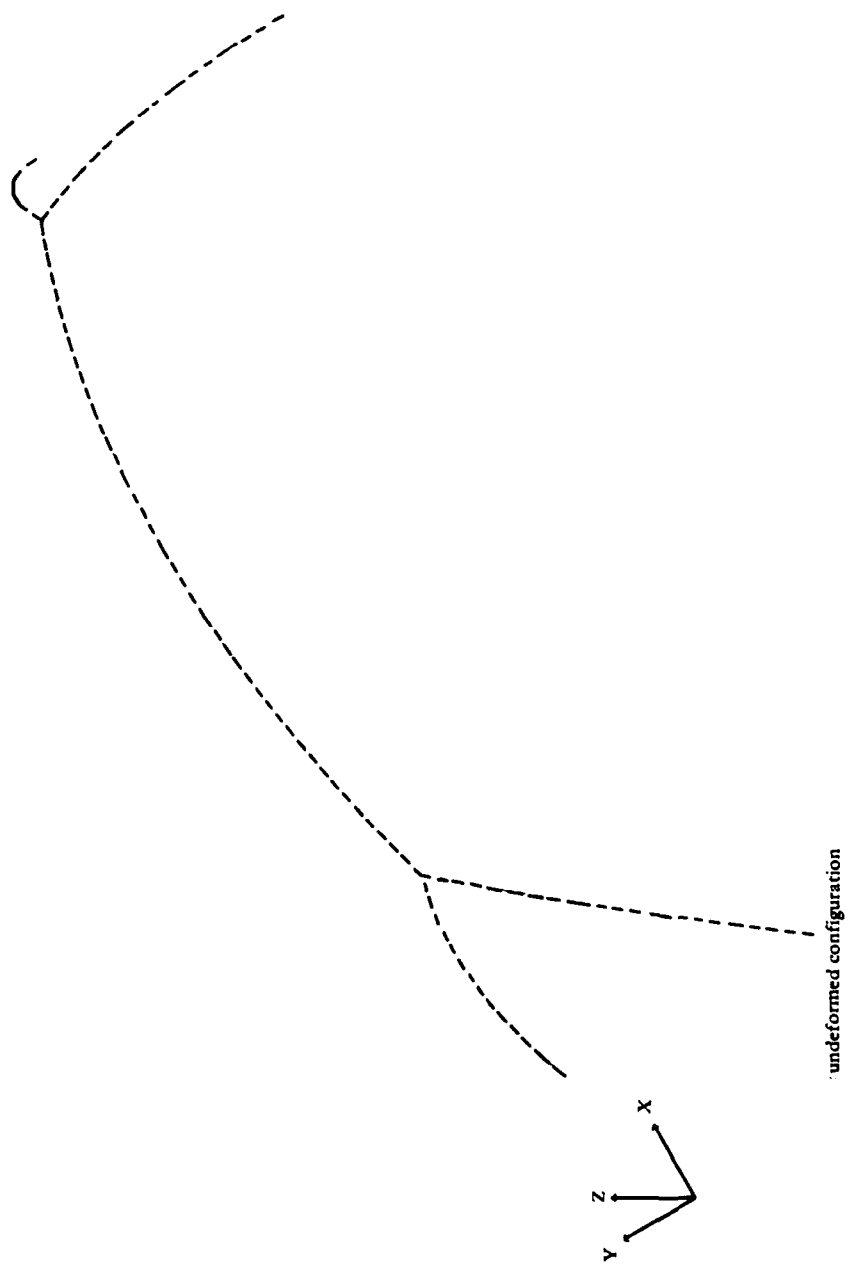


Figure 8. Perspective view of the undeformed structure (field 3 = 0).

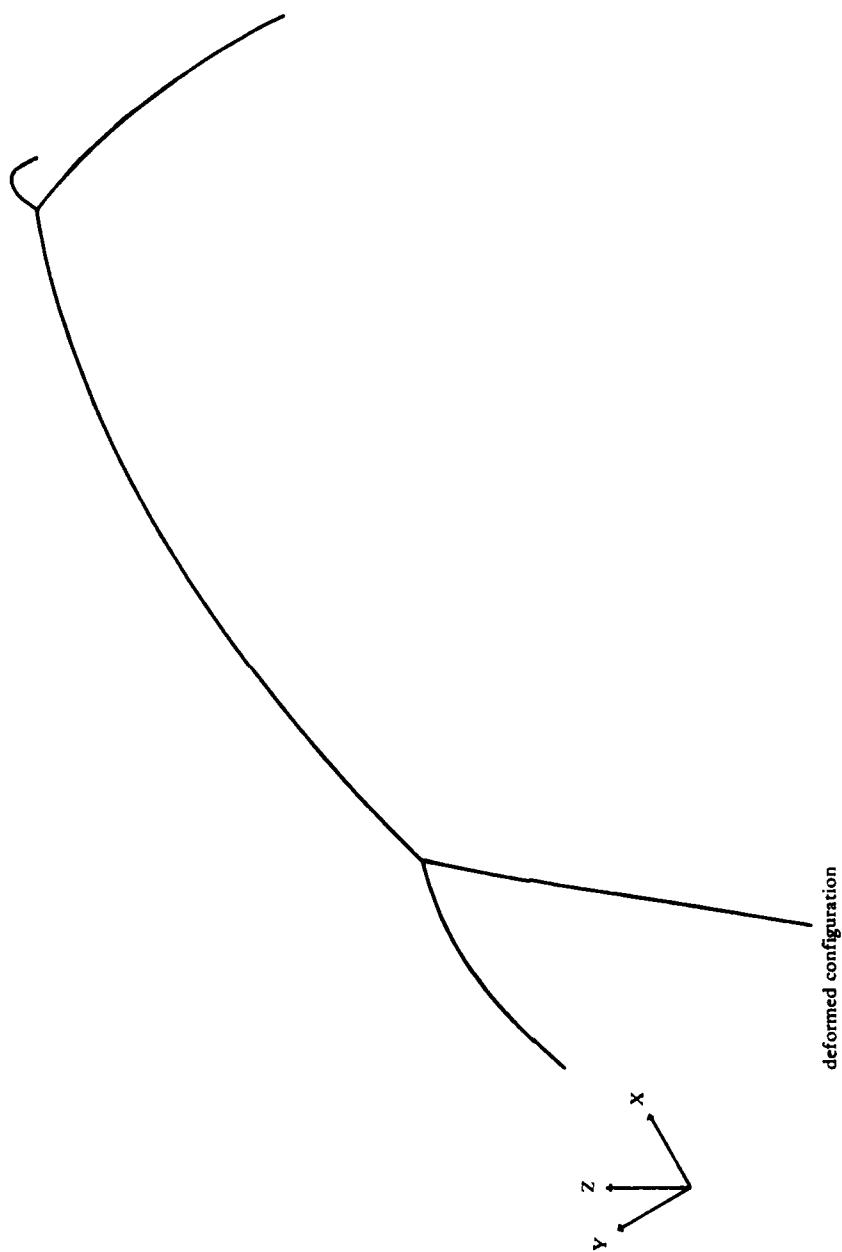


Figure 9. Perspective view of the deformed structure (field 3 = 1).

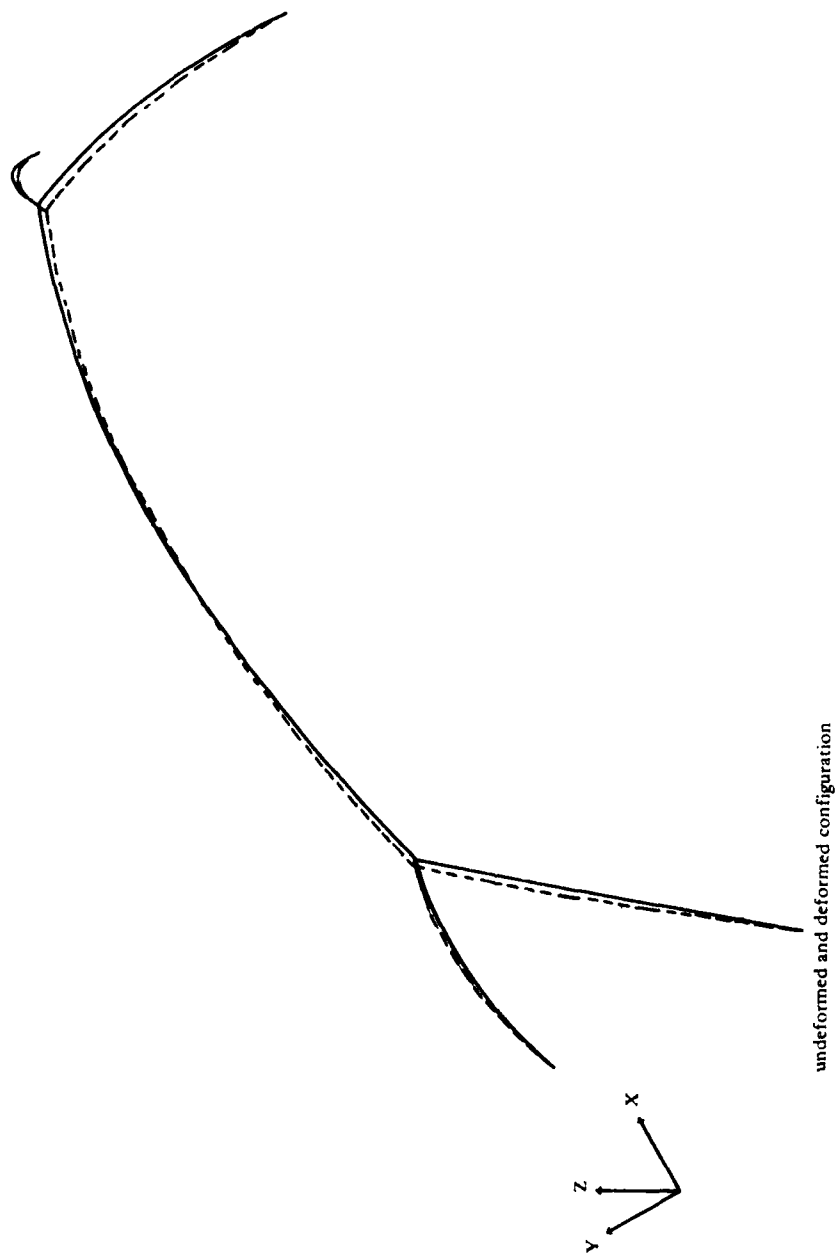


Figure 10. Perspective view of the deformed structure with the undeformed shape for comparison (field 3 = 2).

apply current profile at 45 dec increments

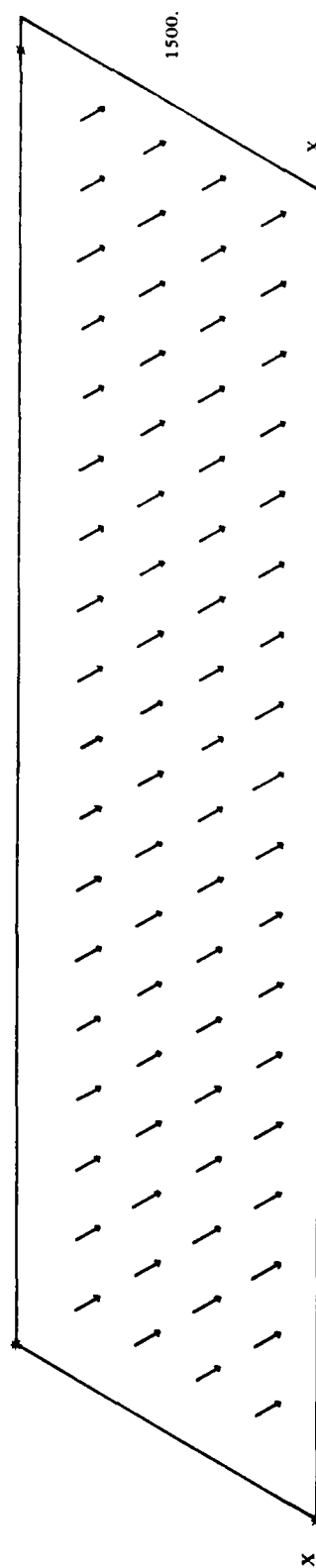
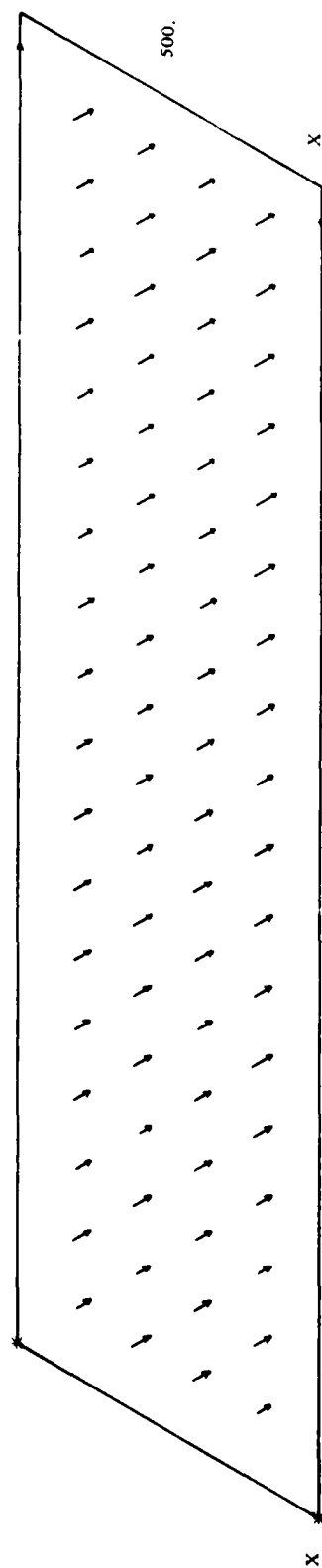


Figure 11. Unidirectional current field.

test for current option 3

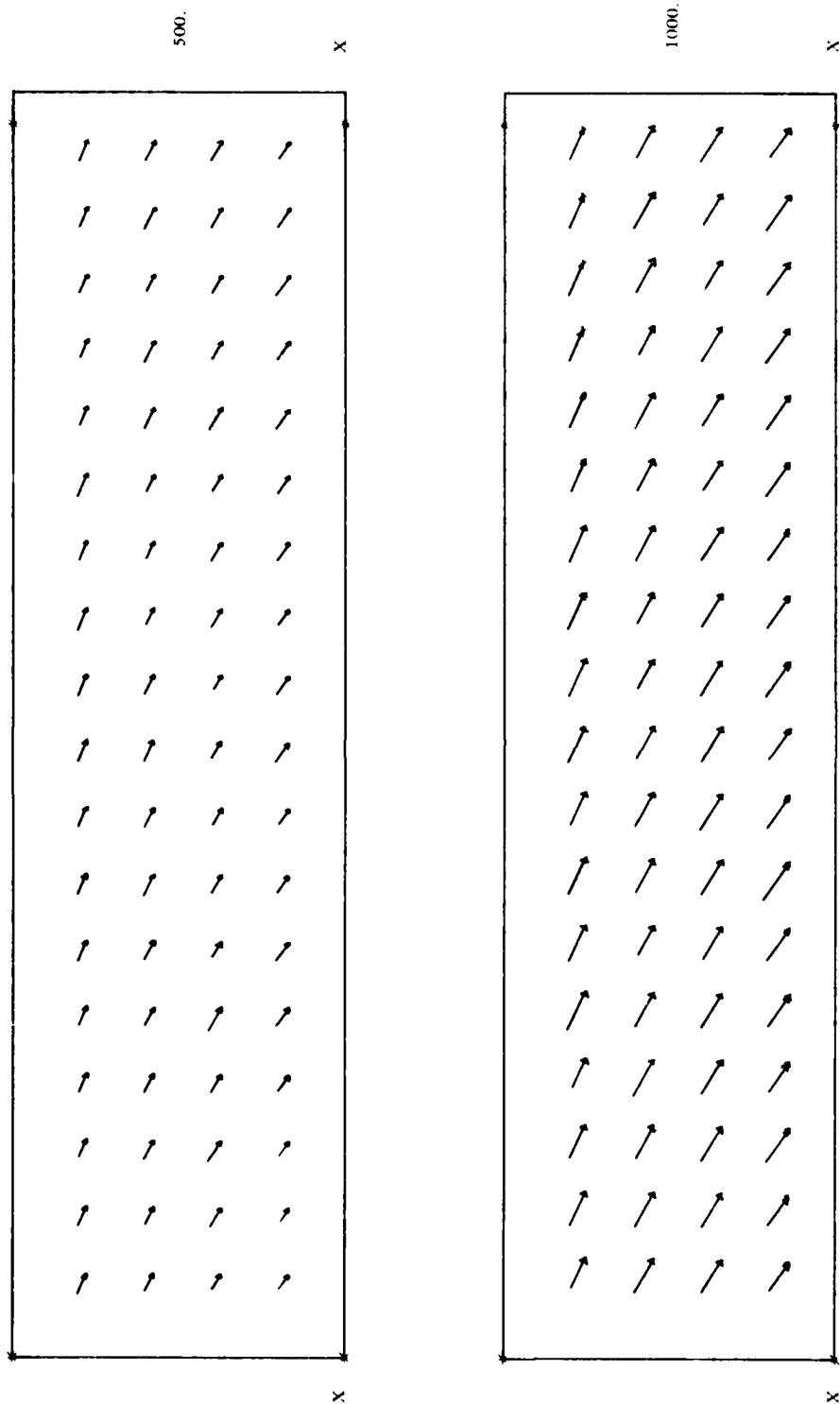


Figure 12. Non-unidirectional current field. (Note by sighting along the arrows that the field does curve.)

EOD CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	^EOD	Right adjust
3	9-16		Not used	
4	17-24		Not used	
5	25-32		Not used	
6	33-40		Not used	
7	41-48		Not used	
8	49-56		Not used	
9	57-64		Not used	
10	65-72		Not used	
11	73-77		Not used	
12	78-80		Not used	

NOTE: The EOD card is used to specify the end of data transmission or end of a parametric case.

EOP CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	⌵EOP	Right adjust
3	9-16		Not used	
4	17-24		Not used	
5	25-32		Not used	
6	33-40		Not used	
7	41-48		Not used	
8	49-56		Not used	
9	57-64		Not used	
10	65-72		Not used	
11	73-77		Not used	
12	78-80		Not used	

NOTE: The EOP card is used to specify the end of the problem and is required for a normal termination.

Cable Array Source Deck

The cable array source deck contains all of the cards required to describe the physical characteristics of the cable array under consideration. The last card in the cable array source deck must be an EOD card to signify the end of data transmission. The form of the cable array source deck is given below.

Cable Array Source Deck

<u>Card Type*</u>	<u>Comments</u>
NJNC	One card
ANC	One for each array anchor
IR	One for each cut going from original to reduced array
CAB	One (plus one continuation card) for each array cable
DCAB	One for each discrete device attached to a cable
DJNC	One for each discrete device attached at a junction
DEN	One card
EOD	Must be last card in source deck

Cable Array Source Tape

The cable array source tape is an alternate means of transmitting to DECEL1 the physical characteristics of the cable array under consideration. A recommended program for generating the cable array source tape from the cable array source deck is given below.

Cable Array Source Tape Generation

```
PRØGRAM STAPE
DIMENSION DATA(10)
DATA(IREAD = Unit number of card reader)
DATA(ITAPE = Unit number of source tape)
1 READ(IREAD,10)(DATA(I),I=1,10),EX,NSEG
WRITE(ITAPE,11)(DATA(I),I=1,10),EX,NSEG
IF(DATA(2).NE.4HDCAB)GØ TØ 3
READ(IREAD,20)TANDRG
WRITE(ITAPE,21)TANDRG
```

(continued)

*These cards may be arbitrarily ordered except for the EOD card. It is strongly recommended that the cards in the cable array source deck be given unique card numbers (Field 1 of each card). Note that LUN, NDAT, COMP, VEL, ANG, and EOP cards are not permitted in the cable array source deck.

Cable Array Source Tape Generation (Continued)

```
3 CONTINUE
  IF(DATA(2).EQ.4H EOD)GO TO 2
  GO TO 1
10 FORMAT(F4.0,A4,8F8.0,F5.0,I3)
11 FORMAT(F4.0,A4,8E15.8,/,E12.5,I3)
20 FORMAT(F8.0)
21 FORMAT(E15.8)
2 REWIND TAPE
  END
```

Parametric Study Source Decks

The parametric study source decks are used to transmit to DECEL1 accuracy requirements, current fields, and changes in the physical properties of the cable array under consideration. Each parametric study source deck must begin with an NDAT card and a Parametric Descriptive Title card and end with an EOD card. The form of the parametric study source decks is given below.

Parametric Study Source Decks

<u>Card Type*</u>	<u>Comments</u>
NDAT	Must be first card in parametric study source deck. Field 3 (current option) can change as 0 1, 0 2, or 0 3. The changes 1 2, 1 3, and 2 3, even with intermediate zeros, are not permitted.
Parametric Title Card	NDAT card <u>must</u> be followed immediately by parametric title card.
COMP	Must appear after first NDAT card. The accuracy requirement transmitted is retained until the appearance of a COMP card in another parametric study source deck.
VEL	Must not appear after NDAT card containing current option 0. All VEL cards required to transmit a current profile must appear after the first NDAT card containing a current option 1 or 2 or 3. The current profile transmitted is retained until the appearance of a VEL card in another parametric study source deck. The appearance of the first VEL card in a parametric study source deck zeros the entire current profile. Thus, to change from one current profile to another, all VEL cards required to specify the new profile must appear in the appropriate parametric study source deck.
ANG	Must not appear after NDAT card containing current option 0. One ANG card must appear after the first NDAT card containing current option 1, 2 or 3. The current angles transmitted are retained until the appearance of an ANG card in another parametric study source deck.
ANC	Used to change anchor data. See Note.
CAB	Used to change cable data. See Note.
DCAB	Used to change discrete device on cable data. See Note.
DJNC	Used to change discrete device at junction data. See Note.
EOD	Must be last card in parametric study source deck.

*These cards may be arbitrarily ordered except for the NDAT, Parametric Title, and EOD cards. Note that LUN, JNC, IR, DEN, and EOP cards are not permitted in the parametric study source decks.

NOTE: The array design changes which are permitted are those changing the physical data of the array but not the overall geometric layout of, or the number of discrete devices on, the array. These changes are keyed by matching the card number and type appearing in a parametric study source deck to the card number and type appearing in changes in the array physical data is given below.

Summary of Changes in the Array Physical Data Permitted (P)
and Not Permitted (NP)

Card Type	Field Number											
	1	2	3	4	5	6	7	8	9	10	11	12
ANC	NP	NP	NP	P	P	P	Not used					
CAB	NP	NP	NP	NP	NP	P	P	P	P	P	P	P
CONTINUATION CAB	P											
DCAB	NP	NP	NP	1≠2	NP	P	P	P	P	P	P	P
DJNC	NP	NP	NP	NP	NP	P	P	P	Not used			

OVERALL INPUT DECK

The overall input deck consists of a LUN card (optional) specifying the I/O options and the logical unit numbers of the required I/O devices, followed by the cable array source deck (or tape), followed by any number of parametric study source decks, and ended by an EOP card signifying the end of the problem. The form of the overall input deck is given below.

Overall Input Deck

- LUN Card (optional)
 - Cable Array Source Deck (or Tape)
 - Parametric Study Source Decks
- EOP Card

EXAMPLE

1. Compilation of cable array source deck errors only.

```
1000^LUN^^^^^^60^^^^^^61^^^^^^24 (or omit this card)
*****Main Title Card*****
      Cable Array Source Deck (or Tape)
1001^EOP
```

2. Deflections of the source deck cable array due to a current profile.

```
(LUN card omitted)
*****Main Title Card*****
      Cable Array Source Deck (or Tape)
1001NDAT^^^^^^1
*****Parametric Study 1 Title Card*****
1002COMP
1003^VEL
1010^VEL
1011^ANG
1012^EOD
1013^EOP
```

3. Deflections of the source deck cable array due to a current profile and effects of buoyancy changes on these deflections.

```
(LUN card omitted)
*****MAIN TITLE CARD*****
Cable Array Source Deck (or Tape) containing a card:
^^^9DJNC^^^^^^3^^^^^^^^^^^^^^^^^^^^10000.^^^1.95^^^35.3
1001NDAT^^^^^^1
*****Parametric (see note) Study 1 Title Card*****
1002COMP
1003^VEL
1010^VEL
1011^ANG
1012^EOD
1013NDAT^^^^^^1
*****Parametric Study 2 Title Card*****
^^^9DJNC^^^^^^3^^^^^^^^^^^^^^^^^^^^12500.^^^1.95^^^35.3
1014^EOD
1015^EOP
```

NOTE: In each case unique card numbers were assigned, otherwise an error would have resulted. However, any or all card numbers could have been omitted and no error would result.

ERROR MESSAGES

DECEL1 contains a series of internal error checks to insure that the original cable array is properly reduced to a statically determinate array; the input data are consistent; and the deck is properly structured.

If errors are found, the entire list of input cards is printed; and cards with errors are identified by an error code number. The text of the coded error message is printed after the card listing. All cards are scanned for errors; however, only the first error on a card is detected. A card with a DECEL1 detected error should be scanned visually to check for other errors.

DEFINITION OF ERRORS

Type 0 -

A type 0 error indicates that the card type identifier (Field 2) is not recognizable.

Type 1A - LUN

Field 6 not equal 0 or 1

Type 1B - LUN

Field 8 not equal 0,1,2

Type 1C - LUN

Non-unique numbers assigned to required I/O units.

Type 1A - NJNC

Field 3 greater than 44 or less than 2.

Type 1A - ANC

Field 3 greater than 44 or less than 1.

Type 1A - IR

Field 3 = Field 4.

Type 1B - IR

Fields 3 or 4 greater than 44 or less than 1.

Type 1A - CAB

Field 3 greater than 22 or less than 1.

Type 1B - CAB

Field 4 = Field 5.

Type 1C - CAB

Fields 4 or 5 greater than 44 or less than 1.

Type 1D - CAB

Fields 7, 8 or 9 less than or equal to 0.

Type 1E - CAB

Fields 10 or 11 less than 0

Type 1F - CAB

Field 10=0 and Field 11 not equal 0

Type 1G - CAB

Field 10 not equal 0 and Field 11=0.

Type 1H - CAB
Field 12 greater than 50 or less than 1.

Type 1A - DCAB
Field 3 greater than 22 or less than 1.

Type 1B - DCAB
Field 4 greater than 2 or less than 1.

Type 1C - DCAB
Field 5 greater than 1000 or less than 1.

Type 1D - DCAB
Field 4=1 and Field 9 less than or equal to 0.

Type 1E - DCAB
Field 4=2 and Field 9 not equal 0.

Type 1F - DCAB
Fields 7,8 or 10 less than 0.

Type 1A - DJNC
Field 3 greater than 44 or less than 1.

Type 1B - DJNC
Field 7 or 8 less than 0.

Type 1A - DEN
Field 3 less than 0.

Type 1A - NDAT
Field 3 not equal 0,1, or 2.

Type 1A - COMP
Field 3 less than or equal 0.

Type 1A - ANG
Field 4 less than or equal 0.

Type 1B - ANG
Field 5 less than Field 3.

Type 2A - ANC
The junction number assigned to the anchor (Field 3) has been assigned to a preceding ANC card or to an S=L junction (Field 5) on a preceding CAB card.

Type 2A - CAB
The junction number assigned to the S=L junction (Field 5) has been assigned on a preceding CAB card or to an anchor junction (Field 3) on a preceding ANC card.

Type 3 - CAB
A Type 3 error appears only in conjunction with a CAB card and indicates that the number assigned to the cable (Field 3) has been assigned on a preceding CAB card.

Type 4A - IR
The junction number assigned in Field 3 has been assigned in Fields 3 or 4 of a preceding IR card.

- Type 4B - IR
The junction number assigned in Field 4 has been assigned in Field 3 of a preceding IR card.
- Type 6A - NJNC
An NJNC card has previously appeared in the particular source deck.
- Type 6A - DEN
A DEN card has previously appeared in the particular source deck.
- Type 6A - COMP
A COMP card has previously appeared in the particular source deck.
- Type 6A - VEL
Twenty-five VEL cards have previously appeared in the particular source deck.
- Type 6B - VEL
The Z-coordinate at which the current velocity is specified (Field 3) has been used on a preceding VEL card in the particular source deck.
- Type 7 -
A Type 7 error indicates an inadequacy of information in cable array source deck (or tape). The other information column under the error heading contains a 1x3 matrix, the elements of which give respectively the number of NJNC cards read, the number of DEN cards read, and the number of ANC cards read. A zero element is an error (see cable array source deck).
- Type 8 -
A Type 8 error indicates a discontinuity in numbering the cables in the array. The other information column under the error heading contains a 1x22 matrix, the elements of which contain one or zero indicating, respectively, the use or non-use of the corresponding column number as a cable number. Zeros interspersed with ones are in error (see array description).
- Type 9 -
A Type 9 error indicates a discontinuity in numbering the junctions in the array. The other information column under the error heading contains a 1x44 matrix, the elements of which contain one or zero indicating respectively, the use or non-use of the corresponding column number as a junction number. Zeros interspersed with ones are in error (see array description and reduction to a statically determinate array).
- Type 11 -
A Type 11 error indicates an improper reduction of the original cable array to a statically determinate array or an absence of certain input cards in the cable array source deck (or tape). The other information column

under the error heading contains a 1x5 matrix, the elements of which give, respectively, the number of CAB cards read, the number of ANC cards read, the number of junctions in the original cable array (Field 3 of the NJNC card), the number of required cuts (Eq. (1)) calculated from the preceding information, and the number of IR cards read. Column 5 not equal to column 4 is an error (see reduction to a statically determinate array).

Type 12A - IR

The junction number assigned in Field 3 is less than or equal to the number of junctions in the original (unreduced) array (Field 3 of the NJNC card).

Type 12B - IR

The junction number assigned in Field 3 is greater than the number of junctions in the original (unreduced) array plus the number of cuts made in reducing the array (Eq. (1)).

Type 12C - IR

The junction number assigned in Field 4 is greater than the number of junctions in the original (unreduced) array.

Type 12A - CAB

The junction number assigned in Field 4 is greater than the number of junctions in the original (unreduced) array (Field 3 of the NJNC card) plus the number of cuts made in reducing the array (Eq. (1)).

Type 12A - DCAB

The cable number assigned in Field 3 does not correspond to a cable number assigned to a cable (Field 3 of the CAB cards).

Type 12B - DCAB

The distance of the discrete device from the S=0 junction of the cable (Field 10) is greater than or equal to the length of the corresponding cable (Field 9 of the CAB card).

Type 12A - DJNC

The junction number assigned in Field 3 does not correspond to either a junction number assigned to an anchor (Field 3 or the ANC cards) or a junction number assigned to an S=L junction of a cable (Field 5 of the CAB cards).

Type 13 -

A Type 13 error indicates that the original cable array has not been properly reduced to a statically determinate array or that junctions have been improperly numbered. The other information column under the error heading contains the message, improper array reduction or junction numbering. Check tree representation of array (see array reduction section of Users Manual) against junction numbering on ANC and CAB cards.

Type 14A -

A Type 14 error indicates an inadequacy of information in a parametric study source deck. The other information column under the error heading contains a 1x5 matrix, the elements of which give, respectively, the number of COMP cards read, the current field option, the number of VEL cards read, the number of VEL cards containing a Z-coordinate (Field 3) less than or equal to the minimum Z-coordinate transmitted by the ANC cards (Field 6 of the ANC cards), and the number of ANG cards read. If column 1 contains a zero, then a COMP card has not appeared after the first NDAT card (see parametric study source decks).

Type 14B -

A Type 14 error indicates an inadequacy of information in a parametric study source deck. The other information column under the error heading contains a 1x5 matrix, the elements of which give, respectively, the number of COMP cards less than or equal to the minimum Z-coordinate transmitted by the ANC cards (Field 6 of the ANC cards), and the number of ANG cards read. If column 2 contains a one and any of columns 3, 4 or 5 contain a zero, then the standard current field has not been properly formulated (see parametric study source decks and standard current field).

Type 15 -

A Type 15 error indicates that an unpermitted change has been attempted in a parametric study source deck. (See parametric study source decks.)

Type 16 -

A Type 16 error indicates an improper deck structure. See cable array source deck, parametric study source decks, and overall input deck.

Type 17 -

A Type 17 error indicates that the cable array source deck (or tape) contains more than 2150 records. The other information column under the error heading contains the message common/B1/bounds exceeded. See Users Manual. A Type 17 error is readily correctable if the machine being used has sufficient core storage. This correction is achieved by changing the row dimension of DATAT on cards DES025 and INF022 from 2150 to a number exceeding the number of records in the cable array source deck (or tape). Simultaneously the comparison value on card INP615 must be changed from 2150 to the new row dimension of DATAT.

Type 18 -

A Type 18 error indicates that the accuracy required for the array equilibrium calculations (Field 3 of the COMP card) has not been obtained during the calculations. This is for one of two possible reasons.

- A. Some cable segments have gone slack (that is, the segments have near zero tension. An examination of the tensions printed out in conjunction with a Type 18 error will reveal if this is the reason. If it is, see the section on statically unstable cable arrays in Reference 2 for possible remedial actions. If it is not then ...
- B. The accuracy required for the equilibrium calculations is simply too stringent for the computer to handle (see COMP card). An examination of the final value of the accuracy obtained, printed out in conjunction with a Type 18 error, will reveal the best accuracy obtainable. Field 3 of the COMP card should be modified to reflect this information.

ARRAY DESCRIPTIVE OUTPUT

Following each error-free reading of a parametric study source deck, DECEL1 transmits to the line printer a description of the physical characteristics of the cable array under study. This printout includes anchor junctions and locations, information concerning the reduction of the original cable array to a statically determine array, properties of the cables in the array, properties of the discrete devices located at array junctions total number of Type 1 and 2 devices, current field option and current profile and calculational accuracy requirements.

The format of the array descriptive output is self-explanatory. A sample printout is given in Appendix A.

STRUCTURAL OUTPUT

If output option 0 or 2 is selected, DECEL1 transmits to the line printer a structural output. The structural printout follows and refers to the array characterized in the array descriptive output and contains information giving:

- a. A description of the current field (i.e., no current or current from xxx degrees)
- b. The cable forces and angles at each anchor
- c. The position coordinates of the original (unreduced) array junctions, the displacement of these coordinates from the no-current coordinates, and the cable forces and angles at each junction
- d. The maximum and minimum tensions and their locations for each array cable and the maximum displacement from the no-current condition and its location for each cable
- e. The position coordinates, the displacement of these coordinates from the no-current coordinates, and the tension at each Type 1 and 2 DCAB device in the array

This latter information is printed out in the same order that the Type 1 and 2 DCAB devices are numbered. Note that it is possible to obtain the latter information for any point on any cable in the array by defining a "dummy" Type 2 DCAB device to be located at the point. A dummy Type 2 DCAB device is simply one for which fields 6, 7, and 8 of the DCAB card are left blank so that the "device" has no effect on the array equilibrium calculations.

The format of the structural output is self-explanatory. A sample printout is given in Appendix A (Figure 17).

DEVICE LOCATION OUTPUT

If output option 1 or 2 is selected, DECEL1 transmits to tape or cards a device location output. The device location output contains information giving:

1. A description of the current field (i.e., no current or current from xxx degrees)
2. The position coordinates of each Type 1 and 2 discrete device in the array

Four types of records are associated with the device location output. Each of these records is written with the format:

(A4,I4,3F10.2)

REC Record

Field	Format	Contents
1	A4	^REC
2	I4	Record number
3	F10.2	Not used
4	F10.2	Not used
5	F10.2	Not used

NOTE: The REC record is used to identify the cable array under study. The record number (Field 2) is referenced in the array descriptive output in the statement, "DEVICE LOCATION OUTPUT RECORD XX REFERS TO THIS ARRAY." The information following a REC record refers to the identified array.

CUR Record

Field	Format	Contents
1	A4	^CUR
2	I4	0 if no current acting on array 1 if current is acting on array
3	F10.2	Blank if Field 2 = 0 Current angle if Field 2 = 1
4	F10.2	Not used
5	F10.2	Not used

NOTE: The CUR record is used to describe the current field (i.e., no current or current from xxx degrees). The information following a CUR record refers to the identified current field.

DEV Record

Field	Format	Contents
1	A4	^DEV
2	I4	Discrete device index (Field 5 of the DCAB and DJNC cards)
3	F10.2	X coordinate of device
4	F10.2	Y coordinate of device
5	F10.2	Z coordinate of device

NOTE: The DEV records are used to transmit the position coordinates of the Type 1 and 2 discrete devices in the array. There is one DEV record for each indexed (Types 1 and 2) device for each identified current field.

EOP Record

Field	Format	Contents
1	A4	^EOP
2	I4	Not used
3	F10.2	Not used
4	F10.2	Not used
5	F10.2	Not used

NOTE: The EOP record is used to signify the end of output transmission.

A typical overall device location output file is illustrated below.

```
^REC^^1
^CUR^^0
    DEV Records (one for each indexed device)
^CUR^^1 current angle
    DEV Records
^CUR^^1 current angle
    DEV Records
^REC^^2
^CUR^^0
    DEV Records
^EOP
```

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Appendix A
EXAMPLE PROBLEM

An example problem has been included both to illustrate actual input and output and as a test case. The test case can be used to confirm proper operation of DECEL1 when implemented on a particular host computer. The test case structure is shown in Figure 13. The structure represents an acoustic array in the horizontal leg; this leg has been buoyed at the center to keep it approximately horizontal. A signal cable rises from one anchor to a subsurface buoy. The applied current is unidirectional with the profile shown in Figure 14. The current is acting broadside to the structure. The DECEL1 model of the structure is shown in Figure 15; other details of the modeling are shown in Tables 4 through 8.

Input card images are shown in Figure 16. Note that one dummy-DCAB-device card was intentionally placed "out of sequence" just after the NJNC card. This illustrates that the card sequence is essentially arbitrary, except as noted elsewhere in the manual.

The output from DECEL1 is shown in Figures 17 and 18. Note that the "number of indexed devices" count includes the three DJNC devices. The "Array Equilibrium with no Current" portion defines both the initial positions of devices and the properties of the DCAB devices. If the "do not print" flag had been set on any DCAB card, that device would not have been tabulated here; however, its effects would have been accounted for in the solution.

In the portion of the output where the current was applied (Figure 18), the displacement of all junctions and devices is listed relative to the present no-current position and relative to the original no-current case. In this case both displacements are identical since the new no-current reference flag had not been set on the NDAT card.

Figure 19 shows the configuration of the array both in the no-current condition (dotted lines) and with current applied (solid lines). For this plot the default perspective view angles were used. Other views (plan or elevation) of the same structure in the same current could be obtained by additional identical NDAT cases with the perspective plotting angles changed accordingly.

Table 4. Cables

Cable No.	Junction		Length (ft)	Weight/Foot (lb/ft)	Diameter (in.)	Drag Coefficient
	From	To				
1	1	2	3,000	0.25	1.0	1.4
2	2	8	3,000	0.25	1.0	1.4
3	2	4	5,000	0.20	0.75	1.4
4	4	9	3,000	0.25	1.0	1.4
5	4	10	3,000	0.25	1.0	1.4
6	9	7	4,000	0.3	1.25	1.4

Table 5. Anchor Locations

Anchor No.	Junction No.	x	y	z
1	1	0	1,000	0
2	3	0	-1,000	0
3	5	7,000	-1,000	0
4	6	7,000	1,000	0

Table 6. Imaginary Reaction Cuts

Junction No.	Cut No.
3	8
5	9
6	10

Note: In the model the cables terminate at cuts rather than at anchors.

Table 7. DJNC Devices

Device Junction No.	Device Buoyancy (lb)	Device Drag Coefficient	Device Frontal Area (ft ²)
2	3,000	1.0	26.0
4	3,000	1.0	26.0
7	3,000	1.0	26.0

Table 8. DCAB Devices

Device Index	On Cable No.	S Coordinate (ft)	Device Buoyancy (lb)
9	3	2,500	1,000

Note: Other dummy devices are used to obtain a printout of the spatial location of the device; these devices have not been tabulated here. Dummy devices have a very small weight and no drag.

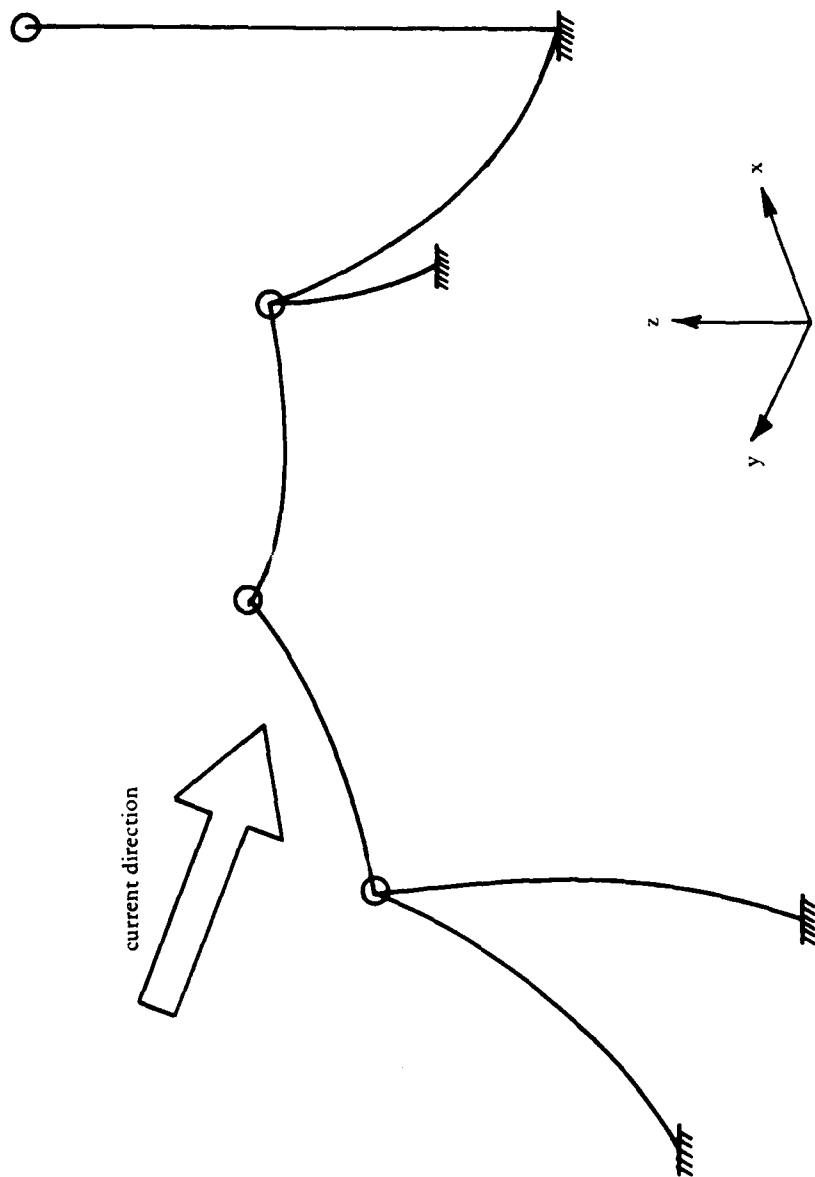


Figure 13. DECEL1 test case structure.

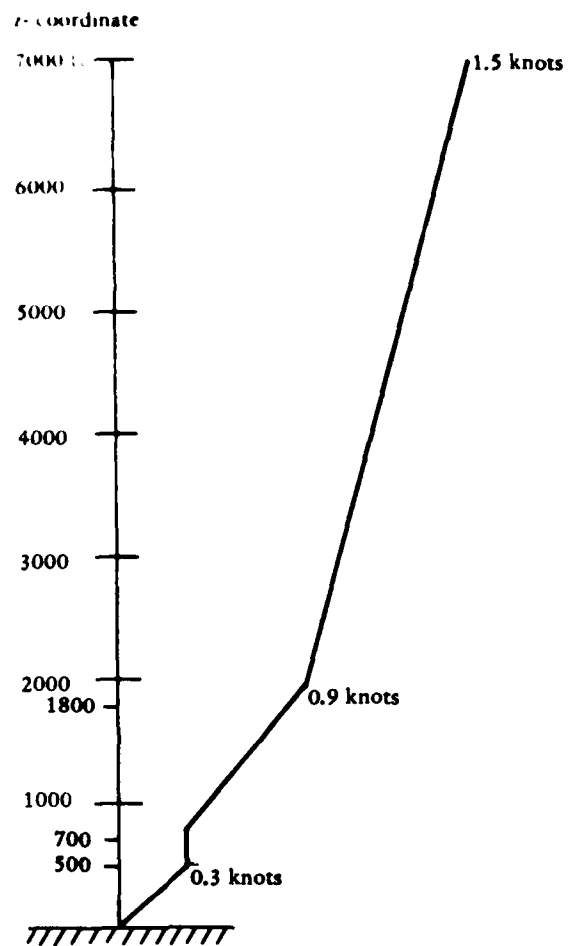


Figure 14. Current profile.

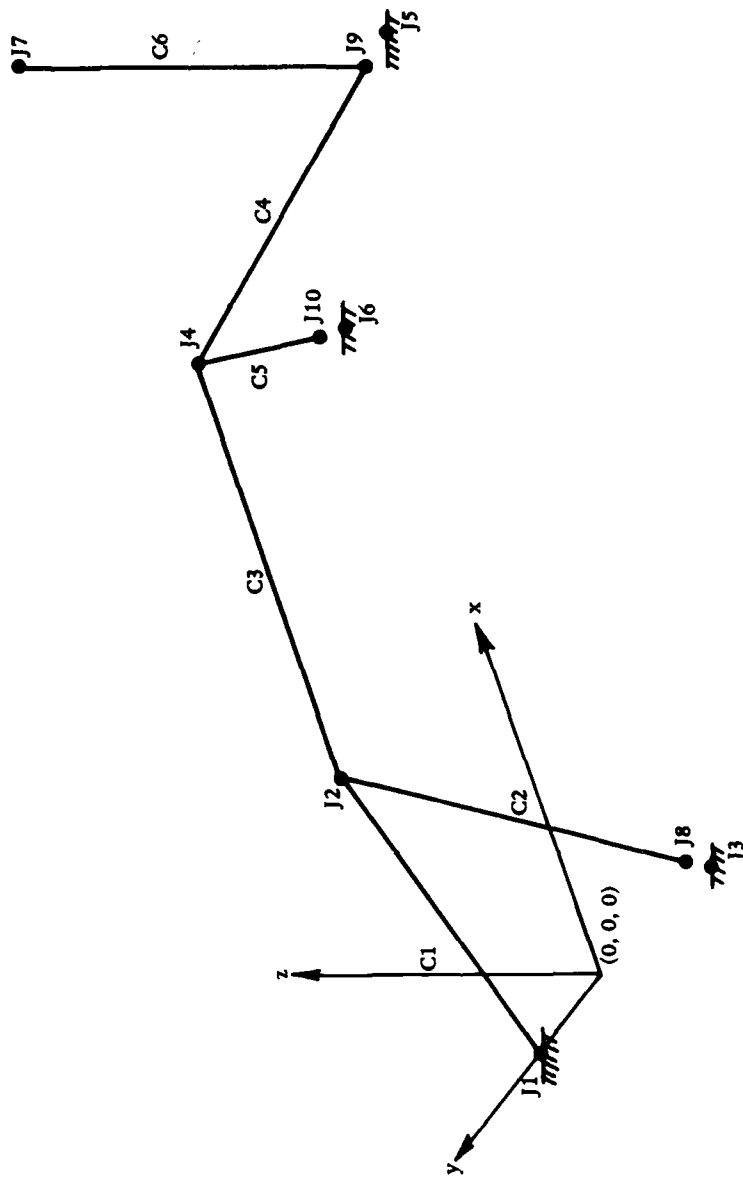


Figure 15. DECEL1 test case structure model.

UECF11 TEST CASE

NJNC	7			0.001		0.01	750.	
NCAB	1	2						
ANC	1	0.0	1000.	0.0				
ANC	3	0.0	-1000.	0.0				
ANC	5	7000.0	-1000.	0.0				
ANC	6	7000.	1000.	0.0				
IR	8	3						
IR	9	5						
IR	10	6						
CAB	1	1	2	-0.25	1.4	1.0	3000.	50
0.03								
CAH	2	2	8	-0.25	1.4	1.0	3000.	50
0.03								
CAB	3	2	4	-0.20	1.4	0.75	5000.	50
0.03								
CAB	4	4	9	-0.25	1.4	1.0	3000.	50
0.03								
CAB	5	4	10	-0.25	1.4	1.0	3000.	50
0.03								
CAB	6	9	7	-0.30	1.4	1.25	4000.	50
0.03								
NCAB	1	2		0.001		0.01	1500.	
NCAB	1	2		0.001		0.01	2250.	
NCAB	2	2		0.001		0.01	750.	
NCAB	2	2		0.001		0.01	1500.	
NCAB	2	2		0.001		0.01	2250.	
NCAB	3	2		0.01		.1	1000.	
NCAB	3	2		0.01		.1	2000.	
NCAB	3	2		1000.	1.	5.	2500.	
NCAB	3	2		0.01		.1	3000.	
NCAB	3	2		0.01		.1	4000.	
NCAB	4	2		0.001		0.01	750.	
NCAB	4	2		0.001		0.01	1500.	
NCAB	4	2		0.001		0.01	2250.	
NCAB	5	2		0.001		0.01	750.	
NCAB	5	2		0.001		0.01	1500.	
NCAB	5	2		0.001		0.01	2250.	
NCAB	6	2		0.001		0.01	1000.	
NCAB	6	2		0.001		0.01	2000.	
NCAB	6	2		0.001		0.01	3000.	
NJNC	2			3000.	1.0	26.		
NJNC	4			3000.	1.0	26.		
NJNC	7			3000.	1.0	26.		
DEFN	1.59							
END								
DATA	1							
APPLY 90 DEGREE CURRENT (TOWARD -Y AXIS)								
COMP	0.1							
VEL	0.0	0.0						
VFL	500.0	0.3						
VEL	700.0	0.3						
VEL	1800.0	0.9						
VEL	7000.0	1.5						
ANG	90.	1.	90.					
PPLT	2							
FCD								
ECP								

Figure 16. Input card images.

DECEL1 UPDATE INFORMATION
=====

THIS IS THE JANUARY 1980 VERSION OF DECEL1 AS DESCRIBED IN THE USERS MANUAL
NO UPDATES HAVE BEEN ADDED

NO ERRORS DETECTED

DECEL1 TEST CASE

APPLY 90 DEGREE CURRENT (IC=AKU -Y AXIS)

PHYSICAL CHARACTERISTICS OF THE STRUCTURAL CABLE ARRAY

PHI= 0.00

SINCE PHI=0, THE MAGNETIC AND ARRAY REFERENCED COORDINATE SYSTEMS ARE IDENTICAL.

ALL X,Y,Z RESULTS AND DISPLACEMENTS ARE GIVEN IN TERMS OF THE ARRAY FIXED COORDINATE SYSTEM.

NO. OF ANCHORS IS 4

JUNCTION NO.	X-COORDINATE	Y-COORDINATE	Z-COORDINATE
1	0.00	1000.00	0.00
3	0.00	-1000.00	0.00
5	7000.00	-1000.00	0.00
6	7000.00	1000.00	0.00

NO. OF JUNCTIONS IN ORIGINAL ARRAY IS 7

NO. OF CUTS MADE IN ORIGINAL ARRAY IS 3

JUNCTION NO. OF CUT	JUNCTION NO. AT WHICH CUT MADE
4	3
9	5
10	6

Figure 17. Output from DECEL1 for the example problem.

NO. OF CABLES IS 6

CABLE NO.	S#0 JUNC	S#L JUNC	LENGTH	DIAMETER	WEIGHT/LENGTH	NORM DRAG COEFFICIENT	RIGIDITY	CONSTITUTIVE EXPONENT	NO. OF ELEMENTS	TANG DRAG COEFFICIENT
1	1	2	3000.00	1.000	-.250	1.400	0.	0.000	50	.030
2	2	8	3000.00	1.000	-.250	1.400	0.	0.000	50	.030
3	2	4	5000.00	.750	-.200	1.400	0.	0.000	50	.030
4	4	9	3000.00	1.000	-.250	1.400	0.	0.000	50	.030
5	4	10	3000.00	1.000	-.250	1.400	0.	0.000	50	.030
6	9	7	4000.00	1.250	-.300	1.400	0.	0.000	50	.030

PROPERTIES OF THE DEVICES LOCATED AT JUNCTIONS ARE AS FOLLOWS

DEVICE JUNC. NO.	DEVICE WEIGHT	DEVICE DRAG COEFFICIENT	DEVICE FRONTAL AREA
2	3000.00	1.000	26.00
4	3000.00	1.000	26.00
7	3000.00	1.000	26.00

TOTAL NO. OF INDEXED DEVICES IS 20

ACCURACY REQUIRED IN CALCULATIONS IS .1000
DECEL TEST CASE

ARRAY EQUILIBRIUM WITH NO CURRENT

ARRAY ANCHORS

JUNC. NO. OF ANCHOR	CABLE AT ANCHOR	TENSION AT ANCHOR	X-COMP	Y-COMP	Z-COMP	MOR.-COMP	CABLE ANGLES WRT X-AXIS	XY-PLANE
1	1	974.87	466.84	-420.50	745.39	628.30	-42.01	49.87
3	2	974.89	466.85	420.50	745.41	628.31	42.01	49.87
5	4	983.22	-466.83	423.53	754.60	630.33	137.78	50.13
6	5	983.28	-466.86	-423.53	754.65	630.35	-137.79	50.13

ARRAY CABLES

CABLE NO.	MAXIMUM TENSION	S-COORD OF	MINIMUM TENSION	S-COORD CF
1	1622.02	3000.00	974.87	0.00
2	1622.04	0.00	974.89	3000.00
3	1054.82	2500.00	933.69	46.01
4	1631.29	0.00	983.22	3000.00
5	1631.35	0.00	983.28	3000.00
6	3000.00	4000.00	1800.00	0.00

Figure 17. Continued.

ARRAY JUNCTIONS

JUNC. NO.	CABLE AT JUNCTION	TENSION AT JUNCTION	CABLE ANGLES WRT X-AXIS	XY-PLANE	JUNCTION LOCATION X-COORD	Y-COORD	Z-COORD
2	1	1622.02	137.99	-67.21	1110.22	-200	2588.59
2	2	1622.04	-137.99	-67.21			
2	3	933.74	.00	-56			
4	3	933.74	-180.00	.57	5897.72	.02	2592.27
4	4	1631.29	-62.22	-67.27			
4	5	1631.35	42.21	-67.27			
7	6	3000.00	0.00	-90.00	7000.00	-1000.00	4000.01

INDEXED DEVICES ALONG ARRAY CABLES

DEVICE INDEX	CABLE NO.	S COORDINATE	TENSION AT DEVICE	DEVICE LOCATION X-COORD	Y-COORD	Z-COORD	DEVICE WEIGHT	DEVICE LENGTH	NORMAL DMAG CU	TANG DRAG CU
1	1	750.00	1124.74	334.42	698.78	599.49	.00	0.00	0.000	0.000
2	1	1500.00	1284.54	625.66	436.45	1238.06	.00	0.00	0.000	0.000
3	1	2250.00	1450.98	882.06	205.51	1904.42	.00	0.00	0.000	0.000
4	2	750.00	1451.00	882.06	-205.51	1904.42	.00	0.00	0.000	0.000
5	2	1500.00	1284.56	625.66	-436.45	1238.06	.00	0.00	0.000	0.000
6	2	2250.00	1124.76	334.41	-698.79	599.49	.00	0.00	0.000	0.000
7	3	1000.00	952.99	2103.66	.00	2684.83	.01	0.00	0.000	0.000
8	3	2000.00	1012.17	3057.19	.01	2980.75	.01	0.00	0.000	0.000
9	3	2500.00	1054.82	3509.25	.01	3193.98	1000.00	0.00	1.000	0.000
10	3	3000.00	1019.43	3958.20	.01	3020.73	.01	0.00	0.000	0.000
11	3	4000.00	956.85	4906.32	.01	2707.82	.01	0.00	0.000	0.000
12	4	750.00	1460.14	8124.52	-2105.74	1907.72	.00	0.00	0.000	0.000
13	4	1500.00	1293.56	6379.21	-436.40	1241.34	.00	0.00	0.000	0.000
14	4	2250.00	1133.51	6666.31	-699.02	601.17	.00	0.00	0.000	0.000
15	5	750.00	1460.21	6124.52	205.77	1907.72	.00	0.00	0.000	0.000
16	5	1500.00	1293.61	6379.21	436.42	1241.34	.00	0.00	0.000	0.000
17	5	2250.00	1133.57	6666.31	699.09	601.16	.00	0.00	0.000	0.000
18	6	1000.00	2100.00	7000.00	-1000.00	1000.01	.00	0.00	0.000	0.000
19	6	2000.00	2400.00	7000.00	-1000.00	2000.01	.00	0.00	0.000	0.000
20	6	3000.00	2700.00	7000.00	-1000.00	3000.01	.00	0.00	0.000	0.000

Figure 17. Continued.

DECEL1 TEST CASE

APPLY 90 DEGREE CURRENT (TOWARD -Y AXIS)

NUMBER OF ITERATIONS FOR CONVERGENCE - 12

CURRENT FIELD OPTION IS 1

Z-COORDINATE OF CURRENT	MAGNITUDE OF CURRENT AT Z	DIRECTION OF CURRENT AT Z FROM N-AXIS (DEGREES)
(FEET)	(KNOTS)	
0.00	0.000	0.000
500.00	.300	0.000
700.00	.300	0.000
1000.00	.900	0.000
7000.00	1.500	0.000

*****CURRENT DIRECTION IS POSITIVE IN THE CLOCKWISE SENSE FROM THE N-AXIS*****

ARRAY EQUILIBRIUM WITH 270.00 DEGREE CURRENT

ARRAY EQUILIBRIUM WITH CURRENT DIRECTION
270.00 DEGREES FROM X-AXIS(+ IS COUNTERCLOCKWISE)
90.00 DEGREES FROM N-AXIS(+ IS CLOCKWISE)

ARRAY ANCHORS

JUNC. NO. OF ANCHOR	CABLE AT ANCHOR	TENSION AT ANCHOR	X-COMP	Y-COMP	Z-COMP	HCR-COMP	CABLE ANGLES WRT X-AXIS XY-PLANE
1	1	2120.84	921.12	-1197.18	1488.71	1510.53	-52.42 44.58
3	2	105.56	93.45	15.84	-46.45	94.79	9.64 -26.10
5	4	104.64	-92.76	15.83	-45.78	94.10	-25.94 170.32
6	5	2135.04	-921.38	-1202.57	1504.41	1514.96	-127.46 44.80

ARRAY CABLES

CABLE NO.	MAXIMUM TENSION	S-COORD CF	MINIMUM TENSION	S-COORD CF	MAXIMUM DISP.	S-COORD CF	LOCATION OF THIS POINT X-COORD Y-COORD Z-COORD	NO CURRENT X-COORD Y-COORD Z-COORD	LOC. OF THIS POINT X-COORD Y-COORD Z-COORD
1	2704.86	3000.00	2120.84	0.00	486.17	3000.00	1172.55 -421.42 2354.31	1110.22 -1.00 2588.59	-270.59 1706.31
2	696.39	0.00	94.79	2814.21	576.02	976.69	1027.61 -730.14 1451.71	809.61 3510.22 .01	3194.48 1709.52
3	1274.32	2500.00	1175.90	2550.07	1098.62	2501.10	3508.36 -1034.93 2825.89	5897.72 7000.00 .02	-210.84 1709.52
4	696.81	0.00	94.10	2616.90	574.10	970.61	5978.03 -738.15 1457.38	6196.28 5897.72 7000.00	-210.84 1709.52
5	2720.35	0.00	2135.04	3000.00	483.26	0.00	5834.45 -418.76 2359.53	5897.72 7000.00 .02	-210.84 1709.52
6	3001.43	4000.00	1891.74	0.00	1363.45	4000.00	7000.00 -2333.47 3715.67	7000.00 -1000.00 4000.01	-210.84 1709.52

Figure 18 Output from DECEL1.

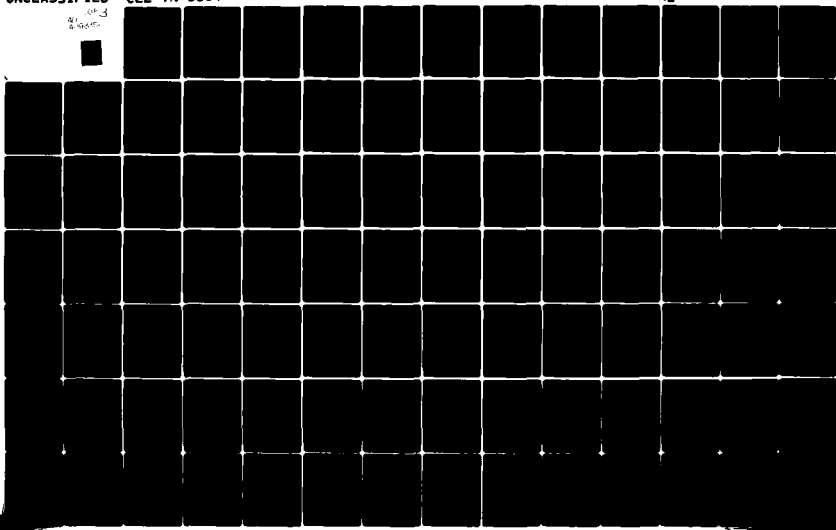
AD-A093 356

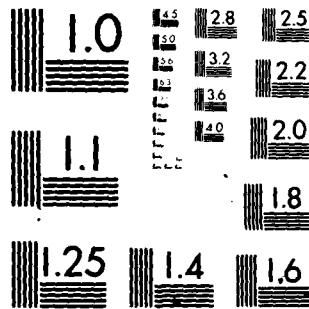
CIVIL ENGINEERING LAB (NAVY) PORT HUENEME CA F/G 13/13
DECEL1 USERS MANUAL. A FORTRAN IV PROGRAM FOR COMPUTING THE STA--ETC(U)
AUG 80 S SERGEV
CEL-TN-1584

NL

UNCLASSIFIED

01-3
2-1584-10





MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A

ARRAY JUNCTIONS										

JUNC. NO.	CABLE AT JUNCTION	TENSION AT JUNCTION	CABLE ANGLES WRT X-AXIS	XY-PLANE	X-COORD	Y-COORD	Z-COORD	DISP FROM NO CURRENT	DISP 1 JM ORIG NO CURRENT	
								X-DISP	Y-DISP	Z-DISP
2	2	696.39	-104.61	-63.07	117.55	-421.42	2354.31	62.33	-421.42	-234.28
2	3	1183.16	-27.14	-1.28	5834.45	-418.76	2359.53	-63.27	-418.78	-232.74
4	3	1183.48	-152.72	-50						
4	4	696.11	-75.56	-63.00						
4	5	2720.35	43.31	-60.55						
7	6	3101.43	90.00	-88.23	7000.00	-2333.47	3715.67	.00	-1333.47	-284.34

INDEXED DEVICES ALONG ARRAY CABLES										

DEVICE INDEX	CABLE NO.	S COORDINATE	TENSION AT DEVICE	X-COORD	Y-COORD	Z-COORD	DISP FROM NO CURRENT	DISP FROM ORIG NO CURRENT		
							X-DISP	Y-DISP	Z-DISP	
1	1	750.00	2256.30	315.98	589.93	542.51	-18.43	-108.85	-56.97	
2	1	1500.00	2398.83	614.23	208.61	1115.20	-11.43	-227.84	-123.46	
3	1	2250.00	2547.87	898.33	-134.96	1718.08	16.27	-340.47	-186.34	
4	2	750.00	521.60	1067.69	-688.35	1662.67	185.63	-482.83	-241.75	
5	2	1500.00	341.51	906.55	-820.23	943.19	280.89	-363.78	-295.48	
6	2	2250.00	169.94	620.14	-894.13	257.07	285.72	-195.35	-342.41	
7	3	1000.00	1193.47	2092.39	-802.26	2417.37	-11.28	-802.26	-267.46	
8	3	2000.00	1239.35	3040.22	-1006.85	2650.43	-16.97	-1006.86	-330.32	
9	3	2500.00	1214.32	3507.35	-1034.92	2825.47	-1.90	-1034.93	-368.51	
10	3	3000.00	1245.35	3972.33	-1007.15	2683.28	14.13	-1007.16	-337.45	
11	3	4000.00	1196.75	4916.46	-801.46	2436.58	10.14	-801.48	-271.24	
12	4	750.00	522.08	5938.34	-686.98	1668.23	-186.18	-481.25	-239.48	
13	4	1500.00	341.95	6098.03	-819.88	948.62	-281.18	-383.08	-292.72	
14	4	2250.00	170.11	6381.92	-894.01	261.42	-286.39	-194.93	-339.74	
15	5	750.00	2563.14	6107.12	-132.76	1722.43	-17.40	-338.53	-185.29	
16	5	1500.00	2413.83	6389.56	210.20	1118.42	10.35	-226.63	-122.92	
17	5	2250.00	2270.95	6686.00	590.79	544.31	17.69	-108.30	-56.85	
18	6	1000.00	2149.66	7000.00	-1507.81	861.12	.00	-507.81	-138.88	
19	6	2000.00	2419.27	7000.00	-1930.95	1766.54	.00	-930.95	-233.46	
20	6	3000.00	2704.36	7000.00	-2215.68	2723.92	.00	-1215.68	-276.09	
ANALYSIS COMPLETED										

Figure 18. Continued.

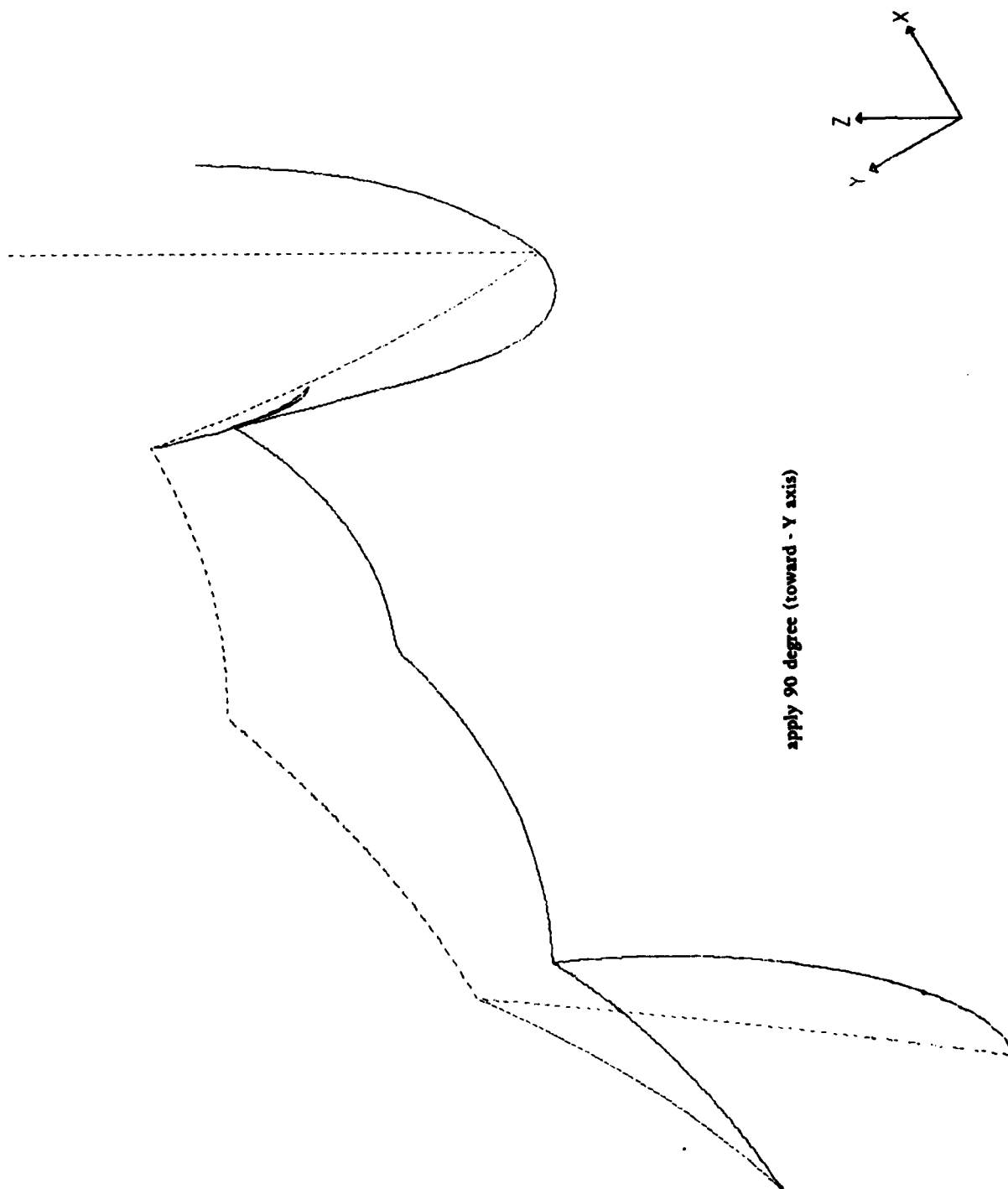


Figure 19. Undeformed and deformed configurations of the test case structure.

Appendix B
DECEL1 PROGRAM LISTING

```

1  *DECK DECELL
2  PROGRAM DECELL(INPUT,OUTPUT,TAPE8,TAPE2,TAPE25,TAPE60=INPUT,TAPE6
3  11=OUTPUT,TAPE3,TAPE4,TAPE10,NPFILE)
4
5  C
6  C A FORTRAN IV PROGRAM FOR COMPUTING THE STATIC DEFLECTIONS
7  C OF STRUCTURAL CABLE ARRAYS
8
9  C
10 C DECELL* IS THE CIVIL ENGINEERING LABORATORY'S ENHANCED
11 C VERSION OF THE *DESAD* PROGRAM WRITTEN BY RICHARD SKOP
12 C AND JAMES MARK OF N.R.L. (*DECELL* MEANS DESAD-CELL VERSION1)
13 C
14 C
15 C QUESTIONS OR COMMENTS ABOUT DECELL* SHOULD BE DIRECTED TO-
16 C STEVE SERGEV PHONE-(805) 982-5500
17 C
18 C
19 C COMMON /B3/ VELX(25),VELY(25)
20 C COMMON /B1/ FEJUNC,IR,DELTA1,DELTA,IRS,TFJUNC,E,ES,FCAB,HCAB,JUMP,
21 C IPJUNC,PCAB,PCABO,PCABO,HCABO,THETA,PJUNCO
22 C COMMON /B2/ HCAB,ANODE,ERJUNC,IRJUNC,DATI,DATN,P,PJUNC,CUCAB,DCAB,
23 C IFATE,NANC,ANJUNC,INHEAD,IPNNI,INTAPE,OUTAPE,ITIME,IFLG,OFLG,NIR,THE
24 C 2IAS,THETA,CUMPD,THETA,IRJUNC,RHO,TEST,NVSEG,2VEL,VELZ,PIP,ECICAB,
25 C 3E,PCAB,ZJUNC,LJUNC,PATH,ICAB,IVOPT,WCAH,IDEV,ICHECK,NDEV,NDATC
26 C COMMON /BREF/ NOCUR
27 C COMMON /TITLE/ TITLE(8),PHI,CUNITS,IUNIT,VELXP(25),VELYP(25)
28 C COMMON /PLT/ KPLOT,SIZE,IN(3),IPOINT,KCPLT
29 C COMMON /ITER/ KOUNIP,NIT,MATIER,NSTEPS,ISTEP,PERCNTV,INCPRT
30 C COMMON /PIBLN/ PI
31 C DIMENSION FEJUNC(3,44), IR(3,44), IRS(3,44), TFJUNC(3,44), PJUNC(
32 C 1,44)
33 C DIMENSION FCAB(3,51,22), HCAB(3,51,22), PJUNCS(3,44), PCAB(3,51,22
34 C 1)
35 C DIMENSION PCABE(3,51,22), PCABO(3,51,22), RCABO(3,51,22)
36 C DIMENSION ANODE(22), ERJUNC(44), IRJUNC(44), DATI(10), DATN(10), H
37 C 1(22)
38 C DIMENSION PJUNC(3,44), CUCAB(22), DCAB(22), ANJUNC(44), TEST(14)
39 C DIMENSION 2VEL(25), VELZ(25), ECICAB(22), EXPCAB(22), ZJUNC(22)
40 C DIMENSION IJUNC(22), PATH(22), ICAB(22), WCAH(22), IDEV(1000)
41 C DIMENSION ICHECK(44)
42 C DIMENSION DATI(2150,13)
43 C EQUIVALENCE (DATI(1),FEJUNC(1))
44 C INTEGER OCTAPE,ZJUNC,ERJUNC,ANJUNC,OFLG
45 C REAL IR,IRS,
46 C CALL INPURA
47 C PI=2.*3.1415926
48
49 C
50 C NIT IS THE NUMBER OF ITERATIONS ALLOWED BEFORE THE PROGRAM IS
51 C TERMINATED.
52 C IF CONVERGENCE HAS NOT BEEN REACHED BY NIT/2 ITERATIONS, AN
53 C AVERAGE OF SUCCESSIVE NORMAL POSITIONS WILL BE MADE FOR AN
54 C ADDITIONAL NIT/2 ITERATIONS.
55
56 C
57 C 5 IF(N51=0)
58 C ISCH=25
59 C BEVIND ISCH

```



```

58 KOUNTY=0
59 KOUNTY=0
60 KOUNTY=0
61 ITIME=1
62 CALL INPUT TO READ DATA AND IDENTIFY ERRORS
63
64
65
66
67
68
69
70
71
72
73
74
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114

10 CALL INPUT
11 IF (KOUNTY.NE.0) IFIRST=0
12
13 CHECK TO SEE IF ANY ERRORS IN DATA
14
15 IF (FATE.NE.0.) GO TO 305
16
17 GET HERE IF NO ERRORS -- PRINT OUT PHYSICAL CHARACTERISTICS OF ARR
18
19 ABIEE (IPRINT,310)
20 CALL PHSUUT
21
22 KMULT IS A MULTIPLIER FOR CHANGING CURRENT ANGLE THETA
23
24 KMULT=0
25 IF (IFIRST.NE.0) GO TO 15
26
27 JUMP=0--NO CURRENT JUMP=1--CURRENT
28
29 JUMP=0
30 IF (I(VOPI.EG.0) GO TO 20
31 KOUNTY=0
32 THIN=THETA/KMULT*THETAS
33 IMETA=360.*PHI-THIN
34 IFTH=0
35 IF (INSTEPS.G(1) ISIEP=1
36
37 GET HERE TO CALCULATE FORCES AND IF SUCCESSIVE APPROXIMATION ROUTE
38 NOT SATISFIED -- ZERO FORCES
39
40 DO 25 J=1,NJUNC
41 DO 25 I=1,3
42 FEJUNC(I,J)=0.
43 DO 30 N=1,NCAP
44 INNNENQUEIN
45 DO 30 N=1,NNA
46 DO 30 I=1,3
47 FCAB(I,M,N)=0.
48
49 PICK UP DISCRETE DEVICE DATA FROM TEMPORARY STORAGE TAPE AND
50 CALCULATE DEVICE FORCES -- DJNC FORCES ARE STORED IN FEJUNC --
51 UCAR FORCES IN FCAR -- E(ORCE(1) IS ROUTINE FOR CALCULATING
52 DEVICE FORCES IN DIRECTION I
53
54
55
56
57
58
59
60
61
62
63
64
65
66
67
68
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113
114

35 K=0 (ININPE,315) (DATA(K),K=1,10)
36 IF (DATA(2).EG.TEST(3)) GO TO 40
37 IF (DATA(2).EG.TEST(4)) GO TO 50
38 IF (DATA(2).EG.TEST(9)) GO TO 60
39 GO TO 35
40 N=DATA(3)

```

```

115      DC 45 J=1,3
116      I=J
117      45 FJUNC(I,K)=FJUNC(I,K)+CFORCE(I,M,K)*CDUMMY(KDUMMY)
118      GO TO 35
119      50 K=DAT(1,3)
120      45 DAT(1,1)/H(K)+1.000001
121      DC 55 J=1,3
122      I=J
123      55 FCAH(I,M,K)=FCAH(I,M,K)+CFORCE(I,M,K)
124      GO TO 35
125      C
126      C
127      C
128      60 MEWIND INTAPE
129      C
130      C
131      C
132      C
133      C
134      C
135      10 65 J=1,NCAB
136      K=J
137      INNN=NNODE(K)-1
138      DO 65 MM=1,INNN
139      M=MM
140      DO 65 II=1,J
141      I=II
142      65 FCAH(I,M,K)=FCAH(I,M,K)+CFORCE(I,M+1,K)*M(K)*0.5
143      C
144      C
145      C
146      C
147      C
148      C
149      C
150      C
151      C
152      C
153      C
154      C
155      C
156      C
157      C
158      C
159      C
160      C
161      C
162      C
163      C
164      C
165      C
166      C
167      C
168      C
169      C
170      C
171      C

```

03/07/80 11:41:06

FIN 4.6-433E

001=1

74/74

PROGRAM OF CEL

```

172 96 CONTINUE
173 C
174 C IF JUNC IS NOW DETERMINED, AND THE REACTIVE FORCES IN THE ARRAY, HCA
175 C CAN BE CALCULATED BY SUMMING FROM THE FREE ENDS TO THE FIXED ANCHO
176 C
177 C
178 DO 130 K=1,NCAB
179 IALN=NCAB-I-K
180 KPATH(INDL,K)
181 INN=NNODE(K)
182 IALJ=LJUNC(K)
183 DO 100 I=1,3
184 HCA(I,INN,K)=TFJUNC(I,IALJ)
185 IF (LJUNC(K).EQ.ZJUNC(L)) GO TO 105
186 GO TO 115
187 DO 110 I=1,3
188 HCA(I,INN,K)=HCA(I,INN,K)+RCAB(I,I,L)
189 115 CONTINUE
190 DO 125 M=1,INNN
191 H=INN-I-M
192 IF (H.EQ.0) GO TO 130
193 DO 120 I=1,3
194 HCA(I,H-K,K)=HCA(I,H,K)+PCAB(I,M-K)
195 125 CONTINUE
196 130 CONTINUE
197 C
198 C ALL REACTIVE FORCES ARE NOW DETERMINED AND THE CONFIGURATION OF TH
199 C ARRAY, PCAB AND PJUNC, CAN BE FOUND BY INTEGRATING FROM THE FIXED
200 C ANCHOR TO THE FREE ENDS -- INTEGRATION BY THE TRAPEZOIDAL RULE IS
201 C AGAIN USED
202 C
203 DO 155 N=1,NCAB
204 KPATH(N)
205 IALN=LJUNC(N)
206 INN=NNODE(N)
207 INZ=LJUNC(N)
208 DO 135 I=1,3
209 PCAB(I,INZ)=PJUNC(I,INZ)
210 DO 145 M=2,INNN
211 M=MM
212 DO 145 I=1,3
213 IF (TCAB(M,K).NE.0.) GO TO 140
214 PCAB(I,M,K)=PCAB(I,M-1,K)
215 GO TO 145
216 PCAB(I,M,K)=PCAB(I,M-1,K)+(EXCAB(M-1,K)+HCA(M-1,K))/TCAB(M-1,K)+
217 EXCAB(M,K)+HCA(M,K)/(LH(M,K))/2.
218 145 CONTINUE
219 DO 150 I=1,3
220 PJUNC(I,IALN)=PCAB(I,INNN,K)
221 155 CONTINUE
222 IF (JUMP.EQ.0) GO TO 175
223 IF (KOUNT.H.LI.NI/2) GO TO 175
224 C 170 N=1,NCAB
225 KPATH(N)
226 IALN=LJUNC(N)
227 INN=NNODE(N)
228

```

```

230      DO 160 M=1,INNN
231      DO 160 I=1,3
232      DO 165 J=1,3
233      DO 165 K=1,3
234      DO 170 CONTINUE
235      DO 175 CONTINUE
236      C
237      C      ARRAY CONFIGURATION NOW DETERMINED -- CHECK TO SEE IF IT SATISFIES
238      C      GEOMETRIC CONSTRAINTS -- SKIP THIS SECTION IF NO IR#S
239      C
240      IF (NIR.EC.0) GO TO 245
241      C
242      C      CALCULATE ERROR E
243      C
244      E2=0.
245      DO 180 M=1,NIR
246      KEN=ERJUNC(K)
247      KIN=IRJUNC(K)
248      DO 180 I=1,3
249      E2=E2+(PJUNC(I,KEN)-PJUNC(I,KIN))**2
250      E=ESQRT(E2)
251      C
252      C      COMPARE ERROR TO ACCURACY REQUIREMENTS
253      C
254      IF (E.LE.COMPD/10.) GO TO 245
255      C
256      GET HERE IF GEOMETRIC CONSTRAINTS NOT SATISFIED
257      C
258      GO TO (185,220), LEAP
259      C
260      GET HERE FIRST TIME THROUGH IMAGINARY REACTION ROUTINE
261      C
262      LEAP=2
263      KIN=0
264      EPREV=0.0
265      C
266      STORE SUCCESSFUL POSITIONS AND REACTIONS
267      C
268      190 FS=F
269      C
270      KIN=KNIN*2
271      ALLOW=MAX(F/2,1)
272      IF (INT(LEAP/2)) GO TO 218
273      CONVERGENCE - IF THE DISPLACEMENT
274      ARBITRARY DEFINITION OF SLOW CONVERGENCE - IF THE DISPLACEMENT
275      ERROR IS LARGE COMPARED TO THE CONVERGENCE TOLERANCE AND IS
276      CHANGING SLOWLY - SLOW CONVERGENCE IS INDICATED AFTER MAXITER/2
277      ITERATIONS
278      IF (KIN*GT.1.AND).E.GT.COMPD*100. .AND. EPREV.E.LI.COMPD) GO TO 195
279      LIMIT THE ITERATIONS TO SATISFY THE DISPLACEMENT TOLERANCE AT THE
280      CUTS TO MAXITER
281      IF (INT(LEAP/2)) GO TO 200
282      GO TO 210
283      195 WRITE (IPRNT,320) NINR
284      GO TO 205
285      200 WRITE (IPRNT,325) WRITE
286      205 WRITE (IPRNT,330) FILE
287      WRITE (IPRNT,335) EPREV,E*COMPD

```

```

286 IPCIVEL=PEKCNIV*100.
287 IF (NSTEIS.GI.1) WRITE (IPRNT,340) IPCTVEL
288 WRITE (IPRNT,345)
289 GO TO 300
290
291 210 EPOCH=C
292 10 215 N=1,N1H
293 KEN=ERJUNC(N)
294 N1H=INJUNC(N)
295 DO 215 I=1,3
296 PJUNCS(I,KEN)=PJUNC(I,KEN)
297 PJUNCS(I,KIN)=PJUNC(I,KIN)
298 215 IRS(I,KIN)=IR(I,KIN)
299 GO TO 225
300
301 C GET HERE ANY OTHER TIME THROUGH IMAGINARY REACTION ROUTINE
302 C SEE IF ITERATION SUCCESSFUL
303
304 220 IF (E.LT.E5) GO TO 190
305
306 C REDUCE DELTA IF NOT SUCCESSFUL INTERATION
307
308 DELTA=DELTA/2.
309
310 C CALCULATE NEW IMAGINARY AND EQUILIBRATING REACTIONS AND GO BACK TO
311 C RECALCULATE ARRAY EQUILIBRIUM
312
313 225 DO 230 N=1,N1H
314 KEN=ERJUNC(N)
315 DO 230 I=1,3
316 IR(I,KEN)=0.
317 DO 235 K=1,N1H
318 KEN=ERJUNC(K)
319 N1H=INJUNC(N)
320 DO 235 I=1,3
321 IR(I,KIN)=IRS(I,KIN)*DELTA*(PJUNCS(I,KEN)-PJUNCS(I,KIN))/E5
322 235 IPT(I,KEN)=IR(I,KEN)-IR(I,KIN)
323
324 C CHECK CHANGES IN IMAGINARY REACTIONS
325
326 DO 240 N=1,N1H
327 KIN=IRJUNC(N)
328 DO 240 I=1,3
329 IF (IR(I,KIN).NE.IRS(I,KIN)) GO TO 70
330 240 CONTINUE
331
332 C NO CHANGES -- TIME TO QUIT
333
334 CALL ERROR
335 GO TO 305
336
337 C GET HERE IF ACCURACY REQUIREMENTS SATISFIED OR NO IRS
338 C OUTPUT EQUILIBRIUM IF NO CURRENT -- IF CURRENT, FIRST CHECK TO SEE
339 C IF ACCURACY REQUIREMENT SATISFIED BY SUCCESSIVE APPROXIMATIONS
340
341 245 CONTINUE
342 IF (JUMP.C.E.0) GO TO 250
343 250 CONTINUE

```

```

343 JUM=JUMP+1
344 GO TO (255,235),JUM
345 IF (OFLG.EQ.0).OR.(OFLG.EQ.2) CALL STROUT
346 IF (KPLT.NE.0.AND.JUM.NE.1) CALL PERPLT (IVOPT,NCAH,NNUDE,PCAB,PC
347 JAHU,TITLE)
348 IF (OFLG.EQ.1).OR.(OFLG.EQ.2) CALL TAPOUT
349 IF (OFLG.EQ.1) GO TO 270
350 IF (JUM.NE.1) GO TO 270
351 DO 255 N=1,NCAH
352 I=NNENQUE(N)
353 DO 260 M=1,INNN
354 UC 260 I=1,3
355 PCABU(I,M,N)=PCAB(I,M,N)
356 HCAHU(I,M,N)=HCAH(I,M,N)
357 UC 265 N=1,NJUNC
358 UC 265 I=1,3
359 PJUNC(I,N)=PJUNC(I,N)
360 IF (KPLT.NE.0.AND.IVOPT.EQ.0) CALL PERPLT (IVOPT,NCAH,NNUDE,PCAB,
361 JPCABU,TITLE)
362 C APPLY CURRENT IF REQUIRED
363 C
364 27: IF (IVOPT.EQ.0) GO TO 300
365 JUMP=1
366 IF (JUM.EQ.1) GO TO 275
367 IF (KPLT.NE.0) CALL CPLT (IVOPT,IPRINT,PJUNC,NANC,TITLE,ANJUNC)
368 IF (ITIN.GE.THETA) GO TO 300
369 KMULT=KMULT+1
370 IF TH=1
371 C
372 C STONE EXISTING CONFIGURATION FOR COMPARISON PURPOSES
373 C
374 275 UC 280 N=1,NCAH
375 I=NNENQUE(N)
376 UC 280 M=1,INNN
377 UC 280 I=1,3
378 PCABE(I,M,N)=PCAB(I,M,N)
379 280 CONTINUE
380 C
381 C RECALCULATE FORCES
382 C
383 C IF (IFHT.EQ.0) GO TO 20
384 UC TO 15
385 C
386 C GET HERE IF CURRENT -- CHECK SUCCESSIVE APPROXIMATION ACCURACY
387 C
388 C
389 285 KOUTH=KOUTH+1
390 MACCY=SCRT(U)
391 LIMIT THE TOTAL NUMBER OF ITERATIONS TO GET THE CABLE SHAPE
392 TO HIT ITERATIONS
393 IF (KOUTH.GE.411) WRITE (IPRINT,350) KOUTH,MACCY,COMPD
394 IF (KOUTH.GE.411) CALL STROUT
395 IF (KOUTH.GE.411) GO TO 300
396 UC 245 N=1,NCAH
397 I=NNENQUE(N)
398 UC 295 M=1,INNN
399 U=0.

```

```

400      DO 230 J=1,N
401      290 U=0*(PCAB(I,M,N)-PCAB(I,M,N))**2
402      C
403      IF NOT ACCURATE STORE CONFIGURATION AND RECALCULATE FORCES
404      C
405      IF (SQRT(U).GT.COMPD) GO TO 275
406      295 CONTINUE
407      C
408      GET HERE IF POSITION ACCURATE AND OUTPUT POSITION
409      C
410      IF (LINCHMT.EQ.1.AND.ISTEP.LT.NSTEPS) CALL STROUT
411      CHECK TO SEE IF CURRENT IS TO BE INCREMENTED
412      IF (NSTEPS.EQ.1) GO TO 235
413      IF (ISTEP.LE.NSTEPS) ISTEP=ISTEP+1
414      IF (ISTEP.GT.NSTEPS) GO TO 255
415      GO TO 275
416      C
417      GO BACK FOR MORE DATA
418      C
419      300 IFIRST=1
420      COUNT=0
421      GO TO 10
422      305 CONTINUE
423      WRITE (11PHN1,355)
424      GO TO 5
425      C
426      310 FORMAT (///,5X,'18%NO ERRORS DETECTED')
427      315 FORMAT (F4.3A4,RE15.8)
428      320 FORMAT (1P1'23%SLOW CONVERGENCE AFTER 15,11% ITERATIONS/')
429      325 FORMAT (1P1'18%NO CONVERGENCE IN 15,11% ITERATIONS/')
430      330 FORMAT (11H CASE TITLE/1X,10(1H=)/1X,8A10/)
431      335 FORMAT (24H PREVIOUS ERROR VALUE = ,E15.5/24H PRESENT ERROR VALUE
432      1 = ,E15.5/33H ACCEPTABLE ERROR (COMP VALUE) = ,E15.5)
433      340 FORMAT (1/23H PRESENT VALUE OF CURRENT = ,14.22H PERCENT OF FULL VA
434      1LUE)
435      345 FORMAT (//39H PARAMETRIC CASE TERMINATED, SEE MANUAL)
436      350 FORMAT (//1X,30HPHOGHAM DID NOT CONVERGE AFTER 15,1X,38HITERATIONS,
437      1 PARAMETRIC CASE TERMINATED//24H BEST ACCURACY OBTAINED = ,E15.4/2
438      27H DESIRED ACCURACY (COMP) = ,E15.4//28H APPROXIMATE RESULTS PRIN
439      31ED/1X,27(1P=))
440      355 FORMAT (11H)
441      END

```

CARD NO. SEVERITY DETAILS DIAGNOSIS OF PROBLEM

254 I AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.
 341 I THIS IF DEGENERATES INTO A SIMPLE TRANSFER TO THE LABEL INDICATED.
 344 I AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.

```

1      *DECK INFORM
      SUBROUTINE INFORM
      =====
      C
      C
      C      THIS SUBROUTINE IS USED TO INFORM THE USER OF UPDATES THAT HAVE
      C      BEEN ADDED TO DECEL THAT MAY AFFECT INPUT OR CALCULATIONS OR
      C      OUTPUT.
      C      ANY NEW UPDATES SHOULD BE DESCRIBED HERE BY ADDING TO THE
      C      INFORMATIVE PRINT STATEMENTS
      C
      C
      C      =====
      C      PRINT 5
      C      PRINT 10
      C      RETURN
      C
      C
      C      5 FORMAT (1P1,26H DECEL UPDATE INFORMATION/2X,25(1H=)/)
      C      10 FORMAT (176H THIS IS THE JANUARY 1990 VERSION OF DECEL AS DESCRIBE
      C      10 IN THE USERS MANUAL/26H NO UPDATES HAVE BEEN ADDED)
      C
      C      END
      INF 1
      INF 2
      INF 3
      INF 4
      INF 5
      INF 6
      INF 7
      INF 8
      INF 9
      INF 10
      INF 11
      INF 12
      INF 13
      INF 14
      INF 15
      INF 16
      INF 17
      INF 18
      INF 19-
  
```


03/07/80 11.41.06

FIN 4.6+433E

FUNCTION CFORCE 74/74 UPT=1

```

1  *DECK CFORCE
   FUNCTION CFORCE (I,M,N)
   C
   C THIS ROUTINE CALCULATES THE FORCE/LENGTH IN DIRECTION I AT NODE M
   C ON CABLE A USING THE NORMAL DRAG FORCE APPROXIMATION
   C
   COMMON /B3/ VELX(25),VELY(25)
   COMMON /B1/ FEJUNC,IR,DELTA,IRS,IFJUNC,E,ES,FCAB,RCAB,JUMP,CFO
   LPJUNCS,PCAB,PLABE,PCABO,RCABO,THETA,PJUNCO
   COMMON /B2/ NCAB,NNODE,ERJUNC,IRJUNC,DALI,DATN,P,PJUNC,CCAB,UCAB,CFO
   IFATE,NANJ,ANJUNC,IHEAD,IPRNT,INTAPE,OUTAPE,ITIME,IFLG,OFLG,NIR,THECFO
   ZIAS,THETA,CUMPO,THETAB,NJUNC,RHO,TEST,NVSEG,ZVEL,VELZ,PIP,ECICAB,CFO
   3EXPCAB,ZJUNC,LJUNC,PATN,ICAB,IVOPT,WCAB,IDEV,ICHECK,NDEV,NDATC
   COMMON /TANDRE/ TCAB(22),TUCAB(1000)
   COMMON /PIELN/ PI
   DIMENSION FEJUNC(3,44), IR(3,44), IRS(3,44), IFJUNC(3,44), PJUNCO(CFO
   13,44)
   DIMENSION FCAB(3,51,22), RCAB(3,51,22), PJUNCS(3,44), PCAB(3,51,22CFO
   18
   1)
   DIMENSION PCABE(3,51,22), PCABO(3,51,22), RCABU(3,51,22)
   DIMENSION NNODE(22), ERJUNC(44), IRJUNC(44), DALI(10), DATN(10), MCFO
   21
   1(22)
   DIMENSION PJUNC(3,44), CCAB(22), DCAB(22), ANJUNC(44), TEST(14)
   DIMENSION ZVEL(25), VELZ(25), ECICAB(22), EXPCAB(22), ZJUNC(22)
   DIMENSION LJUNC(22), PATN(22), ICAB(22), WCAB(22), IDEV(1000)
   DIMENSION ICHECK(44)
   DIMENSION WICAB(3), VADNM(3), PSPACE(3)
   DIMENSION NN(3), VT(3)
   INTEGER OUTAPE,ZJUNC,ERJUNC,ANJUNC,OFLG
   INTEGER PATH
   REAL IR,IRS
   C
   C CALCULATE THE WEIGHT/LENGTH VECTOR
   C
   WICAB(1)=0.
   WICAB(2)=0.
   WICAB(3)=WCAB(N)
   C
   C CHECK TO SEE IF CURRENT OR NO CURRENT
   C
   JUM=JUMP+1
   GO TO (5,10), JUM
   C
   C GET HERE IF NO CURRENT
   C
   5 CFORCE=WICAB(1)
   RETURN
   C
   C GET HERE IF CURRENT
   C
   C CALCULATE LOCATION OF NODE IN SPACE
   C
   10 UC 15 K=1,3
   IF PSPACE(K)=P(CAB(K),M,N)
   C
   C IF (IVOPT.EQ.3) CALL INTVEL (W,PSPACE)
   C
   C IF (IVOPT.EQ.3) GO TO 25
   UC 20 K=1,3
   WIK(WIK)=VELCC(K,PSPACE)

```

03/07/80 11:41:06

FTP 4.6*433E

FUNCTION CFCRCE 74/74 OPT=1

```

25 CONTINUE
C
C CALCULATE THE TANGENTIAL PROJECTION OF THE CURRENT ON THE CABLE
C
VPRCJ=0.
DC 30 KK=1,3
N=KK
VPROJ=VPRCJ*W(K)*HCAB(K,M,N)/TCAB(M,N)
C
C CALCULATE THE NORMAL COMPONENT OF THE CURRENT AND ITS MAGNITUDE
C
DC 35 KK=1,3
N=KK
VNORM(K)=W(K)-VPROJ*HCAB(K,M,N)/TCAB(M,N)
VMAG=SQRT(VNORM(1)**2+VNORM(2)**2+VNORM(3)**2)
C
C CALCULATE THE FORCE/LENGTH
C
C CALCULATE TANGENTIAL COMPONENT OF CURRENT AND ITS MAGNITUDE
VT(1)=W(1)-VNORM(1)
VT(2)=W(2)-VNORM(2)
VT(3)=W(3)-VNORM(3)
VIM=SQRT(VT(1)**2+VT(2)**2+VT(3)**2)
CFORCE=I*CAH(1)*HPO*.5*(UCAB(N)/12.)*EXCAB(M,N)*(VMAG*VNORM(1)*CUCFO
CAH(N)+VIM*V(1)*TUCAB(N)*PI)
RETURN
END

```

CARD NO. SEVERITY DETAILS DIAGNOSIS OF PROBLEM

42 I AM IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.

```

1      *DECK EFORCE
2      FUNCTION EFORCE (I,M,N)
3
4      C
5      C
6      C
7      C
8      C
9      C
10     C
11     C
12     C
13     C
14     C
15     C
16     C
17     C
18     C
19     C
20     C
21     C
22     C
23     C
24     C
25     C
26     C
27     C
28     C
29     C
30     C
31     C
32     C
33     C
34     C
35     C
36     C
37     C
38     C
39     C
40     C
41     C
42     C
43     C
44     C
45     C
46     C
47     C
48     C
49     C
50     C
51     C
52     C
53     C
54     C
55     C
56     C
57     C

```

THIS ROUTINE CALCULATES THE DEVICE FORCES IN DIRECTION I
USING THE NORMAL DRAG APPROXIMATION FOR IN-LINE DEVICES

COMMON /B3/ VELX(25),VELY(25)
COMMON /B1/ FEJUNC,IR,DELTA1,DELTA2,IRHS,FEJUNC,E,ES,FCAB,DCAB,JUMP,EFO
IPJUNC,PCAB,PCABF,PCABU,MCABO,THETA,PJUNCO
COMMON /B2/ NCAB,NODE,ERJUNC,IRJUNC,DATA1,DATN,F,PJUNC,COCAB,DCAB,EFO
IFATE,NANC,ANJUNC,IHEAD,IPRNI,INTAPE,OUTAPE,ITIME,IFLO,OFLO,NIR,THEEFO
ZIAS,THETA,SCUPPD,THETAB,NJUNC,RHO,TEST,NVSEG,ZVEL,VELZ,PIP,ECICAB,EFO
JEXPCAB,ZJUNC,LJUNC,PAIR,ICAB,IVOPT,WCAB,IDEV,ICHECK,NDEV,NOATC
COMMON /TANDRG/ TDCAB(22),TDCAB(1000)
COMMON /PIULK/ PI
DIMENSION FEJUNC(3,44), IR(3,44), IRS(3,44), IFJUNC(3,44), PJUNC(16
13,44)
DIMENSION FCAB(3,51,22), MCAB(3,51,22), PJUNC(3,44), PCAB(3,51,22)EFO
1)
DIMENSION PCABF(3,51,22), PCABO(3,51,22), RCAB(13,51,22)
DIMENSION ANODE(22), ERJUNC(44), IRJUNC(44), DATA(10), DAIN(10), HEFO
1(22)
DIMENSION PJUNC(3,44), CDCAB(22), DCAB(22), ANJUNC(44), TEST(14)
DIMENSION ZVEL(25), VELZ(25), ECICAB(22), EXPCAB(22), ZJUNC(22)
DIMENSION LJUNC(22), PAIR(22), ICAB(22), WCAB(22), IDEV(1000)
DIMENSION ICHECK(44)
DIMENSION WTEL(3), VNCR*(3), PSPACE(3)
DIMENSION ***(3), WTCAB(3), VT(3)
INTEGER OUTAPE,ZJUNC,ERJUNC,ANJUNC,OFLO
INTEGER PATH
REAL IR,IRS

INITIALIZE LOCAL VARIABLES

WTCAB(1)=0.
WTCAB(2)=0.
WTCAB(3)=PCAB(N)
DC=DATA(8)
IF (DATA(4).EQ.1) DD=DATA(8)/12.
DL=DATA(5)
DND=DATA(7)

CALCULATE THE WEIGHT VECTOR OF A DEVICE

WTEL(1)=(
WTEL(2)=1.
WTEL(3)=DATA(6)-DL*WTCAB(3)

CHECK TO SEE IF CURRENT ON NO CURRENT

JLM=JUMP*
GO TO (5+1), JLM

SET HERE IF NO CURRENT

EFORCE=WTEL(1)
RETURN

FUNCTION EFFORCE 74/74 OP1=1 PAGE 3

03/07/80 11.41.06

FTN 4.6433E

115

END

EFO 115-

CARD NO. SEVERITY DETAILS DIAGNOSIS OF PROBLEM

52 1
74 1

AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.
AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.

03/07/80 11.41.06

FTN 4.00433E

SUBROUTINE LHRUM 747% OPT=1

CARD NO. SEVERITY DETAILS DIAGNOSIS OF PROBLEM

31 1 AN IP STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.

```

1      *ULCK EXCAR
      FUNCTION EXCAR (M,K)
2
3      C      THIS ROUTINE CALCULATES (1 - STRAIN) AT NODE M OF CAULE K
4
5      C
6      C      COMMON /H3/ VELX(25),VELY(25)
7      C      COMMON /B1/ FEJUNC,IR,DELTAI,DELTA,IRS,IFJUNC,E,ES,FCAB,MCAB,JUMP,EXC
8      C      IPJUNC,PCAB,PCABE,PCABO,MCABO,THETA,PJUNCO
9      C      COMMON /H2/ NCAB,NCODE,ERJUNC,IRJUNC,DATI,DATM,PJUNC,CUCAB,DCAB,EXC
10     C      IFATE,NANC,ARJUNC,THEAD,IPRNT,INTAPE,OUTAPE,ITIME,IFLG,OFLG,NIR,THEXC
11     C      2IAS,THEIAL,CUMPD,THEIAB,NJUNC,RHU,TEST,NVSEG,ZVEL,VELZ,PIPI,ECICAB,EXC
12     C      3EXPCAB,ZJUNC,LJUNC,PATH,ICAB,IVOPT,MCAB,IDEV,ICHECK,NDEV,NDATC
13     C      DIMENSION FEJUNC(3,44), IH(3,44), IAS(3,44), IFJUNC(3,44), PJUNCO(13,44)
14     C      DIMENSION FCAB(3,51,22), MCAB(3,51,22), PJUNCS(3,44), PCAB(3,51,22), EXC(13,44)
15     C      DIMENSION PCABE(3,51,22), PCABO(3,51,22), MCABO(3,51,22)
16     C      DIMENSION NNODE(22), ERJUNC(44), IRJUNC(44), DATI(10), DATM(10), MEXC(18)
17     C      1(22)
18     C      DIMENSION PJUNC(3,44), CCAB(22), DCAB(22), ANJUNC(44), TEST(14)
19     C      DIMENSION ZVEL(25), VELZ(25), ECICAB(22), EXPCAB(22), ZJUNC(22)
20     C      DIMENSION LJUNC(22), PATH(22), ICAB(22), MCAB(22), IDEV(1000)
21     C      DIMENSION ICHECK(44)
22     C      INTEGER OUTAPE,ZJUNC,ERJUNC,ANJUNC,OFLG
23     C      INTEGER PATH
24     C      REAL IR,IRS
25     C      IF (EXPCAB(K).EQ.0.) GO TO 5
26     C      EXCAR=1.-(ICAB(M,K)/ECICAB(K))*EXPCAB(K)
27     C      RETURN
28     C      5 EXCAR=1.
29     C      RETURN
30     C      END
31
32

```


1 TEST(7)=4H EOD
2 TEST(10)=4H NJC
3 TEST(11)=4H VEL
4 TEST(12)=4H NCAT
5 TEST(13)=4H LUN
6 TEST(14)=4H EOP

PIP=PI/180.
INTAPE=24

ISCR=25
IREAD=60
IPRNT=61
IFEUD=0
IAUEV=0
MDATC=0
KFLG=0

NCJUNC=0
KCUP=0
DO 5 I=1,1000
5 IODCAR(I)=0.
DO 10 I=1,44
10 ICHECK(I)=0
DO 15 J=1,22
15 ICAB(I)=0
NANC=0
IFRHO=0
IFJNC=0
NIN=0
IOW=1
IPNCH=8
KPLT=0
20 FATE=0.
KCPLT=0
KPPLT=0

C CHECK LOGICAL UNITS

IF (TIME.G1.1) GO TO 50
ITIME=2

IF READING FROM TAPE LUN MUST BE INCLUDED AS A CARD

HEAD (IREAD*620) TITLEM

SAVE INPUT ON TAPF

IRAD=0
IFURN=1
WRITE (ISCH) IFORM,IRAD
WRITE (ISCH*620) TITLEM
IF (EOP(IREAD)) 25,30

25 STOP
30 DECODE (B*625,TITLEM) IST1,IST2

C CHECK IF FIRST CARD IS LUN OR MAIN TITLE CARD

IF (IST2.EQ.3HLUN) GO TO 35

INP 58
INP 59
INP 60
INP 61
INP 62
INP 63
INP 64
INP 65
INP 66
INP 67
INP 68
INP 69
INP 70
INP 71
INP 72
INP 73
INP 74
INP 75
INP 76
INP 77
INP 78
INP 79
INP 80
INP 81
INP 82
INP 83
INP 84
INP 85
INP 86
INP 87
INP 88
INP 89
INP 90
INP 91
INP 92
INP 93
INP 94
INP 95
INP 96
INP 97
INP 98
INP 99
INP 100
INP 101
INP 102
INP 103
INP 104
INP 105
INP 106
INP 107
INP 108
INP 109
INP 110
INP 111
INP 112
INP 113
INP 114

5. BROUINE INPUT 79/74 OPT=1

[illegible]

03/07/80 11.41.06

FTN 4.6.433E

SUBROUTINE INPUT 74/74 OPT=1

```

230      C      105 DC 110 1=1,2
          ID=DAT1(4)
          IF (ID.EQ.1) GO TO 115
          110 CONTINUE
          IBAU=18
          GO TO 545
235      115 IF ((DAT1(3).LT.1.) .OR. (DAT1(3).GT.22.)) IBAU=17
          IF ((DAT1(3).LT.1.) .OR. (DAT1(3).GT.22.)) GO TO 545
          INDEX=INDEX+1
          IF ((INDEX.LT.1) .OR. (INDEX.GT.1000)) IBAU=19
          IF ((INDEX.LT.1) .OR. (INDEX.GT.1000)) GO TO 545
          IF ((DAT1(7).LT.0.) .OR. (DAT1(8).LT.0.)) IBAU=22
          IF ((DAT1(7).LT.0.) .OR. (DAT1(8).LT.0.)) GO TO 545
          IF ((DAT1(4).EQ.2.) .AND. (DAT1(9).NE.0.)) IBAU=21
          IF ((DAT1(4).EQ.2.) .AND. (DAT1(9).NE.0.)) GO TO 545
          IF ((DAT1(4).EQ.1.) .AND. (DAT1(9).LE.0.)) IBAU=20
          IF ((DAT1(4).EQ.1.) .AND. (DAT1(9).LE.0.)) GO TO 545
          IF ((DAT1(10).LT.0.) IBAU=22
          IF ((DAT1(10).LT.0.) GO TO 545
          TDCAB(INDEX)=EX
          GO TO 530
240      C      GET HERE IF CAB CARD READ
          C
          C
          C
250      120 INDEX=DAT1(3)
          IF (IFLG.EQ.0) READ (IREAD,620) STORE
          IF (IFLG.EQ.1) READ (IREAD,645) TDCAB(INDEX)
          C
          C      SAVE INPUT ON TAPE
          C
          IBAU=0
          IFORM=3
          WRITE (ISCH) IFORM,IBAU
          IF (IFLAG.EQ.0) WRITE (ISCR,620) STORE
          IF (IFLAG.EQ.0) WRITE (ISCR,645) TDCAB(INDEX)
          DECODE (10,640,STORE) TDCAB(INDEX)
          IF ((DAT1(3).LT.1.) .OR. (DAT1(3).GT.22.)) IBAU=9
          IF ((DAT1(3).LT.1.) .OR. (DAT1(3).GT.22.)) GO TO 545
          IF ((DAT1(4).EQ.DAT1(5)) IBAU=10
          IF ((DAT1(4).EQ.DAT1(5)) GO TO 545
          IF ((DAT1(4).GT.44.) .OR. (DAT1(5).GT.44.)) IBAU=11
          IF ((DAT1(4).GT.44.) .OR. (DAT1(5).GT.44.)) GO TO 545
          IF ((DAT1(4).LT.1.) .OR. (DAT1(5).LT.1.)) IBAU=11
          IF ((DAT1(4).LT.1.) .OR. (DAT1(5).LT.1.)) GO TO 545
          IF ((DAT1(7).LE.0.) .OR. (DAT1(8).LE.0.)) IBAU=15
          IF ((DAT1(7).LE.0.) .OR. (DAT1(8).LE.0.)) GO TO 545
          IF ((DAT1(7).LE.0.) .OR. (DAT1(8).LE.0.)) IBAU=15
          IF ((DAT1(7).LE.0.) .OR. (DAT1(8).LE.0.)) GO TO 545
          IF ((EX.LT.0.) .OR. (DAT1(10).LT.0.)) IBAU=13
          IF ((EX.LT.0.) .OR. (DAT1(10).LT.0.)) GO TO 545
          IF ((DAT1(10).EQ.0.) .AND. (EX.NE.0.)) IBAU=14
          IF ((DAT1(10).EQ.0.) .AND. (EX.NE.0.)) GO TO 545
          IF ((DAT1(10).NE.0.) .AND. (EX.EQ.0.)) IBAU=15
          IF ((DAT1(10).NE.0.) .AND. (EX.EQ.0.)) GO TO 545
          IF ((INSEG.LT.1.) .OR. (INSEG.GT.50)) IBAU=10
          IF ((INSEG.LT.1.) .OR. (INSEG.GT.50)) GO TO 545

```

115

03/07/80 11.41.06

FTN 4.6.633E

SUBROUTINE INPUT 74/74 OPT=1

```

IF (ICAB(INDEX).NE.0) GO TO 555
ICAB(INDEX)=1
INDEX=DATI(5)
IF (ICHECK(INDEX).NE.0) IBAD=31
IF (ICHECK(INDEX).NE.0) GO TO 550
ICHECK(INDEX)=1

```

```

C GET HERE IF DATA OK
C
C

```

```

INDEX=DATI(3)
ZJUNC(INDEX)=DATI(4)
LJUNC(INDEX)=DATI(5)

```

```

125 MCODE(INDEX)=NSEG+1
WCAB(INDEX)=DATI(6)
CDCAB(INDEX)=DATI(7)
DCAB(INDEX)=DATI(8)

```

```

H(INDEX)=DATI(9)/NSEG
ECICAB(INDEX)=DATI(10)
EXPCAB(INDEX)=EX
GO TO 500

```

```

C GET HERE IF UEN CARD READ
C
C

```

```

130 IF (DATI(3).LE.0.) IBAD=25
IF (DATI(3).LE.0.) GO TO 545
IFRHO=IFRHO+1

```

```

IF (IFRHO.GT.1) IBAD=36
IF (IFRHO.GT.1) GO TO 565
WHU=DATI(3)
GO TO 50

```

```

C GET HERE IF EOD CARD READ
C
C

```

```

135 IF EOD=IF EOD+1
DC 140 J=1,10
140 DATI(INOW,J)=DATI(J)
IMAX=INOW

```

```

IF (FATE.NE.0.) GO TO 450
IF (IFLG.EQ.1) GO TO 145
GO TO 335

```

```

145 IREAD=ISAVI
IFLG=0
GO TO 335

```

```

C GET HERE IF NUNC CARD READ
C
C

```

```

150 IF (DATI(3).LI.2.) OR (DATI(3).GT.44.) IBAD=5
IF (DATI(3).LI.2.) OR (DATI(3).GT.44.) GO TO 545
IF JNC=IF JNC+1

```

```

IF (IF JNC.GT.1) IBAD=35
IF (IF JNC.GT.1) GO TO 565
NCJUNC=DATI(3)
GO TO 50

```

```

C GET HERE IF NCAT CARD READ
C
C

```

```

155 NCATC=NCATC+1

```

```

INP 286
INP 287
INP 288
INP 289
INP 290
INP 291
INP 292
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INP 294
INP 295
INP 296
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INP 332
INP 333
INP 334
INP 335
INP 336
INP 337
INP 338
INP 339
INP 340
INP 341
INP 342

```

```

C
C
C
345      DEFINE CURRENT UNITS OPTION AND CONVERSION FACTOR
C
C      IUNIT=DATI(10)+1.E-9
C      CUNITS=1.
C      IF (IUNIT.EQ.1) CUNITS=0.01943
C      IF (IUNIT.EQ.2) CUNITS=0.5921
C      DEVT=DATI(18)
C      NSTEPS=1
C      ISTEP=1
C      PERCENTIV=0.
C      INCPNT=0
C      IF (EX.NE.0.0) NSTEPS=EX
C      IF (FLCAT(NSTEPS).NE.EA.AND.NSTEPS.GT.1) INCPNT=1
C      IF (DATI(17).NE.0.0) IFUNC=8H      YES
C      NCUR=DATI(15)
C      HEAD (IHEAD,620) TITLE
C
C      SAVE INPUT ON TAPE
C
C      IBAD=0
C      IFORM=1
C      WRITE (ISCR,620) TITLE
C      IF (INDATC.NE.IFEOD) GO TO 615
C
C      HEAD ANGLE IN DEGREES BETWEEN MAGNETIC NORTH AXIS AND X-AXIS OF
C      ARRAY REFERENCED COORDINATE SYSTEM, ANGLE IS POSITIVE CLOCKWISE
C      AND IS REFERENCED WITH RESPECT TO THE MAGNETIC NORTH AXIS.
C
C      PHIDATI(6)
C      GO TO 45
C      107 IFCOMP=0
C      INDAT=0
C      IFVEL=0
C      IFANG=0
C      IF ((DATI(13).LT.0.0).OR.(DATI(3).GT.3.)) IBAD=26
C      IF ((DATI(13).LT.0.0).OR.(DATI(3).GT.3.)) GO TO 545
C      IVOP1=DATI(13)
C      IF (IVOP1.EQ.3) NSTA=DATI(4)
C      IF (INDATC.EQ.1) GO TO 165
C      IF (IVOP1.EQ.0) GO TO 180
C      IF (KFLG.EQ.0) GO TO 170
C      IF (IVOP1.EQ.KCUR) GO TO 180
C      GO TO 610
C      165 IF (IVOP1.EQ.0) GO TO 175
C      170 KFLG=1
C      KCUR=IVOP1
C      GO TO 180
C      175 KFLG=0
C
C      HEAD ONE INPUT RECORD FROM PARAMETRIC STUDY SOURCE DECK
C
C      180 HEAD (IHEAD,620) STORE
C      185 CALL MACA11
C      STOP

```


03/07/80 11.41.06

FIN 4.6+433E

SUBROUTINE INPUT 74/74 OPT=1

```

      HANG=HANG+1
      IF (HANG.GT.1) IBAU=40
      IF (HANG.GT.1) GO TO 505
      GO TO 180
    C
    C GET HERE IF COMP CARD READ
    C
    C
    230 IFCOMP=IFCOMP+1
      CALL SWITCH
      IF (IFCOMP.EQ.1) NCOMP=0
      IF (DATI(3).LE.0.) IBAU=27
      IF (DATI(3).LE.0.) GO TO 545
      NCOMP=NCOMP+1
      IF (NCOMP.GT.1) (BAU=37
      IF (NCOMP.GT.1) GO TO 565
      COMPD=DATI(3)
      NI=200
      IF (DATI(4).NE.0.0) NI=DATI(4)
      MAXIEK=1000
      IF (DATI(5).NE.0.0) MAXIEH=DATI(5)
      GO TO 180
    C
    C GET HERE TO PLOT VELOCITY FIELD
    C
    C
    235 IF (KPLI.EQ.0) CALL PLOTS (0.0,6LNPFIL)
      KPLI=1
      KCPLI=1
      CALL SWITCH
      ZUP=DATI(3)
      ZDN=DATI(4)
      DZ=DATI(5)
      YIN=DATI(6)
      YMIN=DATI(7)
      YMAX=DATI(8)
      YMIN=DATI(9)
      YMAX=DATI(10)
      ANG=EXX
      IF (ANG.LE.0.0 OR ANG.GE.180.) ANG=90.
      NY=NNSEG
      IF (NY.LE.0) NY=6
    C
    C FIND MAX AND MIN FOR DEFAULT
    C
    C
      DEFAULT=XMIN+YMIN+XMAX+YMAX
      IF (DEFAULT.NE.0.) GO TO 180
      BIG=1.E10
      XMIN=BIG
      YMIN=BIG
      XMAX=-BIG
      YMAX=-BIG
      DO 240 ISF=1,NANIC
        ISA=ANJUNC(ISF)
        XMIN=AMIN(XMIN,XJUNC(ISA))
        YMIN=AMIN(YMIN,YJUNC(ISA))
        XMAX=AMAX(XMAX,XJUNC(ISA))
        YMAX=AMAX(YMAX,YJUNC(ISA))
      240 X=AUS(XMAX-XMIN)

```

```

515      HY=ABS(YMAX-YMIN)
      IF (RY.EQ.0.) YMIN=YMIN-0.15*RX
      IF (RY.EQ.0.) YMAX=YMAX+0.15*RX
      IF (MX.EQ.0.) XMIN=XMIN-0.15*RY
      IF (MX.EQ.0.) XMAX=XMAX+0.15*RY
      GO TO 180

520      C
      C      GET HERE FOR PERSPECTIVE PLOTTING
      C
      C      245 CALL SWITCH
      C      IF OPT=DATI(3)*.01
      C      SIZE=DATI(4)
      C      IH(1)=DATI(5)
      C      IH(2)=DATI(6)
      C      IH(3)=DATI(7)
      C      DEFAULT=IH(1)+IH(2)+IH(3)
      C      IF (DEFAULT.NE.0.0) GO TO 250
      C      IH(1)=302
      C      IH(2)=120
      C      IH(3)=90
      C      250 IF (KPLT.EQ.0) CALL PLOIS (0.0,6LNPFIL)
      C      KPLT=1
      C      KPLT=1
      C      GO TO 180

530      C
      C      GET HERE IF PARAMETERS ARE BEING CHANGED
      C      LOCATE RECORD TO BE CHANGED AND BRANCH
      C
      C      255 IF (INDAT.NE.0) GO TO 260
      C      READ (INTAPE,660) ((DATI(I,J),J=1,10),I=1,IRMAX)
      C      REWIND INTAPE
      C      (KDATE=1
      C      260 DO 265 I=1,IRMAX
      C      IF (DATI(1).EQ.DATI(1ROW,1)).AND.(DATI(2).EQ.DATI(1ROW,2))) GO
      C      110 270
      C      IF (DATI(1ROW,2).EQ.TEST(9)) GO TO 605
      C      265 CONTINUE
      C      270 DO 275 J=1,10
      C      275 DATI(J)=DATI(1ROW,J)
      C      DO 280 J=1,10
      C      IF (DATI(2).EQ.TEST(1)) GO TO (280,285,290,295,305), I
      C      280 CONTINUE
      C      C      GET HERE IF ANC CARD READ
      C      C
      C      285 IF (DATI(3).NE.DATN(3)) GO TO 605
      C      CALL SWITCH
      C      INDEX=DATI(3)
      C      GO TO 90

550      C
      C      GET HERE IF DUNC CARD READ
      C      C
      C      290 IF (DATI(3).NE.DATN(3)) GO TO 605
      C      CALL SWITCH
      C      DATI(4)=2
      C      IF ((DATI(7).LT.0.).OR.(DATI(8).LT.0.)) INAD=24

```


[illegible]

```

685      VELZ(I)=VELZ(J)
686      VELZ(J)=TEMP
687      345 CONTINUE
688      C
689      C
690      C
691      C
692      C
693      C
694      C
695      C
696      C
697      C
698      C
699      C
700      C
701      C
702      C
703      C
704      C
705      C
706      C
707      C
708      C
709      C
710      C
711      C
712      C
713      C
714      C
715      C
716      C
717      C
718      C
719      C
720      C
721      C
722      C
723      C
724      C
725      C
726      C
727      C
728      C
729      C
730      C
731      C
732      C
733      C
734      C
735      C
736      C
737      C
738      C
739      C
740      C
741      C

```

123

INP 742	INP 743	INP 744	INP 745	INP 746	INP 747	INP 748	INP 749	INP 750	INP 751	INP 752	INP 753	INP 754	INP 755	INP 756	INP 757	INP 758	INP 759	INP 760	INP 761	INP 762	INP 763	INP 764	INP 765	INP 766	INP 767	INP 768	INP 769	INP 770	INP 771	INP 772	INP 773	INP 774	INP 775	INP 776	INP 777	INP 778	INP 779	INP 780	INP 781	INP 782	INP 783	INP 784	INP 785	INP 786	INP 787	INP 788	INP 789	INP 790	INP 791	INP 792	INP 793	INP 794	INP 795	INP 796	INP 797	INP 798
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```

CHECK ON CONTINUITY OF CABLE NUMBERING AND COUNT CABLES

395 NCAB=ICAB(22)
   UC 400 N=1:21
   NCAB=NCAB+ICAB(N)
   J=ICAB(N)-ICAB(N+1)
   IF (J.L1.0) GO TO 580
400 CONTINUE
   IF (NCAB.EQ.3) GO TO 580

CHECK ON CONTINUITY OF JUNCTION NUMBERING AND COUNT JUNCTIONS

NJUNC=ICHECK(44)
UC 405 N=1:43
NJUNC=NJUNC+ICHECK(N)
J=ICHECK(N)-ICHECK(N+1)
IF (J.L1.0) GO TO 585
405 CONTINUE

SORT DEVICES ON CABLE NO.(DATI(3))
AND DISTANCE FROM 0 JUNCTION(DATI(10))

NDEV=INDEX
CALL SORT (NDEV,INTAPE)
IF (FATE.EU.0.) GO TO 410
GO TO 530

GET HERE IF ARRAY NUMBERED CORRECTLY
CHECK TO SEE IF NIR CONSISTENT

410 NIRC=NCAB+NANC-NJUNC
   IF (NIRC.NE.NIRC) GO TO 590

GET HERE TO MAKE FINAL CHECK ON INTAPE

415 I=1
420 DO 425 J=1:10
425 DATI(J)=DATI(1,J)
   I=I+1
   IF (DATI(2).EG.TEST(1)) GO TO 430
   IF (DATI(2).EG.TEST(3)) GO TO 435
   IF (DATI(2).EG.TEST(4)) GO TO 440
   IF (DATI(2).EG.TEST(5)) GO TO 445
   IF (DATI(2).EG.TEST(9)) GO TO 450
   GO TO 420

GET HERE FOR IH

430 I1=DATI(3)
   J2=DATI(4)
   IF (I1.LE.NJUNC) IBAD=45
   IF (I1.LE.NJUNC) GO TO 505
   IF (I2.GT.NJUNC) IBAD=46
   IF (I2.GT.NJUNC) GO TO 595
   IF (I1.GT.NJUNC) IBAD=47
   IF (I1.GT.NJUNC) GO TO 595

```

11.01.06

03/07/80

FIN 4.6+433E

SUBROUTINE INPUT 74/74 OPT=1

```

      800      GO TO 420
      C      GET HERE FOR CJNC
      C
      805      435 ID=UATI(3)
      IF (ID.GT.NJUNC) IBAD=51
      IF (ID.GT.NJUNC) GO TO 595
      GO TO 420
      C
      C      GET HERE FOR UCAB
      C
      810      440 ID=UATI(3)
      IF (ID.GT.NCAB) IBAD=49
      IF (ID.GT.NCAB) GO TO 595
      PL=H(ID)*(NMODE(ID)-1)
      IF (UATI(10).GE.HL) IBAD=50
      IF (UATI(10).GE.HL) GO TO 595
      GO TO 420
      C
      C      GET HERE FOR CAB
      C
      820      445 ID=UATI(4)
      IF (ID.GT.NJUNC) IBAD=48
      IF (ID.GT.NJUNC) GO TO 595
      GO TO 420
      C
      C      GET HERE FOR EOD
      C
      825      450 WRITE (INTAPE,660) ((UATI(I,J),J=1,10),I=1,(NMAX)
      REMIND INTAPE
      IF (INDATC.NE.0.AND.FATE.EQ.0.) RETURN
      IF (FATE.EQ.0.) GO TO 455
      GO TO 50
      C
      C      GET HERE IF ALL OK AND CALCULATE PATH
      C
      C      K IS CABLE COUNTER
      C
      835      455 K=0
      C
      C      LOOP=1 LOOKING FOR CABLE'S LEAVING ANCHORS
      C
      C      LOOP=1
      C
      840      JMLP REMEMBERS FIRST VALUE OF K ON A LEVEL OF TREE
      C
      C      JMLP=1
      C
      C      JMAX REMEMBERS NUMBER OF CABLES ON A LEVEL OF ICPOGRAPHIC TREE
      C
      C      JMAX=NAC
      C
      845      IF (LOOP.EQ.1) GO TO 465
      C
      850      JMAX=K
      IF ((LOOP.EQ.1).AND.(K.NE.1)) GO TO 600
      C
      C      IF ((LOOP.EQ.2).AND.(JMLP.EQ.JMLP)) GO TO 600
      C
      C      IF (K.EQ.NCAB) GO TO 50
      C
      855      LOOP=2
      JMLP=JMLP

```

```

      DC 495 J=JMIN,JMAX
      C
      C LOOKING FOR CABLES LEAVING A JUNCTION
      C
      DC 490 N=1,NCAH
      GO TO (470,475), LOOP
      470 IF (ZJUNC(N).EQ.ANJUNC(J)) GO TO 480
      GO TO 490
      475 IPATHJ=PATH(J)
      IF (ZJUNC(N).EQ.LJUNC(IPATHJ)) GO TO 480
      GO TO 490
      C
      C GET HERE IF CABLE N STARTS AT JUNCTION M
      C
      480 K=K+1
      PATH(K)=N
      GO TO (490,485), LOOP
      C
      C REMEMBER HERE FIRST VALUE OF K ON TREE LEVEL
      C
      485 IF (JMAX-EO*(K-1)) JMINP=K
      490 CONTINUE
      495 CONTINUE
      GO TO 460
      C
      C PUT DATA INTO DATA ARRAY
      C
      500 IF (IFCUD.NE.0) GO TO 515
      IF ((DATA(12).EQ.TEST(13)).OR.(DATA(12).EQ.TEST(14))) GO TO 505
      GO TO 515
      505 IO=INDEX
      DC 510 J=1,10
      DATA(IROW,J)=DATA1(I0,J)
      510 DATA(ID,J)=DATA(J)
      GO TO 525
      515 DC 520 J=1,10
      520 DATA(IROW,J)=DATA(J)
      525 IROW=IROW+1
      IF (IROW-LE.2150) GO TO 50
      WRITE (IPRINT,665)
      GO TO 50
      C
      C THIS SECTION GENERATES ALL ERROR MESSAGES
      C
      530 FATE=1.
      IFORNE=4
      WRITE (ISCK) (FORP,IBAD
      535 IF (NDATC.EC.0) GO TO 50
      540 IFM=6
      IFAC=1
      GO TO 530
      545 IFM=1
      GO TO 530
      550 IFM=2
      GO TO 530

```



```

555 IER=3
    IBAU=32
    GC TO 530
915
560 IER=4
    GC TO 530
565 IER=6
    GC TO 530
920
570 IER=7
    FATE=1
    IFORM=5
    IBAU=41
    WRITE (ISCR) IFORM,IBAD
925
    WRITE (ISCR) IFUNC,IFRMO,NANC
    GC TO 535
575 IER=14
    FATE=1
    IFORM=6
    WRITE (ISCR) IFORM,IBAD
930
    WRITE (ISCR) ACUMP,IVORI,NVSEG,NZL,NANG
    GC TO 535
580 IER=8
    FATE=1
    IBAU=42
    IFORM=7
    WRITE (ISCR) IFORM,IBAD
935
    WRITE (ISCR) (ICAB(I),I=1,22)
    GC TO 535
585 IER=9
    FATE=1
    IBAU=43
    IFORM=8
    WRITE (ISCR) IFORM,IBAD
945
    WRITE (ISCR) (ICHECK(I),I=1,44)
    GC TO 535
590 IER=11
    FATE=1
    IBAU=44
    IFORM=9
    WRITE (ISCR) IFORM,IBAD
950
    WRITE (ISCR) ACAB,NANC,ADJUNC,NIRC,NINH
    GC TO 535
595 IER=12
    GC TO 530
600 IER=13
    FATE=1
    IBAU=52
    GC TO 530
955
605 DATA(1)=DATA(1)
    DATA(2)=DATA(2)
610 IER=15
    IBAU=55
    GC TO 530
960
615 IER=16
    IBAU=56
    IF (FORU.LV.C) GC TO 530
    DATA(1)=DATA(1)
    DATA(2)=DATA(2)
965

```

03/07/80 11.41.06

FIN 4.6.433E

74/74 OPT=1

SUBROUTINE INPUT

```

970      C
          GO TO 530
          620 FORMAT (HAIU)
          625 FORMAT (A5,A3)
          630 FORMAT (F4.0,A4,UBR.0,F5.0,I3)
          635 FORMAT (F4.0,A4,RE15.8/E17.5,I3)
          640 FORMAT (10F8.0)
          645 FORMAT (RE15.8)
          650 FORMAT (A4,I4,3E15.8)
          655 FORMAT (1H1.18ANALYSIS COMPLETED)
          660 FORMAT (F4.0,A4,RE15.8)
          665 FORMAT (6X,2H17,18A,45HCOMMON/B1/ BOUND EXCEEDED.  SEE USERS MANUAL
          IL.)
          END
INP 970
INP 971
INP 972
INP 973
INP 974
INP 975
INP 976
INP 977
INP 978
INP 979
INP 980
INP 981
INP 982
INP 983-
```

CARD NO. SEVERITY DETAILS DIAGNOSIS OF PROBLEM

```

861 1 AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.
872 1 AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.
```



```

1  *CHECK MPPLY 1
2  SUBROUTINE MPPLY (C,HR,RI)
3
4  C THIS ROUTINE FINDS REAL ROOTS OF POLYNOMIAL EQUATIONS UP TO
5  C  $C(4)*X^4 + C(3)*X^3 + C(2)*X + C(1) = 0$  FOR USE IN
6  C EVALUATING MAXIMUM CABLE DISPLACEMENTS AND TENSION EXTREMA
7  C
8  C REAL PARTS OF ROOTS ARE PLACED IN RR, IMAGINARY PARTS IN RI
9  C SINCE ONLY REAL ROOTS ARE OF INTEREST, ALL NON-REAL OR
10 C NON-EXISTING ROOTS RETURN RR=0, RI=1
11
12 C DIMENSION C(4), RR(3), RI(3)
13 C IF (C(4).NE.0.) GO TO 40
14 C IF (C(3).NE.0.) GO TO 30
15 C IF (C(2).NE.0.) GO TO 15
16
17 C GET HERE IF EQUATION IDENTICALLY SATISFIED.
18
19 C 5 UC TO 1=1,3
20 C RI(1)=0.
21 C RI(1)=1.
22 C RETURN
23
24 C GET HERE IF EQUATION LINEAR
25
26 C 15 RR(1)=-C(1)/C(2)
27 C RI(1)=0.
28 C UC 25 1=2,3
29 C PR(1)=0.
30 C RI(1)=1.
31 C RETURN
32
33 C GET HERE IF EQUATION QUADRATIC
34
35 C DISC=C(2)**2-4.*C(1)*C(3)
36 C IF (DISC.GE.0.) GO TO 35
37 C GO TO 5
38 C RR(1)=(-C(2)+SQRT(DISC))/(2.*C(3))
39 C RI(1)=0.
40 C PR(2)=(-C(2)-SQRT(DISC))/(2.*C(3))
41 C RI(2)=0.
42 C RR(3)=0.
43 C RI(3)=1.
44 C RETURN
45
46 C GET HERE IF EQUATION CUBIC
47
48 C 40 P=C(3)/C(4)
49 C Q=C(2)/C(4)
50 C R=C(1)/C(4)
51 C A=(3.*Q-P**2)/3.
52 C H=(2.*P**3-9.*P*Q+27.*R)/27.
53 C DISC=(H**2)/4.+ (A**3)/27.
54 C IF (DISC) 56,45,45
55 C DISC=30*H*DISC
56 C IF (H/2.*F0*DISC) CAPA=F1.
57 C IF (H/2.*F1*DISC) CAPA=F1*(1-H/2.*DISC)**4**((1./3.))/(1-H/2.*DISC)

```

```

CAPB=((1+P/2,-DISC)**4)**(1./3.)/(-B/2.-DISC)
RH(1)=CAPB*CAPB-P/3.
RI(1)=0.
IF (DISC.GT.0.) GO TO 20
RH(2)=-CAPB-P/3.
RI(2)=0.
RH(3)=RH(2)
RI(3)=0.
RETURN
5C DISC=2.*SGT(-A/3.)
PHI=ACOS((1+3.*B)/(A*DISC))/3.
RH(1)=-P/3.+DISC*COS(PHI)
RH(2)=-P/3.+DISC*COS(PHI+3.14159265*(2./3.))
RH(3)=-P/3.+DISC*COS(PHI+3.14159265*(4./3.))
PI(1)=0.
PI(2)=0.
PI(3)=0.
RETURN
END

```

RPO 58
 RPO 59
 RPO 60
 RPO 61
 RPO 62
 RPO 63
 RPO 64
 RPO 65
 RPO 66
 RPO 67
 RPO 68
 RPO 69
 RPO 70
 RPO 71
 RPO 72
 RPO 73
 RPO 74
 RPO 75
 RPO 76-


```

1      *DECK START
2      SUBROUTINE STARI
3
4      C
5      C THIS ROUTINE CALCULATES THE INITIAL GUESSES AT THE IMAGINARY
6      C AND EQUILIBRATING REACTIONS AND THE INITIAL DELTA BASED ON
7      C THE TOTAL WEIGHT OF THE ARRAY
8
9      COMMON /B3/ VELX(25),VELY(25)
10     COMMON /B1/ FEJUNC,IR,DELTA1,DELTA,IRS,IFJUNC,E,ES,FCAB,RCAB,JUMP,STA
11     COMMON /B2/ PCAB,PCAB0,PCAB00,THETA,PJUNC0
12     COMMON /B3/ NCAB,NNODE,ERJUNC,IRJUNC,DAT1,DATN,P,PJUNC,CUCAB,DCAB,STA
13     IFATE,NANC,ANJUNC,IREAD,IPRNT,INTAPE,OUTAPE,ITIME,IFLG,OFLG,NIR,THESTA
14     ZIAB,THETA,CUPPD,THFTAB,IRJUNC,RHO,TEST,NVSEF,2VEL,VELZ,PIP,ECICAB,STA
15     DEPCAB,ZJUNC,LJUNC,PATH,ICAB,IVOPT,WCAH,IOEV,ICHECK,NDEV,NUATC STA
16     DIMENSION FEJUNC(3,44), IR(3,44), IRS(3,44), IFJUNC(3,44), PJUNC0(STA
17     13,44)
18     DIMENSION FCAB(3,51,22), HCAB(3,51,22), PJUNCS(3,44), PCAB(3,51,22) STA
19     1)
20     DIMENSION PCAB0(3,51,22), PCAB00(3,51,22), RCAB0(3,51,22)
21     DIMENSION NNODE(22), ERJUNC(44), IRJUNC(44), DAT1(10), DATN(10), HSTA
22     1(22)
23     DIMENSION PJUNC(3,44), CUCAB(22), DCAB(22), ANJUNC(44), TEST(14) STA
24     DIMENSION ZVEL(25), VELZ(25), ECICAB(22), EXPCAB(22), ZJUNC(22) STA
25     DIMENSION ICHECK(44)
26     INTEGER OLTAPE,ZJUNC,ERJUNC,ANJUNC,OFLG
27     INTEGER PATH
28     REAL IR,IRS
29     WEIGHT=0.
30     DO 5 J=1,PJUNC
31     5 WEIGHT=WEIGHT+FEJUNC(3,J)
32     DO 10 N=1,NCAB
33     10 NNODE(N)=1
34     DO 10 M=1,INNA
35     10 WEIGHT=WEIGHT+FCAB(3,M,N)
36     DO 15 N=1,NIR
37     15 KER=ERJUNC(N)
38     DO 15 I=1,J
39     15 IR(I,KER)=0.
40     DO 20 N=1,NIR
41     20 KIR=IRJUNC(N)
42     KER=ERJUNC(N)
43     IR(1,KIR)=0.
44     IR(2,KIR)=0.
45     IR(3,KIR)=WEIGHT/(NIR+1.01)
46     IR(3,KER)=IR(3,KER)-IR(3,NTH)
47     20 DELTA1=ABS(WEIGHT)/(NIR+1)
48     RETURN
49     ENDO

```



```

C
WRITE (IPRINT,575)
WRITE (IPRINT,580)
IF (JUM,61.1) GO TO 115
WRITE (IPRINT,595)
GO TO 120
115 WRITE (IPRINT,590)
WRITE (IPRINT,595)
120 CONTINUE
C
THIS SECTION CALCULATES MAXIMUM AND MINIMUM CABLE TENSIONS
AND MAXIMUM CABLE DISPLACEMENTS FROM NO CURRENT LOCATION
BY EXTRAPOLATION BETWEEN CABLE NODES
C
INITIALIZE EXTREMA
C
DO 295 MN=1,NCAB
  N=NN
  IMAX=ICAB(1,N)
  SIMAX=0.
  IMIN=IMAX
  SIMIN=0.
  DO 130 I=1,3
    IC IO (135,125), JUM
    DC 130 I=1,3
  130 DMAX=DMAX+(PCAB(I,1,N)-PCAB(I,1,N))**2
    DMAX=SQRT(DMAX)
    SOMAX=0.
    MX=NNODE(N)-1
    DC 245 MN=1,MX
    M=MM
    MI=MM+1
  C
  CALCULATE EXTRAPOLATION QUANTITIES
  C
  HR=0.
  HD=0.
  DC 150 I=1,3
    D(I)=(PCAB(I,M,N)-PCAB(I,M,N))/H(N)
    GO TO (145,140), JUM
  140 A(I)=PCAB(M,N)*PCAB(I,M,N)/TCAB(M,N)
    H(I)=(EXCAB(M,N)-PCAB(I,M,N)-PCAB(I,M,N))/H(N)
    U(I)=PCAB(I,M,N)-PCAB(I,M,N)
  145 MR=HR+PCAB(I,M,N)*PCAB(I,M,N)
    MD=MD+PCAB(I,M,N)*PCAB(I,M,N)
    DC 150 D(I)=D(I)
    GO TO (175,155), JUM
  155 DC 160 I=1,3
    TEMP1(I)=PCAB(I,M,N)
    TEMP2(I)=PCAB(I,M,N)
    PCAB(I,M,N)=PCAB(I,M,N)
    PCAB(I,M,N)=PCAB(I,M,N)
    UL=0.
    UV=0.
    UVW=0.
    VW=0.

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03/07/80 11.41.06

FTN 4.6.433E

SUBROUTINE STRUT 74/74 OPT=1

```

      IF (PI(I).NE.0.) GO TO 240
      IF ((HQ(I).LE.0.)OR.(AG(I).GE.H(N))) GO TO 240
      SIG=HU(I)
      225 ZARG=UU*2.*LV*SIG*UVW*SIG**2*2.*VM*SIG**J*WW*SIG**4
      C THESE STATEMENTS CHECK ZARG FOR ZERO AND NEGATIVE VALUES
      C ZARG SHOULD BE POSITIVE, IF IT IS NOT IT IS COMPARED TO H(N).
      C THE LENGTH OF ONE CABLE SEGMENT, IF IT IS SMALL BY COMPARISON, IT
      C IS SET TO A SMALL POSITIVE VALUE
      IF (ZARG.LI.0.)AND.(ABS(ZARG/H(N)).LI.0.0001) ZARG=ABS(ZARG)
      IF (ZARG.EQ.0.) ZARG=0.000001*H(N)
      DE=SUB1(ZARG)
      IF (DE.GT.DMAX) GO TO 235
      230 IF (JTIME.EQ.0) GO TO 240
      GO TO 245
      235 DMAX=DE
      SDMAX=H(N)*(N-1)*SIG
      GO TO 230
      240 CONTINUE
      JTIME=1
      SIG=H(N)
      GO TO 220
      245 CONTINUE
      C
      C EXTREMA ALONG A CABLE NOW DETERMINED
      C CALCULATE FINAL AND INITIAL COORDINATES OF MAXIMALLY DISPLACED POINTS
      C
      GO TO (290,250), JUM
      250 KL=H(N)*MX
      IF (SDMAX.LT.KL) GO TO 260
      K=LJUNC(N)
      DO 255 I=1,K
      A(I)=PJUNC(I,K)
      255 B(I)=PJUNC(I,K)
      GO TO 285
      260 DATA(2)=FEST(4)
      DATA(3)=N
      DATA(10)=SDMAX
      J=(SDMAX/H(N))+1
      J1=J+1
      UC 265 I1=1+3
      I=11
      265 A(I)=SPACE(1)
      DO 270 I=1+3
      TEMP1(I)=HCAH(I,J,N)
      TEMP2(I)=HCAH(I,J1,N)
      TEMP3(I)=PCAB(I,J,N)
      WCAH(I,J,N)=HCAH(I,J,N)
      WCAH(I,J1,N)=HCAH(I,J1,N)
      PCAB(I,J,N)=HCAH(I,J,N)
      PCAB(I,J1,N)=HCAH(I,J1,N)
      270 UC 275 I1=1+3
      I=11
      275 H(I)=SPACE(1)
      DO 280 I=1+3
      HCAH(I,J,N)=TEMP1(I)
      HCAH(I,J1,N)=TEMP2(I)
      PCAB(I,J,N)=TEMP3(I)
      280 PCAB(I,J,N)=TEMP3(I)
      285 CONTINUE

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11.41.06

FTN 4.6.433E

OPT=1

SUMUL TIME SIMOUT

74/74

```

345      WRITE (IPRNT,600) N,IMAX,STMAX,IMIN,STMIN,DMAX,SDMAX,(A(I),I=1,3),STR 343
      1(B(I),I=1,3)
      GO TO 295
      290 WRITE (IPRNT,600) N,IMAX,STMAX,IMIN,STMIN
      295 CONTINUE
      C
      C
      C      GENERATE JUNCTION HEADERS
      C
      C      WRITE (IPRNT,605)
      C      WRITE (IPRNT,610)
      C      IF (JUM.GT.1) GO TO 300
      C      WRITE (IPRNT,615)
      C      WRITE (IPRNT,620)
      C      GO TO 305
      C
      300 CONTINUE
      C      WRITE (IPRNT,625)
      C      WRITE (IPRNT,630)
      C
      305 CONTINUE
      C
      C      THIS SECTION CALCULATES JUNCTION FORCES, LOCATIONS AND DISPLACEMENTS
      C
      C      IF=0
      C      DO 395 J1=1,NJUNC
      C      DO 310 K=1,NARC
      C      IF (ANJUNC(K).EQ.J1) GO TO 395
      C
      310 CONTINUE
      C      GO TO (325,315), JUM
      C
      315 DO 320 J2=1,3
      C      DISP(J2)=PJUNC(J2,J1)-PJURIG(J2,J1)
      C      DISP(J2)=PJUNC(J2,J1)-PJUNC(J2,J1)
      C      J6=1
      C      IF (NDATC(J1).OR.JUM.GT.1) GO TO 335
      C      DO 330 J2=1,3
      C      PJURIG(J2,J1)=PJUNC(J2,J1)
      C
      330 CONTINUE
      C      340 IF (J1.EQ.2)JUNC(J6) GO TO 360
      C      345 IF (J1.EQ.1)JUNC(J6) GO TO 380
      C      350 J6=J6+1
      C      IF (J6.LE.NCAR) GO TO 340
      C      IF (NIR.EQ.0) GO TO 395
      C      J7=1
      C
      355 IF (J1.EQ.1)JUNC(J7) GO TO 365
      C      J7=J7+1
      C      IF (J7.LE.NIR) GO TO 355
      C      GO TO 395
      C
      360 MM=J6
      C      I=ICAR(1,MM)
      C      RX=RCAB(1,1,MM)
      C      MY=RCAB(2,1,MM)
      C      MZ=RCAB(3,1,MM)
      C      GO TO 390
      C
      365 INDEX=IJUNC(I7)
      C      DO 370 J8=1,NCAR
      C      F(SINDEA,EG,IJUNC(I7)) GO TO 375
      C
      370 CONTINUE
      C      375 MM=J8
      C      GO TO 345

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11.41.06

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FIN 4.6.433E

SUBROUTINE SROUT 74/74 OPT=1

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400      300 IN=J0
401      385 MX=MODE (PH)
402      I=ICAB (MX,MM)
403      MX=RCAB (1,1,1,MM)
404      MY=RCAB (2,1,1,MM)
405      H7=RCAB (3,1,1,MM)
406      H7=SCRT (H7**2+RY**2)
407      IF (H7.EV.0.) H7=1.
408      A1=ASIN (H7/H1)/PI
409      A2=ASIN (H7/1)/PI
410      IF (H7.LT.0.) AND. (RY.GE.0.) A1=180.-A1
411      IF (H7.LT.0.) AND. (RY.LT.0.) A1=180.-A1
412      IF (H7.EV.0.) AND. (JUM.EV.1) WRITE (IPRNT,635) J1,MM,T,A1,A2,(PJUSI,635) J1,MM,T,A1,A2,(PJUSI,635) J1,MM,T,A1,A2
413      INC (KJ1),KJ1+1
414      IF ((H7.EV.0.) AND. (JUM.EV.2)) WRITE (IPRNT,635) J1,MM,T,A1,A2,(PJUSI,635) J1,MM,T,A1,A2,(PJUSI,635) J1,MM,T,A1,A2
415      INC (KJ1),KJ1+1
416      IF ((H7.EV.0.) AND. (JUM.EV.3)) DISP (1),I=1,3) (DISP (1),I=1,3)
417      IF ((H7.EV.0.) AND. (JUM.EV.1)) WRITE (IPRNT,635) J1,MM,T,A1,A2
418      IF=1
419      IF (H7.LT.0.) AND. (J1.EQ.2JUNC(J6)) GO TO 345
420      IF (H7.LT.0.) AND. (J1.EQ.2JUNC(J6)) GO TO 350
421      395 IF=0
422      C
423      C
424      C
425      C
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456      C

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STR 571-

END

CARD NO. SEVERITY DETAILS DIAGNOSIS OF PROBLEM

47	I	AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.
194	I	AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.
212	I	AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.
219	I	AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.
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312	I	AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.
369	I	AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.
463	I	AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.


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1  *DECK TANG
2  FUNCTION TANG (I)
3
4
5  C
6  C
7  C
8  THIS ROUTINE CALCULATES THE UNIT TANGENT TO A CABLE AT ANY POINT
9
10 COMMON /B3/ VELX(25),VELY(25)
11 COMMON /B1/ FEJUNC,IR,DELTA,IRS,TFJUNC,E,ES,FCAB,RCAB,JUMP,TAN
12 IPJUNC,PCAB,PCABE,PCABO,RCABO,THETA,PJUNCO
13 COMMON /B2/ NCAB,NNODE,ERJUNC,IRJUNC,DATI,DATN,M,PJUNC,DCAB,DCAB,TAN
14 IFATE,NANC,ANJUNC,IREAD,IPRNT,INTAPE,OUTAPE,ITIME,IFLG,OFLG,NIR,THEI,TAN
15 2IAS,THEIAE,COMPD,THEIAB,NJUNC,RHO,TEST,NVSEG,ZVEL,VELZ,P,IP,ECICAB,TAN
16 3EXPCAB,ZJUNC,CJUNC,PATH,ICAB,IVOR,WCAB,IDEV,ICHECK,NDEV,NDATC
17 DIMENSION FEJUNC(3,44), IR(3,44), IRS(3,44), TFJUNC(3,44), PJUNCO(
18 13,44),
19 DIMENSION FCAB(3,51,22), RCAB(3,51,22), PJUNC(3,44), PCAB(3,51,22)
20 1)
21 DIMENSION PCABE(3,51,22), PCABO(3,51,22), RCABO(3,51,22)
22 DIMENSION NNODE(22), ERJUNC(44), IRJUNC(44), DATI(10), DATN(10),
23 1(22)
24 DIMENSION PJUNC(3,44), DCAB(22), DCAB(22), ANJUNC(44), TEST(14)
25 DIMENSION ZVEL(25), VELZ(25), ECICAB(22), EXPCAB(22), ZJUNC(22)
26 DIMENSION LJUNC(22), PATH(22), ICAB(22), WCAB(22), IDEV(1000)
27 DIMENSION ICHECK(44)
28 INTEGER OUTAPE,ZJUNC,ERJUNC,ANJUNC,OFLG
29 INTEGER PATH
30 REAL IR,IRS
31 N=DATI(3)
32 M=IDATI(10)/H(N))+.1
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11.41.06

FTN 4.6.433E

SUBROUTINE TAPOUT 74/74 OPT=1

03/07/80

```

1      *DECK TAPOUT
      SUBROUTINE TAPOUT
C
C      THIS ROUTINE GENERATES THE TAPE OR CARDS GIVING
C      THE LOCATIONS OF THE INDEXED DEVICES
C
      COMMON /B3/ VELX(25),VELY(25)
      COMMON /B1/ FEJUNC,IR,DELTA,IRS,TFJUNC,E,ES,FCAB,RCAB,JUMP,TAP
      IPJUNC,PCAB,PCABE,PCABO,RCABO,THETA,PJUNCO
      COMMON /B2/ NCAB,NNODE,ERJUNC,IRJUNC,DATN,M,PJUNC,DCAB,PCAB,TAP
      IFATE,NANC,ANJUNC,IREAD,IPRNT,INTAPE,OUTAPE,ITIME,IFLG,UF LG,NIR,THETA,TAP
      215,THEIAC,COMP,THEIAB,NJUNC,RHO,TEST,NVSEG,ZVEL,VELZ,PIP,ECICAB,TAP
      3EPCAB,JJUNC,LJUNC,PATH,ICAB,IVOP,WCAB,IDEV,ICHECK,NDEV,NDATC,TAP
      DIMENSION FEJUNC(3,44), IR(3,44), IRS(3,44), TFJUNC(3,44), PJUNCO(TAP
      13,44)
      DIMENSION FCAB(3,51,22), RCAB(3,51,22), PJUNCS(3,44), PCAB(3,51,22)TAP
      16
      DIMENSION PCABE(3,51,22), PCABO(3,51,22), RCABO(3,51,22)
      DIMENSION NNODE(22), ERJUNC(44), IRJUNC(44), DATN(10), MTAP 19
      1(22)
      DIMENSION PJUNC(3,44), CDCAB(22), DCAB(22), ANJUNC(44), TEST(14)
      DIMENSION ZVEL(25), VELZ(25), ECICAB(22), EXPCAB(22), ZJUNC(22)
      DIMENSION LJUNC(22), PATH(22), ICAB(22), WCAB(22), IDEV(1000)
      DIMENSION ICHECK(44)
      DIMENSION PSPACE(3)
      INTEGER OUTAPE,ZJUNC,ERJUNC,ANJUNC,OFLG
      REAL IR,IRS
      ID1=4H CUR
      ID2=4H DEV
      ID3=4H REC
      JUM=JUMP+1
      GO TO (5,10), JUM
      5 WRITE (OUTAPE,35) ID3,NDATC
      WRITE (OUTAPE,35) ID1,JUMP
      GO TO 15
      10 WRITE (OUTAPE,35) ID1,JUMP,THETA
      15 IF (NDEV.EQ.0) GO TO 30
      DO 25 NK=1,NDEV
      READ (INTAPE,40) (DATI(K),K=1,10)
      INDEX=DATI(5)
      C      CALCULATE LOCATION OF DEVICE IN SPACE
      C
      DO 20 J=1,3
      15J
      20 PSPACE(I)=SPACE(I)
      WRITE (OUTAPE,35) ID2,INDEX,(PSPACE(I),I=1,3)
      25 CONTINUE
      30 CONTINUE
      REWIND INTAPE
      RETURN
      C
      35 FORMAT (44,14,3F10.2)
      40 FORMAT (F4.0,A4,8E15.8)
      END

```

PAGE 2

03/07/80 11.41.06

FTN 4.6.433E

74/74 OPT=1

SUBROUTINE IAPOUT

CARD NR. SEVERITY DETAILS DIAGNOSIS OF PROBLEM

33 1 AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.


```

1      *DECK VELOC
2      FUNCTION VELOC (I,PSPACE)
3
4      C
5      C THIS ROUTINE SPECIFIES THE I COMPONENT OF THE CURRENT FIELD
6      C AT AN ARBITRARY POINT IN SPACE, PSPACE(I)
7
8      COMMON /B3/ VELX(25),VELY(25)
9      COMMON /B1/ FEJUNC,IR,DELTA,DELTA,IRS,IFJUNC,E,ES,FCAB,RCAB,JUMP,VEL
10     PCAB,PCAB,PCAB,PCAB,HCAB,THETA,PJUNC
11     COMMON /B2/ NCAB,NODE,ERJUNC,IRJUNC,DATI,DATN,M,PJUNC,DCAB,DCAB,VEL
12     IFAT,NANC,ANJUNC,THEAD,IPRNT,INTAPE,OUTAPE,ITIME,IFLG,OFLG,NIR,THEVEL
13     2IAS,THETA,COMPO,THETAB,NJUNC,RHO,TEST,NVSEG,ZVEL,VELZ,PIP,ECICAB,VEL
14     3EXPCAB,ZJUNC,LJUNC,PATH,ICAB,IVOPT,WCAB,IDEV,ICHECK,NDEV,NDATC
15     COMMON /PIBLK/ PI
16     COMMON /KITER/ KOUNT,IR,NI,MMITER,NSTEPS,ISTEP,PERCNTV,INCPHNT
17     DIMENSION FEJUNC(3,44), IR(3,44), IRS(3,44), IFJUNC(3,44), PJUNC(10),
18     13,44)
19     DIMENSION FCAB(3,51,22), RCAB(3,51,22), PJUNC(3,51,22), PCAB(3,51,22)
20     1)
21     DIMENSION PCAB(3,51,22), PCAB(3,51,22), RCAB(3,51,22)
22     DIMENSION MNODE(22), ENJUNC(44), IRJUNC(44), DATI(10), DATN(10),
23     1(22)
24     DIMENSION PJUNC(3,44), DCAB(22), DCAB(22), ANJUNC(44), TEST(14)
25     DIMENSION ZVEL(25), VELZ(25), ECICAB(22), EXPCAB(22), ZJUNC(22)
26     DIMENSION ICHECK(44)
27     DIMENSION PSPACE(3)
28     INTEGER OUTAPE,ZJUNC,ERJUNC,ANJUNC,OFLG
29     REAL IR,IRS
30     DIR=PI/18J.
31     PERCNTV=FLGAT(ISTEP)/FLGAT(NSTEPS)
32     T=THETA*DIH
33     GO TO (5,5,40), I
34     5 Z=PSPACE(3)
35     DC TO KR=1,NVSEG
36     K=K
37     IF (Z.GT.ZVEL(K)) GO TO 10
38     GO TO 15
39     10 CONTINUE
40     VFPSX=1.6878*VELX(K)
41     VFPSY=1.6878*VELY(K)
42     GO TO 25
43     15 IF (K.NE.1) GO TO 20
44     VFPSX=1.6878*VELX(K)
45     VFPSY=1.6878*VELY(K)
46     GO TO 25
47     20 SIGMA=2-ZVEL(K-1)
48     SLOPX=(VELX(K)-VELX(K-1))/(ZVEL(K)-ZVEL(K-1))
49     SLOPY=(VELY(K)-VELY(K-1))/(ZVEL(K)-ZVEL(K-1))
50     VFPSX=1.6878*(VELX(K-1)+SLOPX*SIGMA)
51     VFPSY=1.6878*(VELY(K-1)+SLOPY*SIGMA)
52     25 V=0.5*VFPSX+VFPSY*2*VFPSY*2
53     E=(VFPSX*VFPSX+VFPSY*VFPSY)*0.00001
54     55     55     55     55     55     55     55     55     55     55
55     55     55     55     55     55     55     55     55     55     55
56     55     55     55     55     55     55     55     55     55     55
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97     55     55     55     55     55     55     55     55     55     55
98     55     55     55     55     55     55     55     55     55     55
99     55     55     55     55     55     55     55     55     55     55
100    55     55     55     55     55     55     55     55     55     55

```

FUNCTION VELOC 74/74 OPT=1 F1N 4.6433E 03/07/80 11.41.06 PAGE 2

RETURN
35 VELUC=VPG*G*SIN(A)*PENCN1V
RETURN
40 VELUC=0.
RETURN
END

VEL 58
VEL 59
VEL 60
VEL 61
VEL 62
VEL 63-

60

CARD NR. SEVERITY DETAILS DIAGNOSIS OF PROBLEM

34 I AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.
56 I AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.

03/07/80 11.41.06

FTN 4.6.433E

SUBROUTINE MEDVEL 74/74 OPT=1

```

1      *DELK MEDVEL
2      SUBROUTINE MEDVEL (IR,IM)
3
4      C
5      ROUTINE TO READ CURRENT DATA FOR CURRENT OPTION 3
6
7      C
8      COMMON /BIN/ ISCH
9      COMMON /CVEL/ VMAG(25,4),VDIR(25,4),ZPT(25,4),XPT(4),YPT(4),NPPS(4)
10     I),NSTA
11     COMMON /PCUR/ XNPT(4),YMPI(4)
12     COMMON /TITL/ TITLE(8),PHI,CUNITS,IUNIT,VELXP(25),VELYP(25)
13     COMMON /B2/ NCAB,NNUCE,IRJUNC,IRJUNC,DAT1,DATN,PJUNC,CDUCAB,DCAB,RED
14     IFATE,NANC,ANJUNC,IREAD,IPRNT
15     COMMON /PIBLK/ PI
16     DIMENSION NS(4)
17     DIMENSION STORH(8)
18     DIMENSION NNUCE(22), ERJUNC(44), IRJUNC(44), DAT1(10), DATN(10), HRED
19     1(22)
20     DIMENSION PJUNC(3,44), CDCAB(22), DCAB(22), ANJUNC(44)
21     IREAD=0
22     IFORML=1
23     DIR=PI/180.
24     DO 20 J=1,NSTA
25     HEAD (IR,30) STORE
26     WRITE (ISCR) IFORML,IRAD
27     WRITE (ISCR,30) STORE
28     (ECODE (J0,35),STORE) NS(J),NPPS(J),XNPT(J),YMPI(J)
29     IF (XNPT(J).NE.0.0)OR(YMPI(J).NE.0.0) GO TO 5
30     XPT(J)=0.
31     YPT(J)=0.
32     GO TO 10
33     5 W=SQR1(XNPT(J)**2+YMPI(J)**2)
34     A=ATAN2(YMPI(J),XNPT(J))
35     H=A+PI*(0.5)
36     XPT(J)=W*COS(H)
37     YPT(J)=W*SIN(H)
38     IF NPPS(J)
39     DO 15 I=1,NP
40     HEAD (IR,30) STORE
41     WRITE (ISCR) IFORML,IRAD
42     WRITE (ISCR,30) STORE
43     (ECODE (40,30),STORE) NS(J),ZPT(I,J),VMAG(I,J),VDIR(I,J)
44     15 VMAG(I,J)=VMAG(I,J)*CUNITS
45     20 CONTINUE
46     DO 25 J=1,NSTA
47     NP=NPPS(J)
48     DO 25 I=1,NP
49     VDIR(I,J)=J60.0*PI*VDIR(I,J)
50     RETURN
51
52     30 FORMAT (MA10)
53     35 FORMAT (2I5,2F10.0)
54     40 FORMAT (15,5X,3F10.0)
55     END

```

```

1  *DECK INTVEL                                INT 1
2  SUBROUTINE INTVEL (NW, PSPACE)              INT 2
3  COMMON /CVEL/ VMAG(25,4), VDIR(25,4), ZPT(25,4), XPI(4), YPI(4), NPPTS(4) INT 3
4  1) INSTA                                     INT 4
5  COMMON /CLE1/ X,Y,DUMMY(9), VDR(4), VMG(4)  INT 5
6  COMMON /PIBLK/ PI                           INT 6
7  DIMENSION M(3), FSPACE(3)                  INT 7
8  DIMENSION V1(4), V2(4)                     INT 8
9  STAT(Y1,Y2)=Y1*(Y2-Y1)**H                  INT 9
10 X=PSPACE(1)                                INT 10
11 Y=PSPACE(2)                                INT 11
12 Z=PSPACE(3)                                INT 12
13 DO 20 J=1,NSIA                              INT 13
14   NP=NPPTS(J)                               INT 14
15   DO 5 I=1,NP                               INT 15
16     ZDIF=Z-ZPT(I,J)                         INT 16
17     IF (ZDIF.GT.0.) GO TO 5                  INT 17
18     I2=I                                      INT 18
19     I1=I-1                                    INT 19
20     GO TO 10                                 INT 20
21   5 CONTINUE                                INT 21
22   10 IF (I1.EQ.0) GO TO 15                   INT 22
23   V1(I1)=ZPT(I1,J)/(ZPT(I2,J)-ZPT(I1,J))    INT 23
24   V2(I1)=STAT(VMAG(I1,J),VMAG(I2,J))        INT 24
25   VDR(I1)=STAT(VDR(I1,J),VDR(I2,J))         INT 25
26   GO TO 20                                  INT 26
27   15 VMG(J)=VMAG(I2,J)                      INT 27
28   VDR(J)=VDR(I2,J)                          INT 28
29   20 CONTINUE                                INT 29
30   NS=NSIA-1                                 INT 30
31   GO TO (25,45,50), NS                      INT 31
32   25 X1=XPI(1)                               INT 32
33   X2=XPI(2)                                  INT 33
34   Y1=YPI(1)                                  INT 34
35   Y2=YPI(2)                                  INT 35
36   IF (X1-X2.NF.0.0) GO TO 30               INT 36
37   X3=X1                                       INT 37
38   Y3=Y1                                       INT 38
39   GO TO 40                                   INT 39
40   30 IF (Y1-Y2.NE.0.0) GO TO 35             INT 40
41   X3=X1                                       INT 41
42   Y3=Y1                                       INT 42
43   GO TO 40                                   INT 43
44   35 SM1=(Y2-Y1)/(X2-X1)                     INT 44
45   SM1=(Y2-Y1)/(X2-X1)                     INT 45
46   SM2=-1./SM1                                INT 46
47   DC=SM2-SM1                                 INT 47
48   X3=(Y1-SM1*X1)-(Y-SM2*X1)/DC              INT 48
49   Y3=(X1-SM2*Y1)-(X-SM1*Y)/DC              INT 49
50   S1=SDMT((X2-X1)**2*(Y2-Y1)**2)           INT 50
51   S2=SDMT((X3-X1)**2*(Y3-Y1)**2)           INT 51
52   SCS=52/S1                                  INT 52
53   V1(I1)=S0S*(VMG(2)-VMG(1))*VMG(I1)       INT 53
54   V2(I1)=S0S*(VDR(2)-VDR(1))*VDR(I1)       INT 54
55   GO TO 55                                   INT 55
56   45 CALL SCT (I)                            INT 56
57   CALL CRAMEH (V1(I))                       INT 57

```

03/07/80 11:41:06

FTN 4.6+433E

SUBROUTINE INIVEL 74/74 OPT=1

```

60      CALL SET (2)
        CALL CRAMER (V2(1))
        GO TO 55
50      CALL SET (1)
        CALL CRAMER (V1(1))
        CALL SET (2)
        CALL CRAMER (V2(1))
        CALL SET (3)
        CALL CRAMER (V2(2))
        CALL SET (4)
        CALL CRAMER (V1(2))
        CALL SET (5)
        CALL CRAMER (V1(3))
        CALL SET (6)
        CALL CRAMER (V2(3))
        CALL SET (7)
        CALL CRAMER (V2(4))
        CALL SET (8)
        CALL CRAMER (V1(4))
        V1(1)=.25*(V1(1)+V1(2)+V1(3)+V1(4))
        V2(1)=.25*(V2(1)+V2(2)+V2(3)+V2(4))
55      DTR=PI/180.
        TRT=V2(1)*DTR
        W1(1)=V1(1)*COS(TRT)*1.688
        W1(2)=V1(1)*SIN(TRT)*1.688
        W1(3)=0.0
        RETURN
        END

```

155

CAMD NR. SEVERITY DETAILS DIAGNOSIS OF PROBLEM

31 I AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.

03/07/80 11:41:06

FTN 4.6*43E

SUBROUTINE SET 76/74 OPT=1

```

1      *CHECK SET
2      SUBROUTINE SET (I)
3      COMMON /LEVEL/ VMAG(25,4),VDIR(25,4),ZPT(25,4),XPT(4),YPT(4),NPPS(4)
4      SET 3
5      1)INSTA
6      SET 4
7      COMMON /CLET/ X,Y,X1,X2,X3,Y1,Y2,Y3,Z1,Z2,Z3,VDR(4),VMG(4)
8      SET 5
9      GO TO (5,10,15,20,25,30,35,40), I
10     SET 6
11     5 CONTINUE
12     X1=XPT(1)
13     SET 7
14     X2=XPT(2)
15     SET 8
16     X3=XPT(3)
17     SET 9
18     Y1=YPT(1)
19     SET 10
20     Y2=YPT(2)
21     SET 11
22     Y3=YPT(3)
23     SET 12
24     Z1=VMG(1)
25     SET 13
26     Z2=VMG(2)
27     SET 14
28     Z3=VMG(3)
29     SET 15
30     RETURN
31     10 CONTINUE
32     Z1=VDR(1)
33     SET 16
34     Z2=VDR(2)
35     SET 17
36     Z3=VDR(3)
37     SET 18
38     RETURN
39     15 CONTINUE
40     X3=XPT(4)
41     SET 19
42     Y3=YPT(4)
43     SET 20
44     Z3=VDR(4)
45     SET 21
46     RETURN
47     20 CONTINUE
48     Z1=VMG(1)
49     SET 22
50     Z2=VMG(2)
51     SET 23
52     Z3=VMG(4)
53     SET 24
54     RETURN
55     25 CONTINUE
56     X1=XPT(3)
57     SET 25
58     Y1=YPT(3)
59     SET 26
60     Z1=VMG(3)
61     SET 27
62     RETURN
63     30 CONTINUE
64     Z1=VDR(3)
65     SET 28
66     Z2=VDR(2)
67     SET 29
68     Z3=VDR(4)
69     SET 30
70     RETURN
71     35 CONTINUE
72     X1=XPT(3)
73     SET 31
74     Y1=YPT(3)
75     SET 32
76     Z1=VMG(3)
77     SET 33
78     RETURN
79     40 CONTINUE
80     Z1=VDR(3)
81     SET 34
82     Z2=VDR(2)
83     SET 35
84     Z3=VDR(4)
85     SET 36
86     RETURN
87     45 CONTINUE
88     X2=XPT(1)
89     SET 37
90     Y2=YPT(1)
91     SET 38
92     Z2=VDR(1)
93     SET 39
94     RETURN
95     50 CONTINUE
96     Z1=VMG(3)
97     SET 40
98     Z2=VMG(1)
99     SET 41
100    Z3=VMG(4)
101    SET 42
102    RETURN
103    END

```

03/07/80 11.41.06

FTN 4.6.433E

OPT=1

74/74

SUBROUTINE CRAMEH

```

1  *DECK CRAMEH
   SUBROUTINE CRAMEH (ANS)
   COMMON /CLET/ X,Y,Z1,X2,X3,Y1,Y2,Y3,Z1,Z2,Z3,VDM(4),VMG(4)
   U=X1*(Y2*(Z3-Y3*Z2)-Y1*(X2*Z3-X3*Z2)+Z1*(X2*Y3-Y2*X3))
   AN=- (Y2*Z3-Y3*Z2)-Y1*(Z2-Z3)-Z1*(Y3-Y2)
   HA=X1*(Z2-Z3)+X2*Z3-X3*Z2+Z1*(X3-X2)
   CN=X1*(Y3-Y2)-Y1*(X3-X2)-(X2*Y3-Y2*X3)
   IF (U.NE.0) GO TO 5
   ANS=-(AN*X+BN*Y)/CN
   RETURN
5  AN=AN/I
   H=HN/I
   C=CN/D
   ANS=-(1./C)*(1.+A*X+B*Y)
   RETURN
   END

```

CRA 1
 CRA 2
 CRA 3
 CRA 4
 CRA 5
 CRA 6
 CRA 7
 CRA 8
 CRA 9
 CRA 10
 CRA 11
 CRA 12
 CRA 13
 CRA 14
 CRA 15
 CRA 16-

```

1      *DECK SORT
      SLRROUTINE SORT (NDEV,INTAPE)
      COMMON /HY/ FEJUNC
      COMMON /TADHKG/ TDCAB(22),TDDCAB(1000)
      DIMENSION DATII(2150,10), FEJUNC(3,44)
      EQUIVALENCE (DATII(1),FEJUNC(1))
      HEAD (INTAPE,70) (DATII(1,J),J=1,10),I=1,NDEV)
      COUNT NUMBER OF DCAB CARDS
      C
      C
      C
      K=U
      DO 5 I=1,NDEV
      IF (DATII(I,2).EQ.4*HDCAB) K=K+1
      5 CONTINUE
      NDCAB=K
      C
      C
      C
      PLT DJNC CARDS AFTER DCAB CARDS
      C
      C
      C
      NDCAB=NDEV-NDCAB
      IF (NDCAB.EQ.0) GO TO 40
      K=NDCAB+1
      DO 20 I=1,NDCAB
      IF (DATII(I,2).NE.4*HDCAB) GO TO 20
      20 IF (DATII(K+2).NE.4*HDCAB) GO TO 15
      K=K+1
      GO TO 10
      15 CALL SWAP (I,K)
      IF (K.EQ.NDEV) GO TO 25
      20 CONTINUE
      25 CONTINUE
      C
      C
      C
      SORT DJNC CARDS BY JUNCTION NUMBERS
      IF (NDCAB.EQ.1) GO TO 40
      NS=NDCAB+1
      NCI=NDEV-1
      DO 35 I=NS,NDI
      II=I+1
      DO 30 K=I,NDEV
      IF (DATII(I,3).LE.DATII(K,3)) GO TO 30
      CALL SWAP (I,K)
      30 CONTINUE
      35 CONTINUE
      40 CONTINUE
      IF (NDCAB.LE.1) RETURN
      C
      C
      C
      SORT DCAB CARDS BY CABLE NUMBER
      NDCAB=NDCAB-1
      DO 50 I=1,NDCAB
      II=I+1
      DO 45 K=II,NDCAB
      IF (DATII(I,3).LE.DATII(K,3)) GO TO 45
      CALL SWAP (I,K)
      45 CONTINUE
      50 CONTINUE
      C
  
```


03/07/80 11.41.06

FTN 4.6+433E

74/74 OPT=1

SUBROUTINE SORT

C SORT BY UNSTRESSED DISTANCE FORM S=0 JUNCTION OF CABLE

C

60

DO 65 I=1,NCCAB1

K=I+1

55 IF (UAT1(I,3).NE.OAT1(K,3)) GO TO 65

IF (UAT1(I,10).LE.OAT1(K,10)) GO TO 63

CALL SWAP (I,K)

60 K=K+1

IF (K.GT.NCCAB) GO TO 65

GO TO 55

65 CONTINUE

RETURN

70

C 70 FORMAT (F4.0,A4,BF0.0)

END

SUR 58
SUR 59
SUR 60
SUR 61
SUR 62
SUR 63
SUR 64
SUR 65
SUR 66
SUR 67
SUR 68
SUR 69
SUR 70
SUR 71
SUR 72-

SWA 1
SWA 2
SWA 3
SWA 4
SWA 5
SWA 6
SWA 7
SWA 8
SWA 9
SWA 10
SWA 11
SWA 12
SWA 13
SWA 14
SWA 15-

```

1      *LECK SWAP
      SUBROUTINE SWAP (I,K)
      COMMON /B1/ FEJUNC
      COMMON /IANDRG/ ICCAB(22),TDDCAB(1000)
      DIMENSION DATI(2150,10), TDATA(10), FEJUNC(3*44)
      EQUIVALENCE (DATI(1),FEJUNC(1))
      DC 5 J=1,10
      TDATA(J)=DATI(I,J)
      DATI(I,J)=DATI(K,J)
      DATI(K,J)=TDATA(J)
      TEMP=TDCCAB(I)
      TDDCAB(I)=TDDCAB(K)
      TDDCAB(K)=TEMP
      RETURN
      END
15

```


Line	Code	Statement	Address
60	C	WRITE (IPRINT,340) TITLE	BAD 58
	C	GO TO 10	BAD 59
	C	HEAD AND PRINT ERROR TYPES AND OTHER INFORMATION	BAD 60
	C		BAD 61
	C		BAD 62
	C		BAD 63
65	C	25 WRITE (IPRINT,375) TYPE(IBAD)	BAD 64
	C	GO TO 10	BAD 65
	C	30 READ (ISCR) IFUNC,IFRHO,NANC	BAD 66
	C	WRITE (IPRINT,375) TYPE(IBAD),IFUNC,IFRHO,NANC	BAD 67
	C	GO TO 10	BAD 68
70	C	35 READ (ISCR) NCOMP,IVOPT,NVSEG,NZL,NANG	BAD 69
	C	WRITE (IPRINT,375) TYPE(IBAD),NCOMP,IVOPT,NVSEG,NZL,NANG	BAD 70
	C	GO TO 10	BAD 71
	C	40 READ (ISCR) (ICAB(I),I=1,22)	BAD 72
	C	WRITE (IPRINT,380) TYPE(IBAD), (ICAB(I),I=1,22)	BAD 73
	C	GO TO 10	BAD 74
75	C	45 READ (ISCR) (ICHECK(I),I=1,44)	BAD 75
	C	WRITE (IPRINT,380) TYPE(IBAD), (ICHECK(I),I=1,44)	BAD 76
	C	GO TO 10	BAD 77
	C	50 READ (ISCR) NCAB,NANC,NOJUNC,NIRC,NIR	BAD 78
	C	WRITE (IPRINT,375) TYPE(IBAD),NCAB,NANC,NOJUNC,NIRC,NIR	BAD 79
	C	GO TO 10	BAD 80
80	C	PRINT TEXT OF ERRORS	BAD 81
	C		BAD 82
	C		BAD 83
	C		BAD 84
85	C	55 WRITE (IPRINT,370)	BAD 85
	C	DC 350 I=1,NEH	BAD 86
	C	IF (IERRL).EQ.0) GO TO 350	BAD 87
	C	WRITE (IPRINT,385) TYPE(I),ICARD(I)	BAD 88
	C	GO TO (60,65,70,75,80,85,90,95,100,105,110,115,120,125,130,135,140)40	BAD 89
	C	1,145,150,155,160,165,170,175,180,185,190,195,200,205,210,215,220,224D	BAD 90
	C	225,230,235,240,245,250,255,260,265,270,275,280,285,290,295,300,305,310	BAD 91
	C	3,310,315,320,325,330,335,340,345). I	BAD 92
	C	60 WRITE (IPRINT,340)	BAD 93
	C	GO TO 350	BAD 94
	C	65 WRITE (IPRINT,345)	BAD 95
	C	GO TO 350	BAD 96
95	C	70 WRITE (IPRINT,400)	BAD 97
	C	GO TO 350	BAD 98
	C	75 WRITE (IPRINT,405)	BAD 99
	C	GO TO 350	BAD 100
	C	80 WRITE (IPRINT,410)	BAD 101
	C	GO TO 350	BAD 102
	C	85 WRITE (IPRINT,415)	BAD 103
	C	GO TO 350	BAD 104
	C	90 WRITE (IPRINT,420)	BAD 105
	C	GO TO 350	BAD 106
	C	95 WRITE (IPRINT,425)	BAD 107
	C	GO TO 350	BAD 108
	C	100 WRITE (IPRINT,430)	BAD 109
	C	GO TO 350	BAD 110
	C	105 WRITE (IPRINT,435)	BAD 111
	C	GO TO 350	BAD 112
	C	110 WRITE (IPRINT,440)	BAD 113
	C	GO TO 350	BAD 114
	C	115 WRITE (IPRINT,445)	BAD 115
	C	GO TO 350	BAD 116

03/07/80 11.41.06

FTN 4.6+433E

SUBROUTINE MAJATA 74/74 UP1=1

```
115      120 WHITE (IPRNT+450)
          GC TO 350
          125 WHITE (IPRNT+455)
          GC TO 350
          130 WHITE (IPRNT+460)
          GC TO 350
          135 WHITE (IPRNT+465)
          GC TO 350
          140 WHITE (IPRNT+470)
          GC TO 350
          145 WHITE (IPRNT+475)
          GC TO 350
          150 WHITE (IPRNT+480)
          GC TO 350
          155 WHITE (IPRNT+485)
          GC TO 350
          160 WHITE (IPRNT+490)
          GC TO 350
          165 WHITE (IPRNT+495)
          GC TO 350
          170 WHITE (IPRNT+500)
          GC TO 350
          175 WHITE (IPRNT+505)
          GC TO 350
          180 WHITE (IPRNT+510)
          GC TO 350
          185 WHITE (IPRNT+515)
          GC TO 350
          190 WHITE (IPRNT+520)
          GC TO 350
          195 WHITE (IPRNT+525)
          GC TO 350
          200 WHITE (IPRNT+530)
          GC TO 350
          205 WHITE (IPRNT+535)
          GC TO 350
          210 WHITE (IPRNT+540)
          GC TO 350
          215 WHITE (IPRNT+545)
          GC TO 350
          220 WHITE (IPRNT+550)
          GC TO 350
          225 WHITE (IPRNT+555)
          GC TO 350
          230 WHITE (IPRNT+560)
          GC TO 350
          235 WHITE (IPRNT+565)
          GC TO 350
          240 WHITE (IPRNT+570)
          GC TO 350
          245 WHITE (IPRNT+575)
          GC TO 350
          250 WHITE (IPRNT+580)
          GC TO 350
          255 WHITE (IPRNT+585)
          GC TO 350
          260 WHITE (IPRNT+590)
```

```
BAD 115
BAD 116
BAD 117
BAD 118
BAD 119
BAD 120
BAD 121
BAD 122
BAD 123
BAD 124
BAD 125
BAD 126
BAD 127
BAD 128
BAD 129
BAD 130
BAD 131
BAD 132
BAD 133
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BAD 135
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BAD 141
BAD 142
BAD 143
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BAD 148
BAD 149
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BAD 151
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BAD 153
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BAD 156
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BAD 160
BAD 161
BAD 162
BAD 163
BAD 164
BAD 165
BAD 166
BAD 167
BAD 168
BAD 169
BAD 170
BAD 171
```


03/07/80 11.41.06

FIN 4.6+433E

SUBROUTINE BAUTA 74/74 OPT=1

420 FORMAT (5X,17#FIELD 3 = FIELD 4)
 425 FORMAT (5X,45#FIELD 3 OR 4 GREATER THAN 44 OR LESS THAN 1)
 430 FORMAT (5X,138#FIELD 3 GREATER THAN 22 OR LESS THAN 1)
 435 FORMAT (5X,17#FIELD 4 = FIELD 5)
 440 FORMAT (5X,44#FIELD 4 OR 5 GREATER THAN 44 OR LESS THAN 1)
 445 FORMAT (5X,39#FIELD 7+8 OR 9 LESS THAN OR EQUAL TO 0)
 450 FORMAT (5X,12#FIELD 10 OR 11 LESS THAN 0)
 455 FORMAT (5X,35#FIELD 10=0 AND FIELD 11 NOT EQUAL 0)
 460 FORMAT (5X,35#FIELD 10 NOT EQUAL 0 AND FIELD 11=0)
 465 FORMAT (5X,39#FIELD 12 GREATER THAN 50 OR LESS THAN 1)
 470 FORMAT (5X,38#FIELD 3 GREATER THAN 22 OR LESS THAN 1)
 475 FORMAT (5X,37#FIELD 4 GREATER THAN 2 OR LESS THAN 1)
 480 FORMAT (5X,40#FIELD 5 GREATER THAN 1000 OR LESS THAN 1)
 485 FORMAT (5X,46#FIELD 4=1 AND FIELD 9 LESS THAN OR EQUAL TO 0)
 490 FORMAT (5X,33#FIELD 4=2 AND FIELD 9 NOT EQUAL 0)
 495 FORMAT (5X,28#FIELD 7+8 OR 10 LESS THAN 0)
 500 FORMAT (5X,38#FIELD 3 GREATER THAN 44 OR LESS THAN 1)
 505 FORMAT (5X,24#FIELD 7 OR 8 LESS THAN 0)
 510 FORMAT (5X,19#FIELD 3 LESS THAN 0)
 515 FORMAT (5X,27#FIELD 3 NOT EQUAL 0,1, OR 2)
 520 FORMAT (5X,28#FIELD 3 LESS THAN OR EQUAL 0)
 525 FORMAT (5X,28#FIELD 4 LESS THAN OR EQUAL 0)
 530 FORMAT (5X,25#FIELD 5 LESS THAN FIELD 3)
 535 FORMAT (5X,30#THE JUNCTION NUMBER ASSIGNED TO THE ANCHOR(FIELD 3) BAD 251
 HAS BEEN ASSIGNED TO A PRECEDING ANCHOR CARD OR/5X,52HTO AN S=L JUNCTBAD 253
 21CN (FIELD 5) ON A PRECEDING CAB CARD)
 540 FORMAT (5X,14#THE JUNCTION NUMBER ASSIGNED TO THE S=L JUNCTION (FIELD 5) BAD 254
 HAS BEEN ASSIGNED ON A PRECEDING CAB CARD OR/5X,55HTO AN BAD 256
 2ACHON JUNCTION (FIELD 3) ON A PRECEDING ANCHOR CARD)
 545 FORMAT (5X,82#A TYPE 3 ERROR APPEARS ONLY IN CONJUNCTION WITH A CABAD 258
 IN CARD AND INDICATES THAT THE /5X,60#NUMBER ASSIGNED TO THE CABLE BAD 259
 2U(FIELD 3) HAS BEEN ASSIGNED ON A PRECEDING CAB CARD)
 550 FORMAT (5X,97#THE JUNCTION NUMBER ASSIGNED IN FIELD 3 HAS BEEN ASSBAD 261
 IGNED IN FIELDS 3 OR 4 OF A PRECEDING IR CARD)
 555 FORMAT (5X,71#THE JUNCTION NUMBER ASSIGNED IN FIELD 4 HAS BEEN ASSBAD 263
 IGNED IN FIELD 3 OF A PRECEDING IR CARD)
 560 FORMAT (5X,50#AN NJNC CARD HAS PREVIOUSLY APPEARED IN THE PARTICULARBAD 265
 IAR SOURCE DECK)
 565 FORMAT (5X,50#A DEN CARD HAS PREVIOUSLY APPEARED IN THE PARTICULARHAD 267
 I SOURCE DECK)
 570 FORMAT (5X,65#A COMP CARD HAS PREVIOUSLY APPEARED IN THE PARTICULARHAD 269
 IR SOURCE DECK)
 575 FORMAT (5X,77#TWENTY FIVE VEL CARDS HAVE PREVIOUSLY APPEARED IN THBAD 271
 LE PARTICULAR SOURCE DECK)
 580 FORMAT (5X,74#THE Z COORDINATE AT WHICH THE CURRENT VELOCITY IS SPRAD 273
 ECIFIED (FIELD 3) HAS /5X,63#HREEN USED ON A PRECEDING VEL CARD IN BAD 274
 THE PARTICULAR SOURCE DECK)
 585 FORMAT (5X,65#AN ANG CARD HAS PREVIOUSLY APPEARED IN THE PARTICULARHAD 276
 IR SOURCE DECK)
 590 FORMAT (5X,116#A TYPE 7 ERROR INDICATES AN INADEQUACY OF INFORMATIONHAD 278
 ON IN THE CABLE ARRAY SOURCE DECK(OR TAPE). THE OTHER INFORMATION/BAD 279
 25X,119#COLUMNS UNDER THE ERROR HEADING CONTAINS A 1X3 MATRIX, THE BAD 280
 ELEMENTS OF WHICH GIVE RESPECTIVELY THE NUMBER OF NJNC CARDS/5X,12#HAD 281
 HEAD, THE NUMBER OF DEN CARDS READ, AND THE NUMBER OF ANCH CARDS BAD 282
 READ. A ZERO ELEMENT IS AN ERROR(SEE CABLE ARRAY SOURCE DECK)) BAD 283
 595 FORMAT (5X,114#A TYPE 8 ERROR INDICATES A DISCONTINUITY IN NUMBERSBAD 284
 IN THE CABLES IN THE ARRAY). THE OTHER INFORMATION COLUMN UNDER /5X#HAD 285

[illegible]

345 655 FORMAT (5X,112HA TYPE 14 ERROR INDICATES AN INADEQUATE TRANSMISSION BY THE ANBAD 343
7C CARDS (FIELD 6 OF THE ANG CARDS), AND THE 75X,125H NUMBER OF ANG CARDS 344
RHS HEAD/5X,125HIF COLUMN 1 CONTAINS A ZERO, THEN A COMP CARL HASBAD 345
9 NOT APPEARED AFTER THE FIRST READ AND USE PARAMETRIC STUDY SOURCE 346
XCE DECK).) BAD 347

350 655 FORMAT (5X,112HA TYPE 14 ERROR INDICATES AN INADEQUATE TRANSMISSION BY THE ANBAD 348
11ION IN A PARAMETRIC STUDY SOURCE DECK, THE OTHER INFORMATION 75X,18AD 349
522PCOLUMN UNDER THE FREQ HEADS CONTAINS A 1 X 5 MATRIX, THE ELEBAD 350
3MENTS OF WHICH GIVE, RESPECTIVELY, THE NUMBER OF COMP CARL/5X,121HAD 351
4READ, THE CURRENT FIELD OPTION, THE NUMBER OF VEL CARDS HEAD, THEBAD 352
5 NUMBER OF VEL CARDS CONTAINING A 2 COORDINATE (FIELD 3)/5X,111LEBAD 353
655 THAN OF EQUAL TO THE MINIMUM 2 COORDINATE TRANSMISSION BY THE ANBAD 354
7C CARDS (FIELD 6 OF THE ANG CARDS), AND THE 75X,125H NUMBER OF ANG CARDS 355
RHS HEAD/5X,117HIF COLUMN 2 CONTAINS A ONE AND ANY OF COLUMNS 3-4AD 356
9, ON 5 CONTAIN A ZERO, THEN THE STANDARD CURRENT FIELD HAS NOT BEEN 357
IN 75X,125HIF COLUMN 2 CONTAINS A ONE AND ANY OF COLUMNS 3-4AD 358
30 STANDARD CURRENT FIELD).) BAD 359

360 660 FORMAT (5X,106HA TYPE 15 ERROR INDICATES THAT AN UNPERMITTED CHANGBAD 360
1E HAS BEEN ATTEMPTED IN A PARAMETRIC STUDY SOURCE DECK. 75X,36H(SEEHAD 361
2 PARAMETRIC STUDY SOURCE DECKS).) BAD 362

365 665 FORMAT (5X,114HA TYPE 16 ERROR INDICATES AN IMPROPER DECK STRUCTUREHAD 363
1E. SEE CABLE ARRAY SOURCE DECK, PARAMETRIC STUDY SOURCE DECKS/75XAD 364
670 FORMAT (5X,101HA TYPE 17 ERROR INDICATES THAT THE CABLE ARRAY SOURCEHAD 366
ICE DECK (CM TAPE) CONTAINS MORE THAN 2150 RECORDS. 75X,119H(SEE THEAD 367
2H INFORMATION COLUMN UNDER THE ERROR HEADS CONTAINS THE MESSAGE 75X,119H(SEE THEAD 368
3CCOMPUN/BL/ MOUTUS EXCEEDED. SEE USERS MANUAL. 75X,125HA TYPE 17 EHAD 369
4OR IS READILY CORRECTABLE IF THE MACHINE BEING USED HAS SUFFICIENTHAD 370
5 COME STORAGE. THIS CORRECTION IS ACHIEVED BY 75X,124HCHANGING THEAD 371
6 HOW DIMENSION OF DATA ON CARDS DE5025 AND INFO22 FROM 2150 TO A BAD 372
7NUMBER EXCEEDING THE NUMBER OF RECORDS IN THE 75X,123HCHAD 373
8SOURCE DECK (OR TAPE). SIMULTANEOUSLY, THE COMPARISON VALUE ON CARBAD 374
90 INPETS MUST BE CHANGED FROM 2150 TO THE NEW 75X,23HCHAD 375
30F DATA).) BAD 376

375 675 FORMAT (5X,108HA TYPE 18 ERROR INDICATES THAT THE ACCURACY REQUIREHAD 377
10 FOR THE ARRAY EQUILIBRIUM CALCULATIONS (FIELD 3 OF THE 75X,9HCHAD 378
2MP CARD) HAS NOT BEEN OBTAINED DURING THE CALCULATIONS. THIS IS FORHAD 379
34 ONE OF TWO POSSIBLE REASONS. 75X,116HA. SOME CABLE SEGMENTS HAVEHAD 380
4F GONE SLACK (THIS IS THE SEGMENTS HAVE NEAR ZERO TENSION). AN EXAMHAD 381
SITUATION OF THE TENSIONS/5X,112HPRINTED OUT IN CONJUNCTION WITH A 18AD 382
6TYPE 14 ERROR WILL REVEAL IF THIS IS THE REASON. IF IT IS, SEE THE BAD 383
7SECTION ON 75X,9HCHAD 384
8SECTION ON 75X,9HCHAD 385
9CY REQUIRED FOR THE EQUILIBRIUM CALCULATIONS IS SIMPLY TOO STRINGENTHAD 386
3NT FOR THE COMPUTER TO HANDLE (SEE COMP CARL). 75X,120HAN EXAMINAD 387
5OR OF THE FINAL VALUE OF THE ACCURACY OBTAINED, PRINTED OUT IN COMBAD 388
JUNCTION WITH A TYPE 18 ERROR, WILL REVEAL 75X,102H(SEE THE BEST ACCURAD 389
BY OBTAINABLE. FIELD 3 OF THE COMP CARD SHOULD BE MODIFIED TO REFLECTHAD 390
GET THIS INFORMATION.) BAD 391
END BAD 392-

*CHECK CPLT

```

SUBROUTINE CPLT (I,OPT,IPRNT,PJUNC,NANC,TITLE,ANJUNC)
COMMON /CPLT/ ZUP,ZDN,DZ,XMIN,XMAX,YMIN,YMAX,YIN,ANG,XY
COMMON /PIBLK/ PI
DIMENSION X(100), Y(100)
DIMENSION PSPACE(3), W(3), TITLE(8)
INTEGER ANJUNC

```

```

C
C SET UP PERSPECTIVE TRANSFORMATIONS
C

```

```

UP(XP,YP)=XF+YP*EX
VP(YP)=YP*EY

```

```

C
C INITIALIZATION
C

```

```

DTM=PI/180.
EX=COS(ANG*DTM)
EY=SIN(ANG*DTM)
HGT=0.07

```

```

C
C CALCULATE SPACE BETWEEN PLOTS
C

```

```

NZ=(ZUP-ZDN)/DZ+1.00001

```

```

PIN=VP(YIN)

```

```

IY=NZ*PIN
SPACE=(10.-IY)/(NZ+1)

```

```

IF (SPACE.GT.0.) GO TO 5
WRITE (IPRNT,75)
RETURN

```

```

5 CONTINUE

```

```

C
C GET COORDINATES
C

```

```

NYI=NY-1
DELI=YIN/NYI
DELU=(YMAX-YMIN)/NYI
NX=(XMAX-XMIN)/DELU+2.00001
IF (NX.GE.3) GO TO 10
WRITE (IPRNT,80)
RETURN

```

```

10 NXI=NX-1
XIN=DELI*NXI
DO 15 I=1,NX
  X(I)=XMIN+(I-1)*DELU
  DO 20 J=1,NY
    Y(I)=YMIN+(J-1)*DELU
  20

```

```

C
C DEFINE SCALE IN UNITS PER INCH
C

```

```

SCALE=DELU/DELI

```

```

C
C FIND NORMALIZATION FACTOR FOR CURRENT
C

```

```

SMAX=0.
DO 40 K=1,NZ
  PSPACE(3)=ZLN*(K-1)*DZ

```

```

*IN FORMAT (27,3)FIELD 3 GREATER THAN 44 OR LESS THAN 10)

```

MAP 228

03/07/80 11:41:06

FIN 4.6*433E

SUBROUTINE CPLT 74/74 OPT=1

```

C
C
C
60      LOOP ON X AND Y
C
C      DC 35 I=2,NX1
C      DC 35 J=2,NY1
C      PSPACE(1)=X(I)
C      PSPACE(2)=Y(J)
C      IF (I*OPT.NE.3) GO TO 25
C      CALL INTVEL (N*PSPACE)
C      XA=XX(1)
C      YA=YY(2)
C      GO TO 30
C
C      25 XA=VELOC(1,PSPACE)
C      YA=VELOC(2,PSPACE)
C      30 S=SQRT(XA**2+YA**2)
C      35 SPAX=AMAX1(SMAX,S)
C      40 CONTINUE
C      SD=0.50*DELI/SMAX
C
C      INITIALIZE AND SET PEN POSITION
C
C      YC=SPACE
C      CALL PLOT (0.,Y0,-3)
C      DC 70 K=1,NZ
C
C      LOOP ON DEPTH LEVELS
C
C      PSPACE(3)=ZDN*(K-1)*DZ
C
C      LABEL DEPTH LEVEL AND INDICATE X-AXIS
C
C      IF (K.EQ.1) GO TO 45
C      YC=PIN+SPACE
C      CALL PLOT (0.,Y0,-3)
C
C      DRAW B07
C
C      45 CALL PLOT (0.,0.,3)
C      PX=UP(0.,YIN)
C      PY=VP(YIN)
C      CALL PLOT (PX,PY,2)
C      PX=UP(XIN,YIN)
C      CALL PLOT (PX,PY,2)
C      CALL PLOT (XIN,0.,2)
C      CALL PLOT (0.,0.,2)
C      XN=0.5*(XIN+PX)*0.25
C      YN=0.5*(PY+PGI)
C      CALL NUMBER (XN,YN,PGI,PSPACE(3),0.,0.)
C      CALL SYMBOL (XIN*.25,0.,HGT,IMX,0.,1)
C      CALL SYMBOL (-.25,0.,HGT,IMX,0.,1)
C
C      PLOT SYMBOL AT EACH ANCHOR POINT
C      DC 50 N=1,NZ
C      Z=ZJUN(C(1))
C      XN=(PJUNC(1,0,1)-XMIN)/SCALE
C      YN=(PJUNC(1,0,1)-YMIN)/SCALE
C      PY=0.06*(XN+YAN)

```

```

115      FY=VP(YAN)
      IF (XAN.GT.XIN.OR.XAN.LT.0.) GO TO 50
      IF (YAN.GT.YIN.OR.YAN.LT.0.) GO TO 50
      CALL SYMBOL (FXO,PYO,HGI,11.0.0.0.0)
      50 CONTINUE
120      C
      C      LOOP ON X AND Y
      C
      DO 65 I=2,NX1
      DO 65 J=2,NY1
      PSPACE(1)=X(I)
      PSPACE(2)=Y(J)
      IF (1/(VF1.NF.3) GO TO 55
      CALL INTVEL (W,WSPACE)
      XA=XW(1)*SU
      YA=YW(2)*SU
      60 TO 60
      55 XA=VELOC(1),PSPACE)*SU
      YA=VELOC(2,PSPACE)*SU
      C
      C      DRAW ARROW
      C
      C      CALCULATE DISTANCE FROM XMIN,YMIN TO TAIL OF ARROW (INCHES).
      C
      CX=X(1)-XMIN)/SCALE
      CY=(Y(1)-YMIN)/SCALE
      PY1=VP(XS,Y)
      PY1=VP(Y)
      CALL PLOT (PX1,PY1,3)
      C
      C      CALCULATE DISTANCE FROM XMIN,YMIN TO HEAD OF ARROW (INCHES)
      C
      CX=X(2)-XMIN)/SCALE
      CY=(Y(2)-YMIN)/SCALE
      PY2=VP(XE,Y)
      PY2=VP(YE)
      CALL PLOT (PX2,PY2,2)
      C
      C      DRAW ARROW HEAD
      C
      DX=FX2-FX1
      DY=FY2-FY1
      ANGLE=ATAN2(DY,DX)/UTH-90.
      HGS=0.28*SQRT(DX**2+DY**2)
      CALL SYMBOL (PX2+Y2,HGS,6,ANGLE,-1)
      65 CONTINUE
      70 CONTINUE
      C
      C      PLOT TITLE
      C
      YC=PIN*0.5*SPACE
      CALL SYMBOL (0,YC,0,0,TITLE,0,0,80)
      C
      C      SET ORIGIN FOR NEXT PLOT
      C
      XC=2.0*MIN
      YC=-(N7-1)*(PIN*SPACE)-SPACE
      90 TO 150

```

END 114

CALL PLOT (X0,Y0,-3)
RETURN

C

175

15 FCRMA1 (////1X,57H TOTAL HEIGHT OF PLOT EXCEEDS 10. INCHES, PLOT NOCPL 175
IT (CREATED////)
60 FCRMA1 (////1X,88H THE NUMBER OF GRID POINTS IN THE X DIRECTION IS LCPL 177
LESS THAN 3, 10 CORRECT THIS INCREASE NY////)
END

CPL 172
CPL 173
CPL 174
CPL 175
CPL 176
CPL 177
CPL 178
CPL 179-

03/07/80 11.41.06

FTN 4.643JE

74/74 OPT=1

SUBROUTINE SSP

```

60      RESTORE GLOBAL COORDINATES
        CALL READS (3,A(1)),H33)
        HEAD VIEW CONTROL CARD
        NFR=1
        XX(1)=0.
        XX(2)=0.
        XX(3)=0.
        XX(4)=0.
        XX(5)=0.
        XX(6)=0.

70      TEST ANGLES FOR ADMISSIBILITY
        L=0
        DO 5 K=1,3
          IF (ABS(H(K)).LT.360.1) GO TO 5
          L=L+1
        5 CONTINUE
        IF (L.LT.2) GO TO 10
        WRITE (IP,100)
        STOP 21
        10 CONTINUE

80      DEFINE PLUG COORDINATES FOR THIS VIEW
        CALL P1 (A(1),A(2),A(3),NUMNP,TH,XX)
        PLUG NFR FRAMES IN THIS VIEW
        DO 90 N=1,NFR
          REWIND 4
        90      READ FRAME DATA
        KTYPE=1
        HY-PASS BOUNDARY ELEMENT PLOTTING
        IF (KTYPE.EQ.7) GO TO 90

100     TEST FOR ADMISSIBLE ELEMENT TYPE
        IF (KTYPE.GT.0.AND.KTYPE.LE.8) GO TO 15
        IF (KTYPE.EQ.12) GO TO 15
        STOP 22
        15 CONTINUE

105     ADVANCE ELEMENT TAPE 4 TO THIS ELEMENT TYPE
        DO 20 L=1,NELTYP
          K=L
          IF (KEL(L).EQ.KTYPE) GO TO 25
          20 CONTINUE
          25 NEXT L
          IF (M.LT.1) GO TO 40

```


03/07/80 11.41.06

FTN 4.6.433E

7474 OPT=1

SUMMULTINE SSP

```

C      PLOT THIS ELEMENT
C      ILINE=0 , SOLID LINE , UNFORMED
C      ILINE=5 , DASHED LINE , NO CURRENT
C      ILINE=0
C      IF (IPOPT.EC.0) ILINE=5
C      IF (IPOPT.EC.2.AND.NE.GT.NUMEL/2) ILINE=5
C      CALL P2 (A(N1)+A(N2),NP,NP(4),NP(5),NP(6),NP(9),NP(10),LR2,ILINE)
C      RC CONTINUE
C      PLOT FRAME LABELS AND TITLE CARDS
C      B5 CALL P3 (MCL,TH)
C      9C CONTINUE
C      9S CONTINUE
C      CLOSE THE PLOT FILE
C      IF(1)=TH(1)+90.
C      IF(2)=TH(2)+90.
C      IF(3)=TH(3)+90.
C      SIZE=SAVS1Z
C      CALL PLOT (0.0,-0.95,-3)
C      RETURN
C      100 FORMAT (//23H SOLUTION TERMINATED***//20H TWO ANGLES .GT. 360)
C      105 FORMAT (8X,10HSEQUENCE =,I2,26H ON CARD ABOVE IS IN ERROR.)
C      END

```

```
1      *DECK PORTB
2      SUBROUTINE PORTB (NUMP,NELIYP,N1,N2,N3,N33,KEL)
3
4      DIMENSION HED(12), IX(19), NP(18), LOUT(12), LIN(12), NPAR(14),
5      K(12), AP(19)
6
7      COMMON A(6600)
8
9      EQUIVALENCE (IX(2),NP(1),AP(1))
10
11      DATA LIN/3,3,5,5,9,5,6,17,0,0,0,4/,LOUT/2,2,4,4,8,4,0,16,0,0,0,18/,
12      NP/60
13      IP=61
14
15      NTR=10
16
17      HEAD AND REFORMAT THE PUTHOLE TAPE - NTR
18
19      REWIND NTR
20
21      1 HEADING AND CONTROL INFORMATION
22      HEAD (NTR) (HED(K),K=1,12),NUMP,NELIYP
23
24      2 EQUATION NUMBERS FOR RETAINED DEGREES OF FREEDOM
25      HEAD (NTR)
26
27      SET UP ARRAY SIZE FOR COORDINATES
28
29      N1=1
30      N11=NUMP
31      N2=N1+NUMP
32      N22=2*NUMP
33      N3=N2+NUMP
34      N33=3*NUMP
35      N4=N3+NUMP
36      I=LOC(A(N4))
37
38      3 HEAD NODE COORDINATES
39      HEAD (NTR) (A(K),K=N1,N11)
40      HEAD (NTR) (A(K),K=N2,N22)
41      HEAD (NTR) (A(K),K=N3,N33)
42
43      PRINT FIRST AND LAST NODE COORDINATES
44
45      SAVE NODE COORDINATES ON TAPE 3
46
47      REWIND 3
48      CALL WRITES (3,A(N1),N33)
49
50      4 NODE TEMPERATURES
```



```

115      25 CONTINUE
      NLMFIX=NPAP(4)
      NLMMAI=NPAP(3)
      MATERIAL PROPERTIES
      C
120      9 UC 30 ISKIP=1,NUMMAT
      READ (NTB)
      9
      10
      11 HEAD (NTB)
      30 CCNINUE
      10
      11
      12 HEAD (NTB)
      C
130      12
      IF (NLMFIX.GT.0) READ (NTB)
      12
      C
      135      HEAD (NTB)
      GC TO 100
      C
      140      35 CONTINUE
      40 CCNINUE
      C
      145      MAT=NPAP(3)
      C
      150      45 ISKIP=1,MAT
      13
      14 HEAD (NTB)
      13
      14
      14 HEAD (NTB)
      14
      45 CCNINUE
      15
      15 HEAD (NTB)
      15
      15 GC TO 100
      C
      155      50 CONTINUE
      NLD=NPAP(4)
      16
      16 HEAD (NTB)
      16
      17
      17 IF (NLD.GT.0) READ (NTB)
      17
      17 HEAD (NTB)
      17
      17
      17 GC TO 100
      C
      170      55 CONTINUE
      19
      MATERIAL PROPERTIES
      C

```

```

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175      ALMMAT=NPAT(3)
      DC 60 ISKIP=1,NUMMAT
      HEAD (NTB)
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230 LRR2=LR2
    IF (IELTYP.EQ.12) LRR2=3
    DC 125 K=1,NUPEL
    C
    CALL HEADS (NIB,IX,LR)
    C
    C BY-PASS THE BOUNDARY ELEMENTS
    IF (IELTYP.EQ.7) GO TO 120
    C
    C CHECK FOR SEQUENTIAL INPUT ORDER
    IF (IX(1).EQ.N) GO TO 105
    WRITE (IP,145) IX(1),K,I
    CALL EX11
    C
    C 105 CONTINUE
    C
    C TEST FOR FOURTH MODE ZERO
    IF (LR2.NE.4) GO TO 110
    IF (NP(4),L1,1) NP(4)=NP(3)
    C
    C 110 IF (IELTYP.NE.12) GO TO 115
    C
    C READ RADIUS,KODE,X3P (BEND), OR JUNK (TANGENT)
    C
    C READ (NIB) AP(4),NP(5),AP(6),AP(7),AP(8)
    IF (NP(1).EQ.1) GO TO 115
    C
    C BEND, READ THETA AND DC ARRAY
    C
    C HEAD (NT8) (AP(IJL),IJL=9,18)
    C
    C PIPE TAPE SAVE FORMATS (TAPE4)
    C TANGENT - 1,N1,NJ,XLN,JUNK(5)-JUNK(14)
    C BEND - 2,N1,NJ,RADIUS,KODE,X3P,THETA,DC(1,1)-DC(3,3)
    C
    C 115 CALL WRITES (4,NP,LR2)
    C
    C PRINT FIRST AND LAST ELEMENT CONNECTIONS
    C
    C 120 CONTINUE
    C
    C 125 CONTINUE
    C
    C 130 CONTINUE
    C
    C RETURN
    C
    C 135 FORMAT (////23H SOLUTION TERMINATED***,//39H NO END-OF-FILE ENCOUNTERED)
    C 140 FORMAT (//20H ***ERROR*** ELEMENT TYPE (12,23H) FINCOUNTED ON TAPPOUR 279
    C 145 FORMAT (//20H ***ERROR*** ELEMENTS ON TAPEB ARE NOT SEQUENTIAL,5X,3POR 281
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*DECK WRITES
SUBROUTINE WRITES (ITAPE,A,LREC)
DIMENSION A(LREC)
WRITE (ITAPE) A
RETURN
END

SUBROUTINE HEADS

74/74 OPT=1

FTN 4.6+433F

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PAGE 1

1
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*DECL. HEADS
SUBROUTINE HEADS (ITAPL,A,LREC)
DIMENSION A(LREC)
HEAD (ITAPL) A
RETURN
END

HEA 1
HEA 2
HEA 3
HEA 4
HEA 5
HEA 6-

```

1      *ELECT P1
2      SUBROUTINE P1 (U,V,M,NUMP,TH,XM)
3
4      C
5      C PLOT VIEW INITIALIZATION PROGRAM
6      C
7      C DIMENSION U(1), V(1), W(1), TH(1), XM(1)
8      C
9      C COMMON /MESH/ XX(12),YY(12),XLEN,YLEN,ALEN,EX(3),EY(3),XMIN,YMIN
10     C
11     C DATA RAD/0.01745329254/
12     C
13     C CONVERT COORDINATES TO A TWO-DIMENSIONAL PROJECTION
14     C
15     C UC 5 I=1,3
16     C   EX(I)=SIN(TH(I)*RAD)
17     C   EY(I)=COS(TH(I)*RAD)
18     C   IF (TH(I).LE.350.) GO TO 5
19     C   EX(I)=0.
20     C   EY(I)=0.
21     C   S CONTINUE
22     C
23     C UC 10 I=1,NUMP
24     C   TEMP=U(I)*EY(1)+V(I)*EY(2)+W(I)*EY(3)
25     C   U(I)=U(I)*EX(1)+V(I)*EX(2)+W(I)*EX(3)
26     C   V(I)=TEMP
27     C   10 CONTINUE
28     C
29     C CONVERT MAX/MIN CONTROL DIMENSIONS TO THE PLOT SYSTEM (U,V)
30     C
31     C DUM=0.0
32     C UC 15 K=1,6
33     C   IF (DUM.LT.+.001) GO TO 25
34     C
35     C   U1=XM(1)*EX(1)
36     C   U2=XM(2)*EX(1)
37     C   U3=XM(1)*EY(1)
38     C   U4=XM(2)*EY(1)
39     C   U5=XM(1)*EX(2)
40     C   U6=XM(4)*EX(2)
41     C   U7=XM(3)*EY(2)
42     C   U8=XM(4)*EY(2)
43     C   U9=XM(5)*EX(3)
44     C   U10=XM(6)*EX(3)
45     C   U11=XM(5)*EY(3)
46     C   U12=XM(6)*EY(3)
47     C
48     C U - VALUES FOR MAX/MIN CONTROL POINTS
49     C
50     C   W(1)=U1+U5+U9
51     C   W(2)=U1+U6+U10
52     C   W(3)=U1+U5+U11
53     C   W(4)=U1+U6+U12
54     C   W(5)=U2+U5+U9
55     C   W(6)=U2+U6+U10
56     C   W(7)=U2+U5+U11
57     C   W(8)=U2+U6+U12

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C
60      W(9)=D3*U7*U11
        W(10)=D3*U8*U11
        W(11)=D3*U7*U12
        W(12)=D3*U8*U12
        W(13)=D4*U7*U11
        W(14)=D4*U8*U11
        W(15)=D4*U7*U12
        W(16)=D4*U8*U12
C
70      FIND MAX-MIN DIMENSIONS IN THE CONTROLLED SCALE DIMENSIONS
C
C      XMIN=W(1)
        YMIN=W(9)
        XMAX=W(11)
        YMAX=W(9)
C
75      DO 20 I=2,8
        IF (YMIN.GT.W(I)) XMIN=W(I)
        IF (W(I).GT.XMAX) XMAX=W(I)
        IF (YMIN.GT.W(I+8)) YMIN=W(I+8)
        IF (W(I+8).GT.YMAX) YMAX=W(I+8)
        CONTINUE
        GO TO 35
C
80      FIND MAX-MIN DIMENSIONS FROM NODAL POINT ARRAY (NO USER CONTROL)
C
C
85      25 XMIN=U(1)
        YMIN=V(1)
        XMAX=U(1)
        YMAX=V(1)
C
90      DO 30 I=2,NUMGRP
        IF (XMIN.GT.U(I)) XMIN=U(I)
        IF (U(I).GT.XMAX) XMAX=U(I)
        IF (YMIN.GT.V(I)) YMIN=V(I)
        IF (V(I).GT.YMAX) YMAX=V(I)
        CONTINUE
C
95      30 SHIFT PLOT ANGLES FOR SYMBOL PLOT OF GLOBAL AXES
C
C
100     35 DO 40 I=1,3
        TP(I)=T(I)-70.0
        CONTINUE
C
C
110     40 FIND PROPER HORIZONTAL SCALE
C
C
        YLEN=(YMAX-YMIN)/10.0
        IF (YLEN.GT.0.0) GO TO 45
        XLEN=(XMAX-XMIN)/10.0
        XLEN=10.0
        GO TO 50
        45 XLEN=(XMAX-XMIN)/YLEN
        YLEN=YLEN
        IF (XLEN.GT.30.0) GO TO 50
        XLEN=(XMAX-XMIN)/30.0
        YLEN=YLEN

```

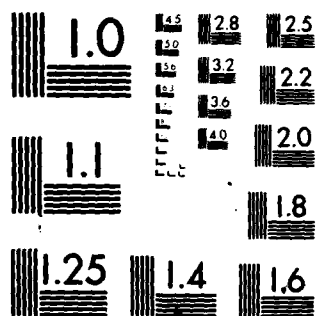
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CIVIL ENGINEERING LAB (NAVY) PORT HUENEME CA F/G 13/13
DECEL1 USERS MANUAL. A FORTRAN IV PROGRAM FOR COMPUTING THE STA--ETC(U)
AUG 80 S SERGEV
UNCLASSIFIED CEL-TN-1584

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MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A

03/07/80 11.41.06

FIN 4.6433E

OPT=1

SUBROUTINE P1

74/74

```

115      ALEN=30.0
        C
        C SET SCALE PARAMETERS
        C
        C 50 CONTINUE
        XX(11)=0.0
        XX(12)=ALEN
        YY(11)=0.0
        YY(12)=YLEN
        C
        C CONVERT PLOT ORDINATES TO RELATIVE VALUES
        C
        DO 55 I=1,NLUMP
          U(I)=U(I)-XPMIN
          V(I)=V(I)-YMIN
        55 CONTINUE
        C
        RETURN
        END
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```

P1 115
P1 116
P1 117
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P1 126
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P1 132
P1 133

CARD NO. SEVERITY DETAILS DIAGNOSIS OF PROBLEM

CARD NO.	SEVERITY	DETAILS	DIAGNOSIS OF PROBLEM
36	I	XM	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
38	I	XM	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
39	I	XM	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
40	I	XM	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
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42	I	XM	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
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45	I	XM	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
46	I	XM	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
51	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
52	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
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67	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
68	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
73	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
75	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.

```
1      *DECK P2
2      SUBROUTINE P2 (U,V,WP,RADIUS,NODE,X3P,THETA,DC,NODES,ILINE)
3
4      C
5      THIS SUBROUTINE PLOTS A 2D 4, 8, OR 16-NODE ELEMENT
6
7      DIMENSION U(1), V(1), NP(1), IT(9)
8      DIMENSION DC(3,3), X3P(3)
9
10     COMMON /MESH/ XX(12),YY(12),XLEN,YLEN,ALEN,EX(3),EY(3),XMIN,YMIN
11
12     DATA II/9,2,10,3,11,4,12,1,9/
13     DATA RAD2/0.03490658/
14
15     C
16     DETERMINE THE TYPE OF ELEMENT TO BE PLOTTED
17
18     IF (NODES.EQ.16) GO TO 40
19     IF (NODES.EQ.8) GO TO 25
20     IF (NODES.EQ.4) GO TO 15
21
22     N=0
23     IM=0
24     IN=0
25     IN=ILINE
26     IF (NODES.NE.16) GO TO 5
27     IF (NP(1).EQ.2) GO TO 60
28
29     N=1
30     IM=1
31     IN=1
32
33     C
34     TWO NODE ELEMENT
35
36     5 DC 10 M=1,2
37     N=N+1
38     J=NP(N)
39     XX(M)=U(J)
40     YY(M)=V(J)
41
42     10 XX(3)=XX(1)
43     XX(4)=XX(2)
44     YY(3)=YY(1)
45     YY(4)=YY(2)
46
47     C
48     CALL LINE (XX,YY,2,1,IM,IN)
49     RETURN
50
51     C
52     FOUR NODE ELEMENT (QUADRILATERAL OR TRIANGLE)
53
54     15 CONTINUE
55     DC 20 M=1,4
56     J=NP(M)
57     XX(M)=U(J)
58     YY(M)=V(J)
59
60     20 YY(5)=YY(1)
61     YY(6)=YY(2)
62     YY(7)=YY(3)
63     YY(8)=YY(4)
64     YY(9)=YY(1)
65     YY(10)=YY(2)
66     YY(11)=YY(3)
67     YY(12)=YY(4)
68
69     C
```


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FTN 4-6-433E

SUBROUTINE P2 74/74 OPT=1

```
CALL LINE (XX,YY,5,1,0,0)
RETURN
60 C EIGHT NODE ELEMENT (BRICK OR WEDGE)
C
C 25 CONTINUE
DO 30 M=1,4
  J=NP(M)
  XX(M)=U(J)
  YY(M)=V(J)
30 C
C
C 35 M=5,0
  J=NP(M)
  J=NP(JJ)
  XX(M)=U(J)
  YY(M)=V(J)
35 C
C
C 75 XX(9)=XX(1)
  YY(9)=YY(1)
  XX(10)=XX(4)
  YY(10)=YY(4)
C
C 80 CALL LINE (XX,YY,10,1,0,0)
  XX(9)=XX(5)
  YY(9)=YY(5)
  XX(10)=XX(8)
  YY(10)=YY(8)
C
C 85 CALL LINE (XX(9),YY(9),2,1,0,0)
  XX(9)=XX(6)
  YY(9)=YY(6)
  XX(10)=XX(3)
  YY(10)=YY(3)
C
C 90 CALL LINE (XX(9),YY(9),2,1,0,0)
  XX(9)=XX(2)
  YY(9)=YY(2)
  XX(10)=XX(7)
  YY(10)=YY(7)
C
C 95 CALL LINE (XX(9),YY(9),2,1,0,0)
  RETURN
C
C SIXTEEN NODE ELEMENT (THICK SHELL)
C
C 100 40 CONTINUE
C
C
C TOP AND BOTTOM (USING SYMBOL FOR MID-NODES)
  IAC=0
  DO 50 I=1,2
    IF (I-EQ,2) INC=4
    DO 45 M=1,9
      JJ=17(M)+INC
      J=NP(JJ)
      XX(M)=U(J)
      YY(M)=V(J)
50 CALL LINE (XX(2),YY(2),9,1,2,1)
  45 C
  C EDGES
  C
```

```

115      C      DO 55 1,1,0.0
      J=NP(1)
      K=NP(1,4)
      X(9)=U(J)
      Y(9)=V(J)
      X(10)=U(K)
      Y(10)=V(K)
      Y(11)=V(K)
      55 CALL LINE (X(9),Y(9),2,1,0,0)

120      C

125      MEIURA
      C      MEMD (PIPE ELEMENT)
      C
      C      60 NSEG=THETA/RAD2
      IF (NSEG.LT.1) NSEG=1
      J=NP(2)
      X(2)=U(J)
      Y(2)=V(J)
      X(3)=X(1)
      X(4)=X(12)
      Y(3)=V(1)
      Y(4)=Y(12)
      THETA=0.
      EDC11=EX(1)*DC(1,1)+EX(2)*DC(2,1)+EX(3)*DC(3,1)
      EDC12=EX(1)*DC(1,2)+EX(2)*DC(2,2)+EX(3)*DC(3,2)
      EDC21=EX(1)*DC(1,1)+EX(2)*DC(2,1)+EX(3)*DC(3,1)
      EDC22=EX(1)*DC(1,2)+EX(2)*DC(2,2)+EX(3)*DC(3,2)
      CALL LINE (X(2),Y(2),1,1,-1,1)
      INTER=PI*RADIUS
      IE (KODE.EQ.1) RIEHM=RADIUS*IAN(0.5*(THETA)
      UCUM=EX(1)*X3P(1)-DC(1,KODE)*RTERM+EX(2)*X3P(2)-DC(2,KODE)*RTEP2
      IMP)=EX(3)*X3P(3)-DC(3,KODE)*RTERM))-XMIN
      VCOM=(CY(1)*X3P(1)-DC(1,KODE)*RTERM)+EY(2)*X3P(2)-DC(2,KODE)*RTEP2
      IMP)+EY(3)*X3P(3)-DC(3,KODE)*RTERM))-YMIN
      UO 70 1=1,NSEG
      X(1)=X(2)
      Y(1)=Y(2)
      T=TA=THETA+RAD2
      X=RADIUS*SIN(THETA)
      Y=RADIUS*(1-COS(THETA))
      X(2)=UCUM+EDC12*Y+UCOR
      Y(2)=EODC21*X+EDC22*Y+VCOM
      IF (1.LT.NSEG) GO TO 65
      J=NP(3)
      X(2)=U(J)
      Y(2)=V(J)
      65 CALL LINE (X(2),Y(2),1,1,0,0)
      70 CONTINUE
      CALL LINE (X(2),Y(2),1,1,-1,1)
      MEIDUPN
      C
      END
165      END
167-

```

CARD NO. SEVERITY DETAILS DIAGNOSIS OF PROBLEM

131 I NP ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
159 I NP ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.

```

1  CHECK P3
   SUBROUTINE P3 (MED,IM)
   C
   C THIS ROUTINE COMPLETES THE PLOT FRAME
   C
   C DIMENSION MED(1), IM(1), M(3)
   C
   C COMMON /MESH/ XX(12),YY(12),XLEN,YLEN,ALEN,EX(3),EY(3)
   C
   C DATA W/IMX,IMY,IMZ/
   C IM=60
   C IM=61
   C
   C PLOT TITLE AND AXES
   C
   CALL SYMBOL (0.0,-.30,14,MED(1),0.0,80)
   CALL PLOT (-1.5,1.5,-3)
   DC 5 IM,3
   IF (IM(1).GT.270) GO TO 5
   CALL SYMBOL (-5*EX(1),.5*EY(1),1.0,13,IM(1),-1)
   CALL SYMBOL (EX(1),EY(1),0.1,6,IM(1),-1)
   CALL SYMBOL (1.2*EX(1),-.075,1.2*EY(1),-.075,.15*IM(1),0.0,1)
   S CONTINUE
   C
   C ADVANCE PAPER TO NEXT FRAME
   C
   CALL PLOT (1.5,-1.5,-3)
   CALL PLOT (ALEN*7.0,0.0,-3)
   C
   RETURN
   END

```

P3 1
P3 2
P3 3
P3 4
P3 5
P3 6
P3 7
P3 8
P3 9
P3 10
P3 11
P3 12
P3 13
P3 14
P3 15
P3 16
P3 17
P3 18
P3 19
P3 20
P3 21
P3 22
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P3 24
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P3 26
P3 27
P3 28
P3 29
P3 30
P3 31-

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